

CITY OF BRIDGEPORT

| File No. | 9 | |
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PLANNING & ZONING COMMISSION APPLICATION

| If yes, a sworn statement disclosing the Beneficiary shall accompany this application upon filing. Address of Property: (number) (number) (street) (street) (state) (st | . NAME OF APPLICANT: Eaton Enterprises, LLC | |
|--|--|----------------|
| Address of Property: | Is the Applicant's name Trustee of Record? Yes No X | |
| Assessor's Map Information: Block No. 38828 | If yes, a sworn statement disclosing the Beneficiary shall accompany this application upon filing. 378 East Main Street CT Address of Property: 371 East Main Street CT | |
| Amendments to Zoning Regulations: (indicate) Article: | (number) (street) (state) (zi | |
| (Attach copies of Amendment) Description of Property (Metes & Bounds): Nichols Street 483', Pembroke Street 45', State Highway Line, East Main Street 143', Nichols Street 104', East Main Street 165', State Highway Line 184', State Highway Line 103'. Existing Zone Classification: NX3, Row House Zone Classification requested: Describe Proposed Development of Property: Sub-Divide the two lots into 29 individual lots for the construction of Two Bedroom Townhouses. Approval(s) requested: Municipal Coastal Site Plan Review Signature: Print Name: Patrick M Rose, Architect Mailing Address: Rose-Tiso & Co., LLC, 35 Brentwood Ave., Fairfield, CT 06825 Phone: 203-610-6262 Cell: 203-581-2788 Fax: 203-610-6404 E-mail Address: Prose@rosetiso.com \$ Fee received Date: Clerk: THIS APPLICATION MUST BE SUBMITTED IN PERSON AND WITH COMPLETED CHECKLIST & Completed & Signed Application Form & A-2 Site Survey & Building Floor Plans & Completed Site / Landscape Plan & Drainage Plan & Building Elevations & Written Statement of Development and Use & Property Owner's List & Fee **Cert. of Incorporation & Organization and First Report (Corporations & LLC's) | | |
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| E-mail Address:prose@rosetiso.com \$Fee received | | 6404 |
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| Completed & Signed Application Form | \$Fee received Date: Clerk: | |
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| Cert. of Incorporation & Organization and First Report (Corporations & LLC's) PROPERTY OWNER'S ENDORSEMENT OF APPLICATION BLD-WF LLC 4-24-24 | ★ Completed Site / Landscape Plan ★ ■ ★ Drainage Plan ★ Building | ng Elevations |
| PROPERTY OWNER'S ENDORSEMENT OF APPLICATION BLD-WF LLC 4-24-24 | Written Statement of Development and Use | |
| BLD-WF LLC 4-24-24 | | |
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| Print Owner's Name Owner's Signature Date | PROPERTY OWNER'S ENDORSEMENT OF APPLICATION | |
| | BLD-WF LLC 4-24- | -24 |
| Print Owner's Name Owner's Signature Date | BLD-WF LLC 4-24- | 24 Date |



Multi-Family Housing, East Main Street & Nichols Street, Bridgeport, CT

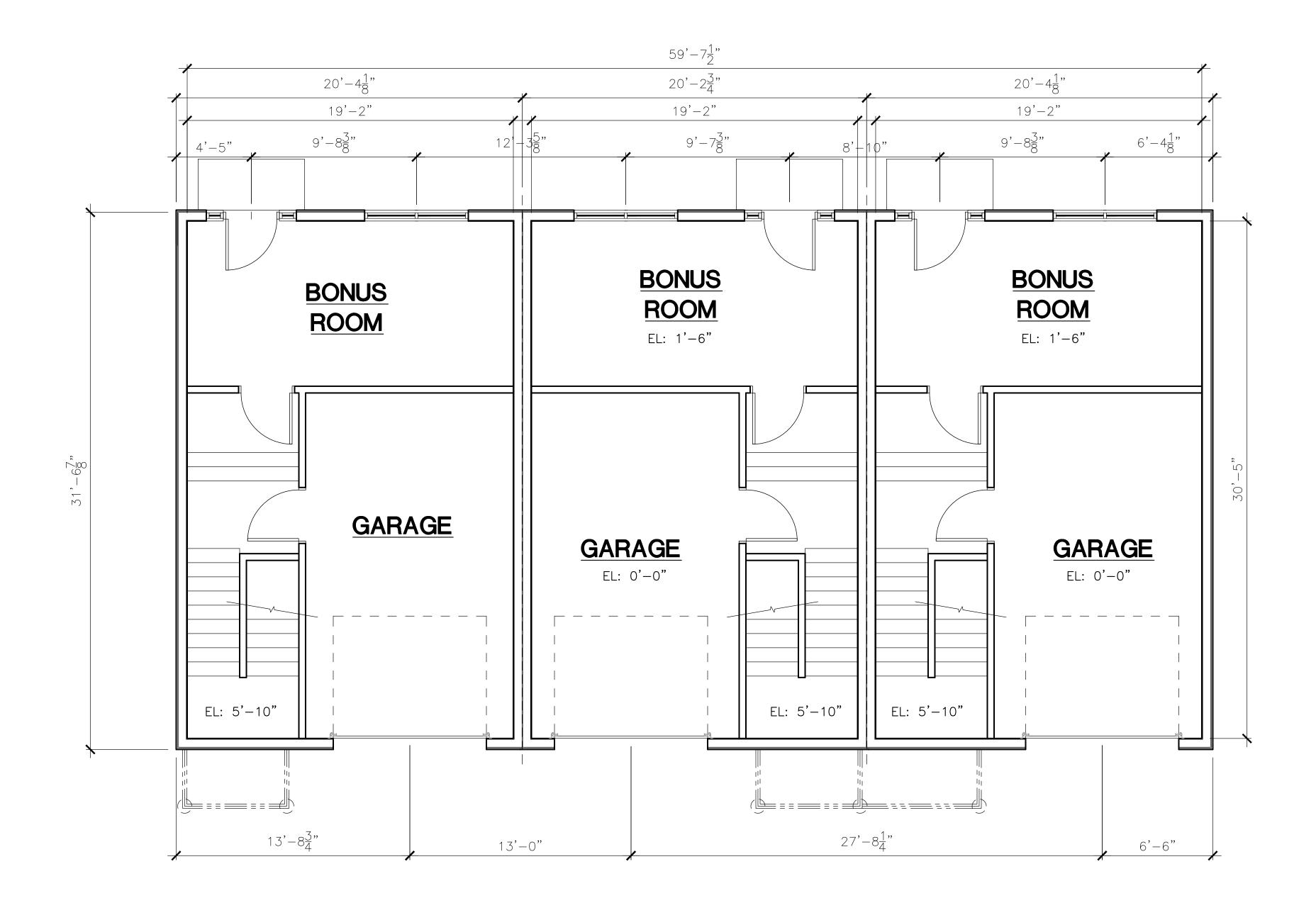
Project Overview:

The project site is located in two parcels one at 378 East Main Street and one at 371 East Main Street in Bridgeport, Connecticut.

The proposed project involves the sub-division of the 1.769Ac. properties into 29 building lots for two bedroom Row Houses with common access to parking in the rear of the buildings. The Row Houses will be clusted in six, five, four and three unit Row House buildings. Development will include buildings, driveways, utilities and parking area. Project requires approval for Municipal Coastal Site Plan Review.

Current application:

The current Zone is NX3 Mixed Residential 1 Zone and the Building Type being used for Zone is Row Building. The Row House units shall have an entry at street level a minimum of 18" above grade, an entrance in the rear and garage entry in the rear. Each Row House shall be two bedroom, two and one half baths with a one car garage and parking space behind garage. Each lot shall be serviced by electrical, water, gas & sewer. Due to 3.70.4 Item 2 requires that 85% of the street frontage be occupied by a building we require a waiver for two townhouses that have a driveway adjacent and two townhouses that have extra land at the corner of East Main Street & Nichols Street due to the irregular shape of the lot in this location.



GRADE LEVEL FLOOR PLAN SCALE: 1/4" = 1'-0"



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PROJECT TITLE

MULTI-FAMILY RESIDENTIAL DEVELOPMENT

NICHOLS AND EAST MAIN STREET BRIDGEPORT, CT

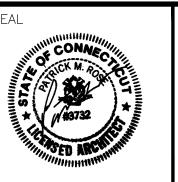
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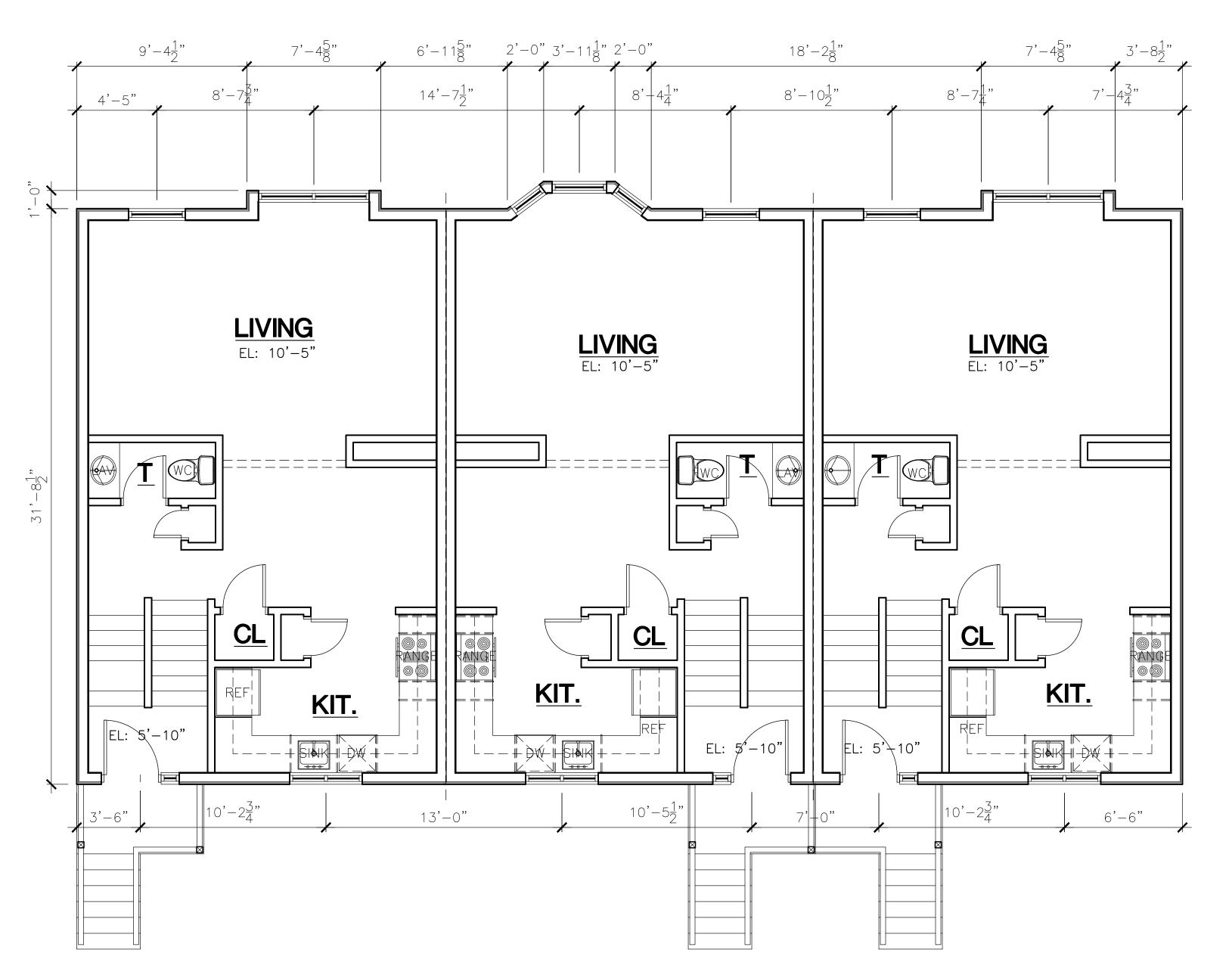
EATON ENTERPRISES, LLC

FLOOR PLAN
3 TOWNHOUSES

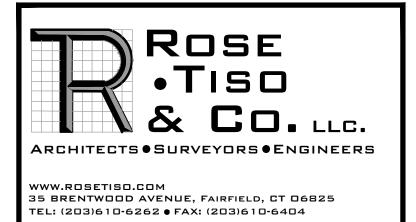
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FIRST FLOOR PLAN
SCALE: 1/4" = 1'-0"



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PROJECT TITLE

MULTI-FAMILY RESIDENTIAL DEVELOPMENT

NICHOLS AND EAST MAIN STREET BRIDGEPORT, CT

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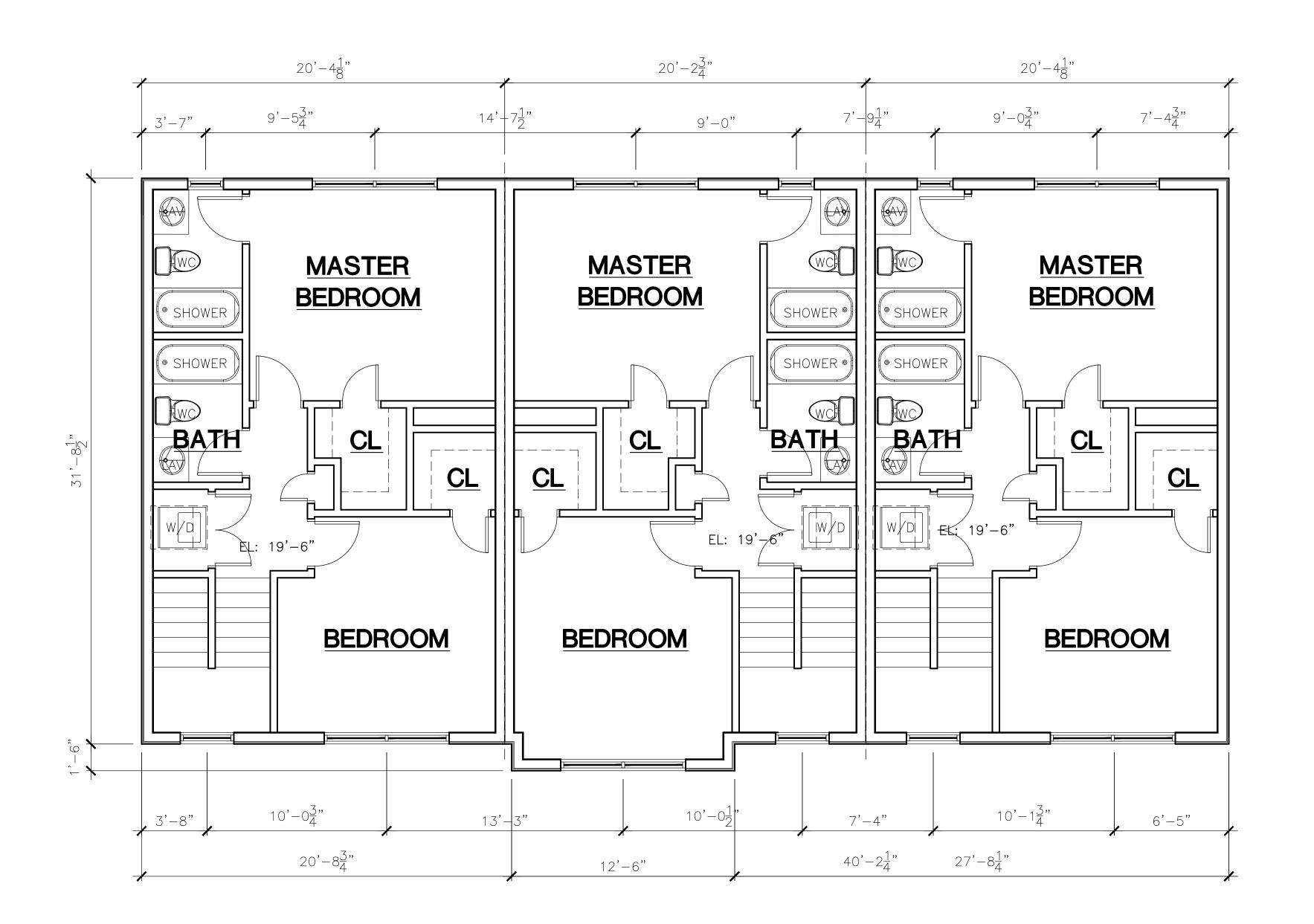
EATON ENTERPRISES, LLC

FLOOR PLAN
3 TOWNHOUSES

| | DESIGNED BY: KM | SCALE: AS NOTED |
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| | DRAWN BY: KM | DATE: 06.20.2023 |
| | CHECKED BY: PR | PROJECT NUMBER: 2772 |
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A-102



SECOND FLOOR PLAN SCALE: 1/4" = 1'-0"

| ROSE |
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| •TISO & CO. LLG. |
| ARCHITECTS • SURVEYORS • ENGINEERS |
| WWW.ROSETISO.COM 35 BRENTWOOD AVENUE, FAIRFIELD, CT 06825 TEL: (203)610-6262 • FAX: (203)610-6404 |

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PROJECT TITLE

MULTI-FAMILY RESIDENTIAL DEVELOPMENT

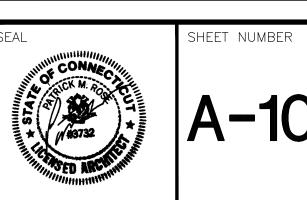
NICHOLS AND EAST MAIN STREET BRIDGEPORT, CT

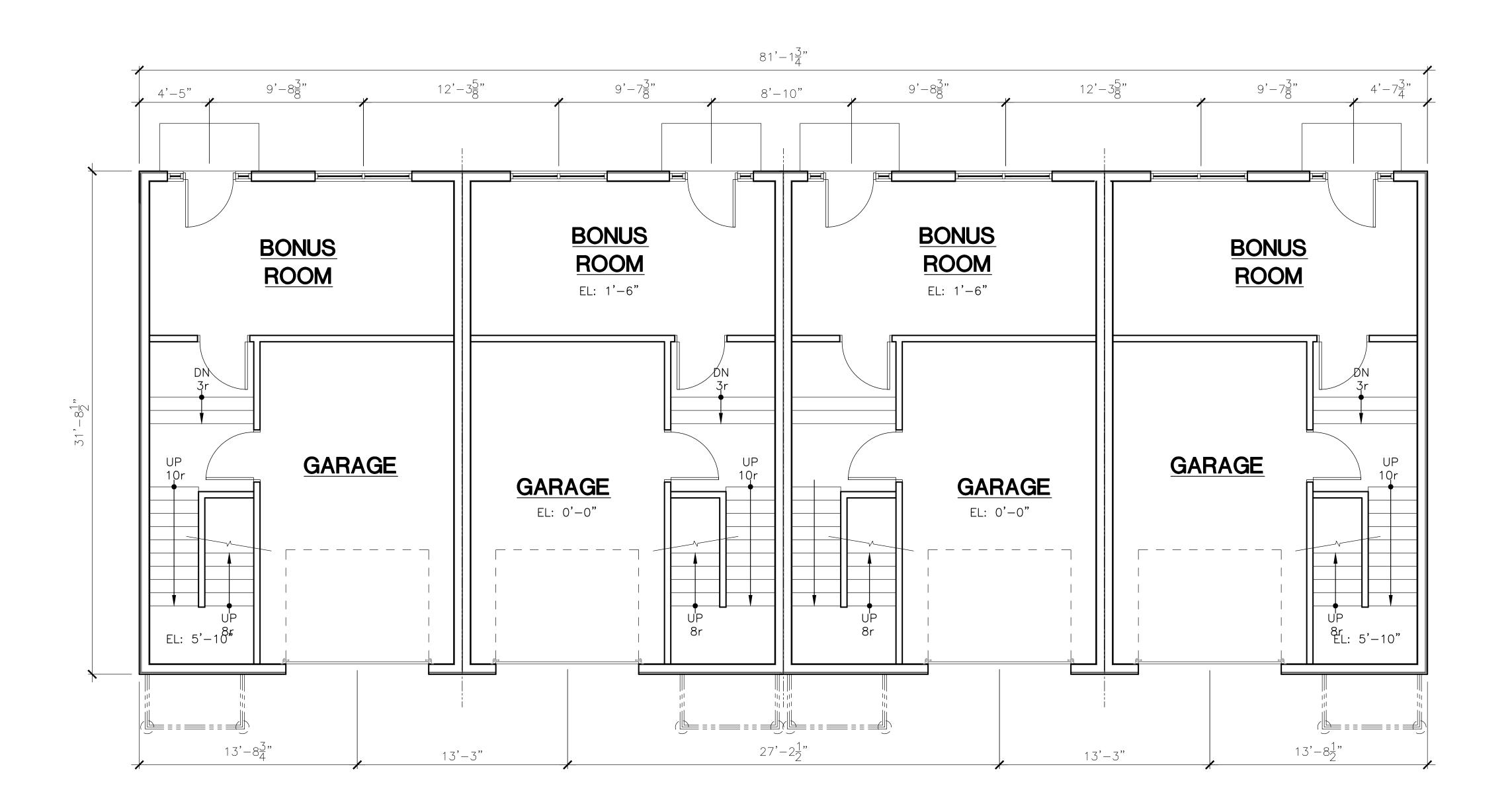
PREPARED FOR:

EATON ENTERPRISES, LLC

FLOOR PLAN
3 TOWNHOUSES

| DESIGNED BY: KM | SCALE: AS NOTED |
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| DRAWN BY: KM | DATE: 06.20.2023 |
| CHECKED BY: PR | PROJECT NUMBER: 2772 |
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GRADE LEVEL FLOOR PLAN
SCALE: 1/4" = 1'-0"



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PROJECT TITLE

MULTI-FAMILY RESIDENTIAL DEVELOPMENT

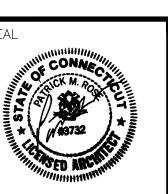
NICHOLS AND EAST MAIN STREET BRIDGEPORT, CT

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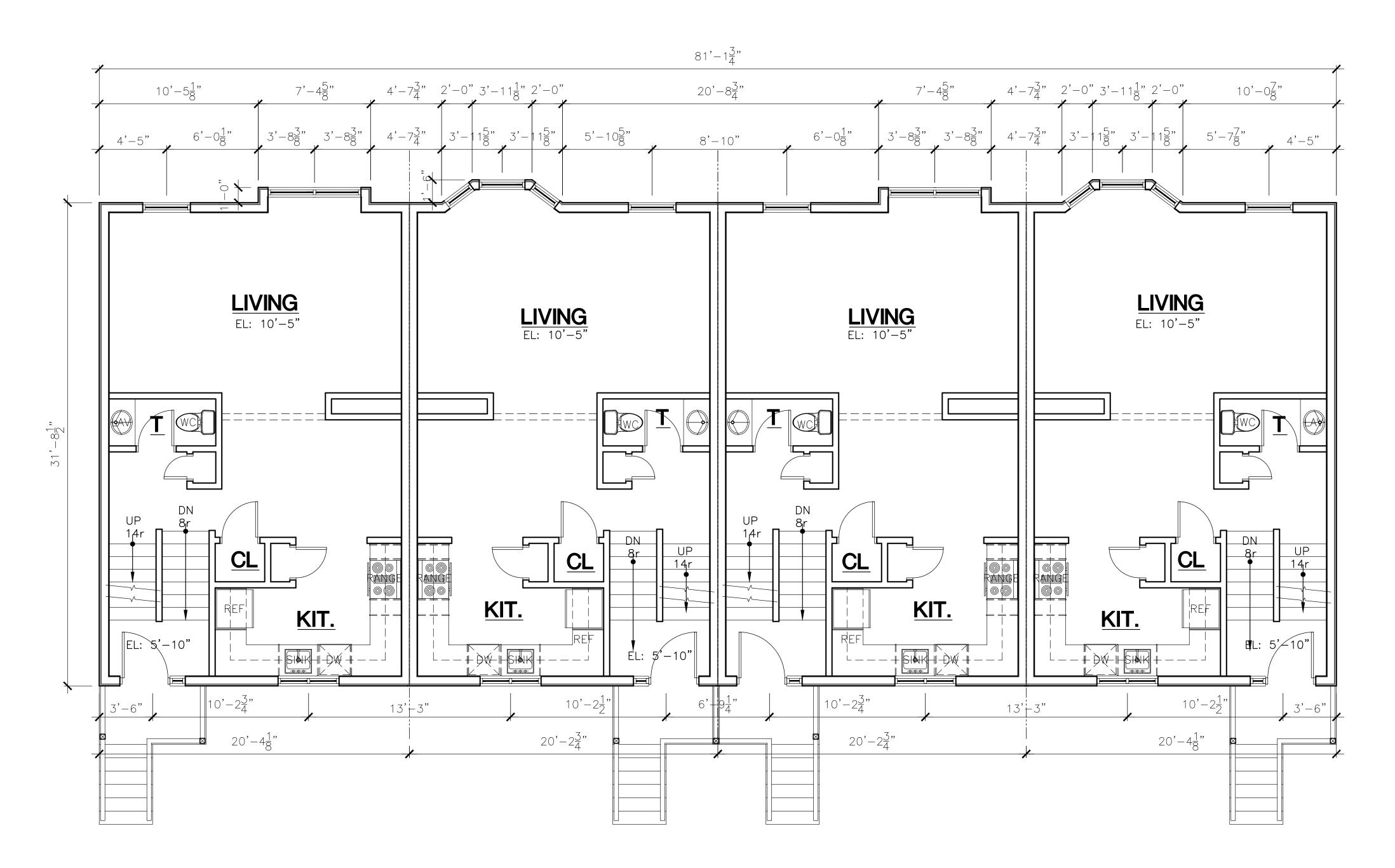
EATON ENTERPRISES, LLC

FLOOR PLAN
4 TOWNHOUSES

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| | CHECKED BY: PR | PROJECT NUMBER: 2772 |
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FIRST FLOOR PLAN
SCALE: 1/4" = 1'-0"



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PROJECT TITLE

MULTI-FAMILY RESIDENTIAL DEVELOPMENT

NICHOLS AND EAST MAIN STREET BRIDGEPORT, CT

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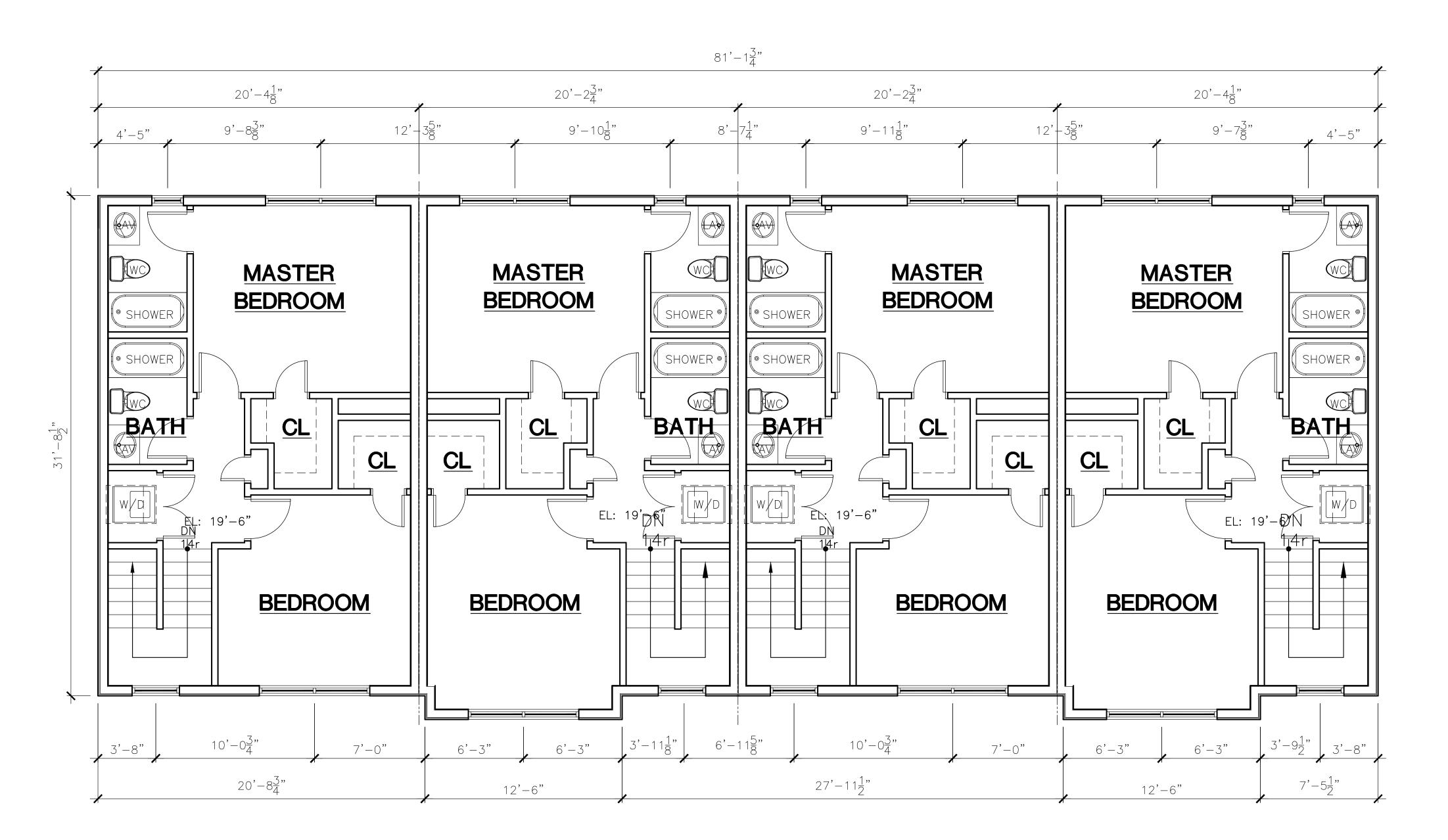
EATON ENTERPRISES, LLC

FLOOR PLAN
4 TOWNHOUSES

| | DESIGNED BY: KM | SCALE: AS NOTED |
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| | DRAWN BY: KM | DATE: 06.20.2023 |
| | CHECKED BY: PR | PROJECT NUMBER: 2772 |
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SECOND FLOOR PLAN SCALE: 1/4" = 1'-0"



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PROJECT TITLE

MULTI-FAMILY RESIDENTIAL DEVELOPMENT

NICHOLS AND EAST MAIN STREET BRIDGEPORT, CT

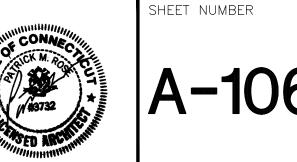
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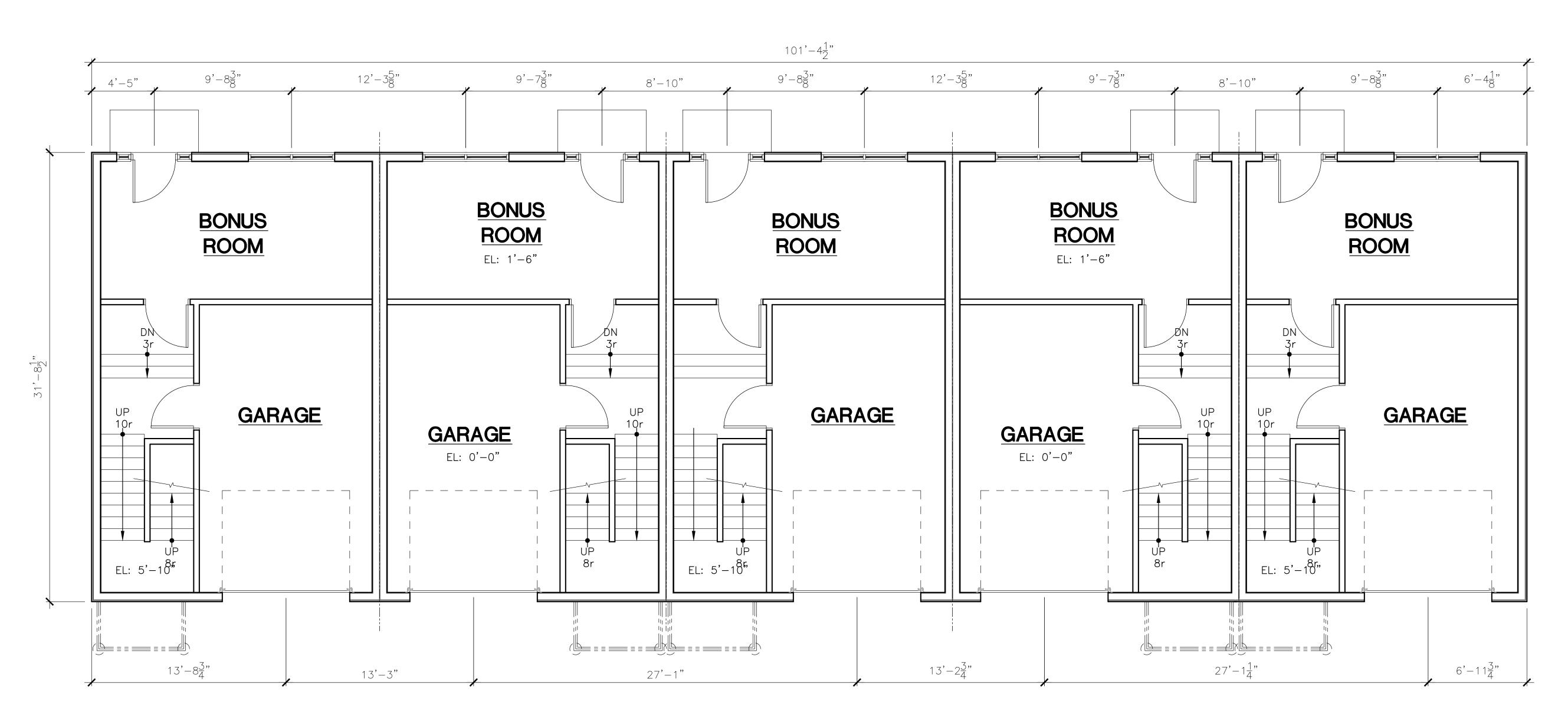
EATON ENTERPRISES, LLC

FLOOR PLAN
4 TOWNHOUSES

| DESIGNED BY: KM | SCALE: AS NOTED |
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GRADE LEVEL FLOOR PLAN SCALE: 1/4" = 1'-0"



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PROJECT TITLE

MULTI-FAMILY RESIDENTIAL DEVELOPMENT

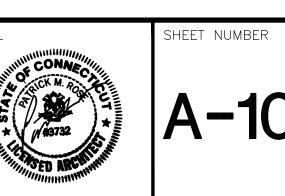
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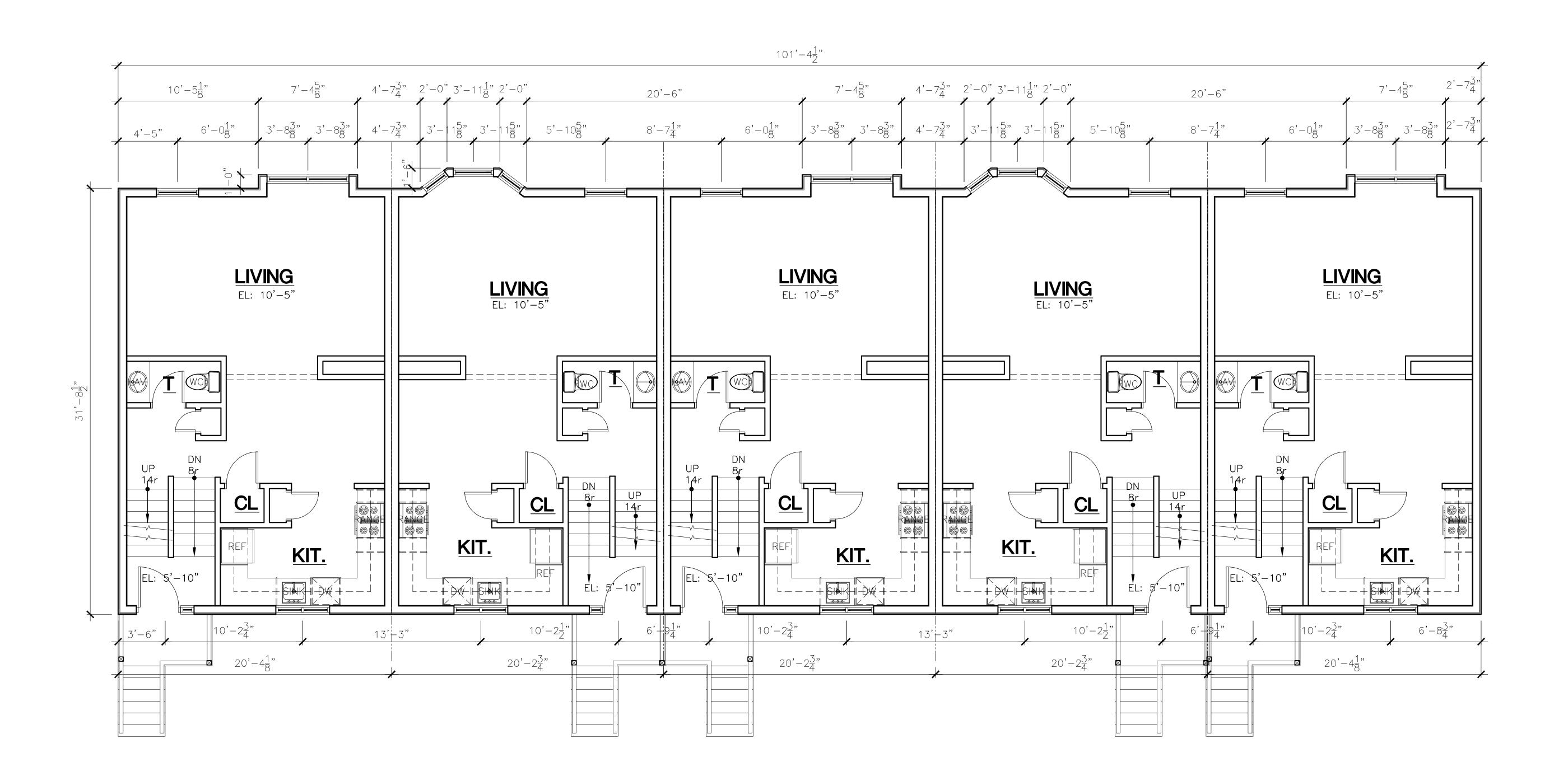
PREPARED FOR:

EATON ENTERPRISES, LLC

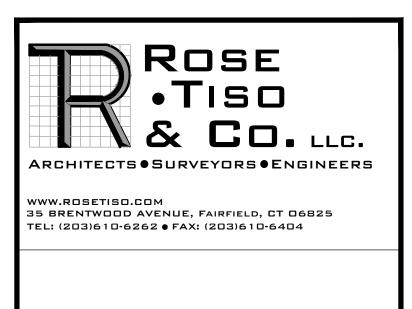
FLOOR PLAN
5 TOWNHOUSES

| DESIGNED BY: KM | SCALE: AS NOTED |
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| DRAWN BY: KM | DATE: 06.20.2023 |
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FIRST FLOOR PLAN
SCALE: 1/4" = 1'-0"



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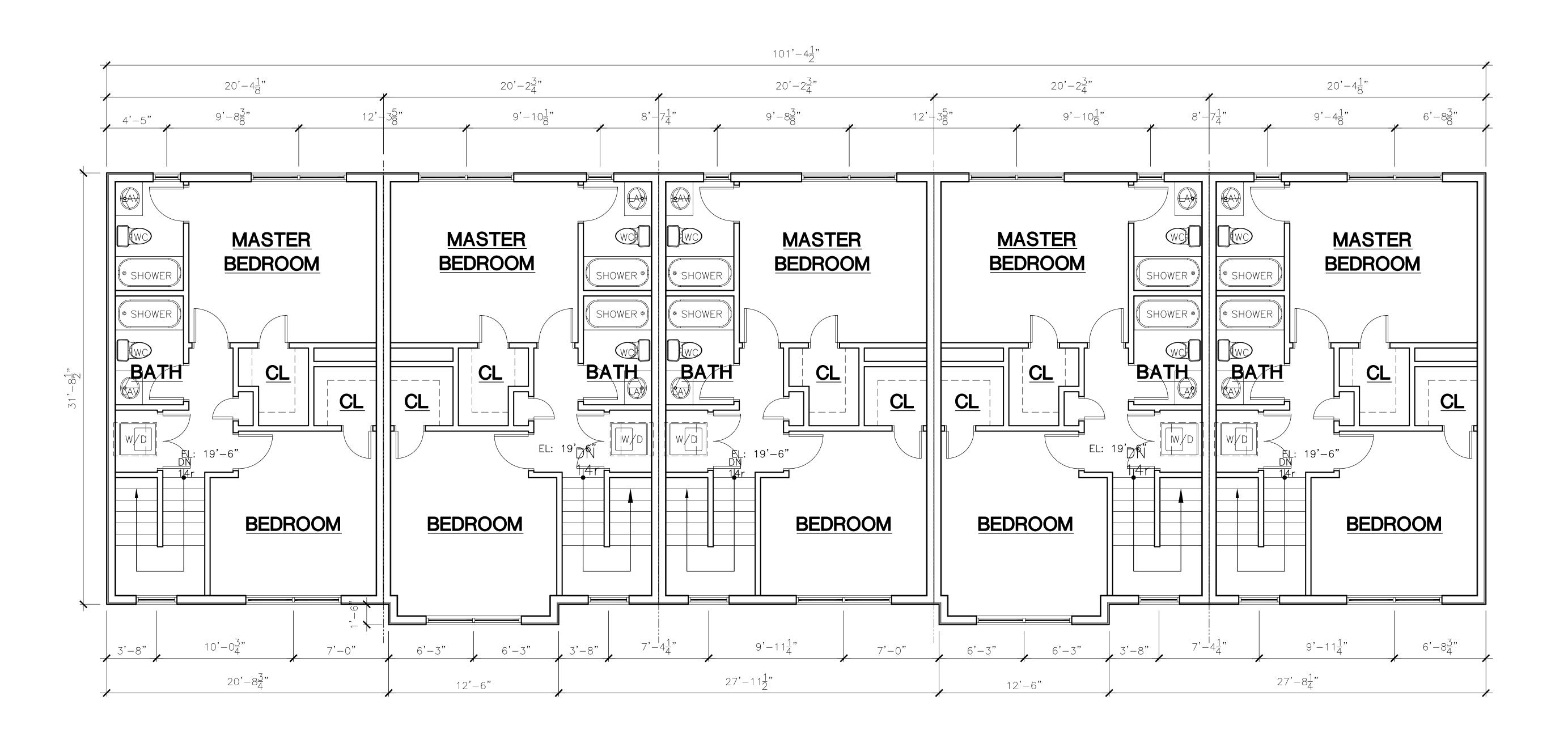
EATON ENTERPRISES, LLC

FLOOR PLAN
5 TOWNHOUSES

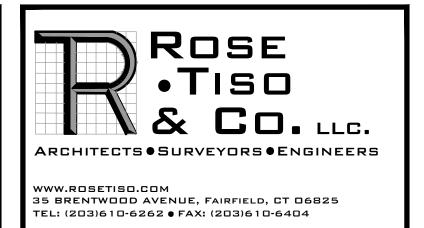
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SECOND FLOOR PLAN SCALE: 1/4" = 1'-0"



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PROJECT TITLE

MULTI-FAMILY RESIDENTIAL DEVELOPMENT

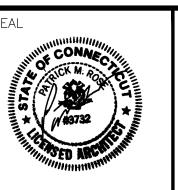
NICHOLS AND EAST MAIN STREET BRIDGEPORT, CT

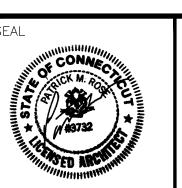
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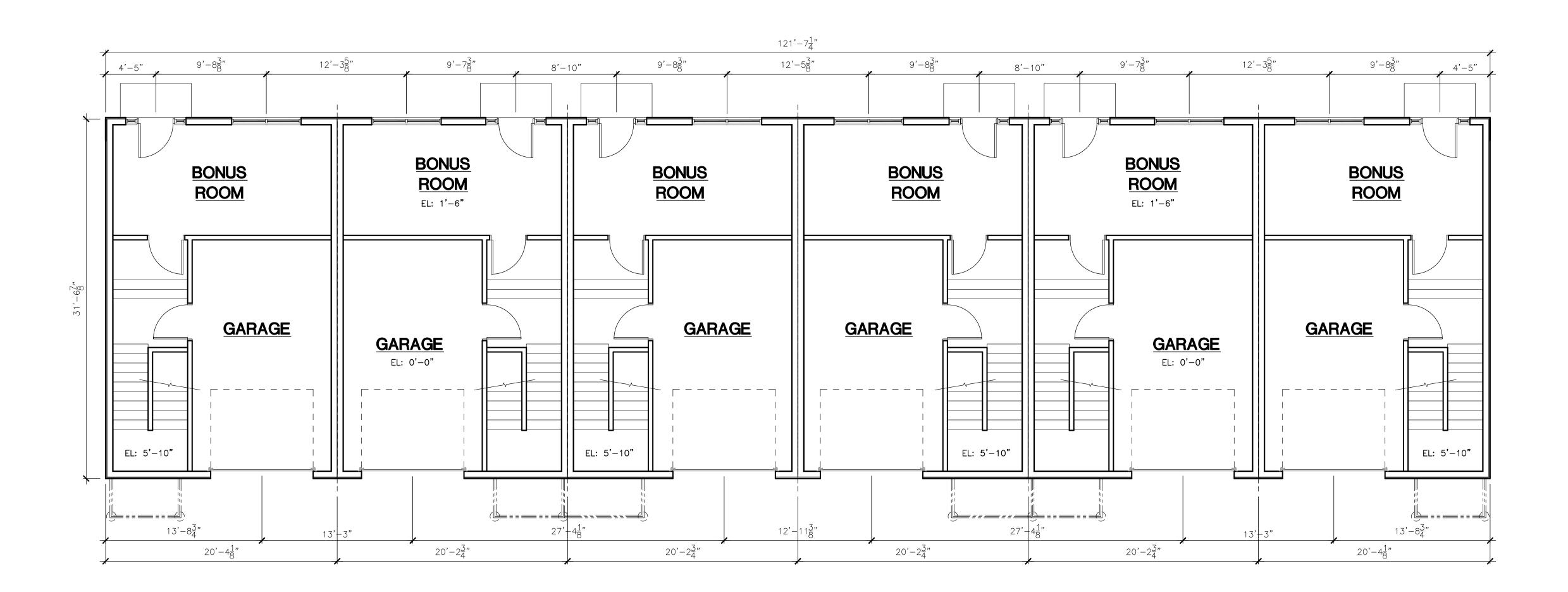
EATON ENTERPRISES, LLC

FLOOR PLAN
5 TOWNHOUSES

| ı | DESIGNED BY: KM | SCALE: AS NOTED |
|---|--|--------------------------------|
| | DRAWN BY: KM | DATE: 06.20.2023 |
| | CHECKED BY: PR | PROJECT NUMBER: 2772 |
| | CAD FILE: R:/2772/ARCH/A —10 | D1.DWG |







GRADE LEVEL FLOOR PLAN SCALE: 3/16" = 1'-0"



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PROJECT TITLE

MULTI-FAMILY RESIDENTIAL DEVELOPMENT

NICHOLS AND EAST MAIN STREET BRIDGEPORT, CT

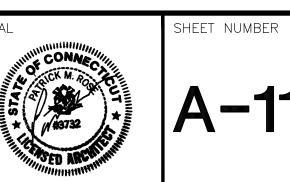
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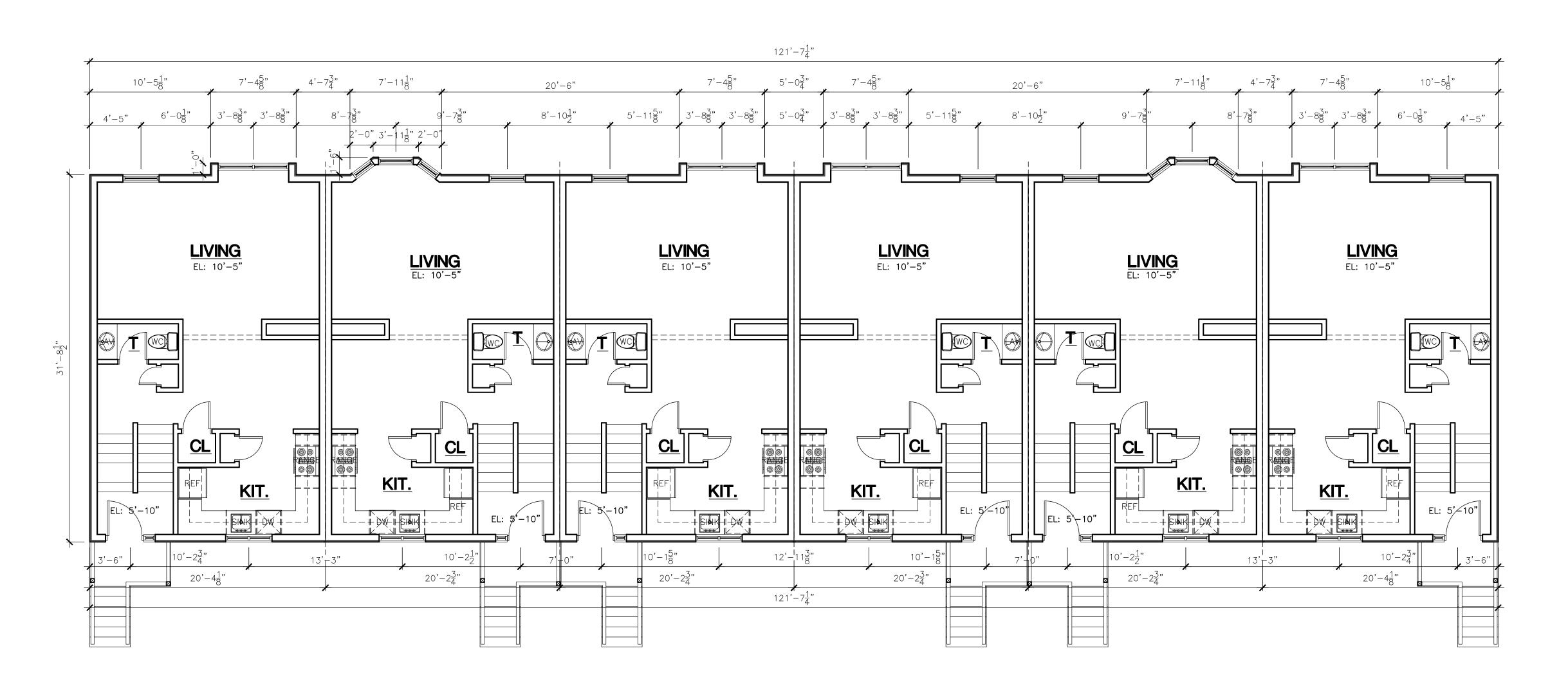
EATON ENTERPRISES, LLC

FLOOR PLAN 6 TOWNHOUSES

| | DESIGNED BY: KM | SCALE: AS NOTED |
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| | DRAWN BY: KM | DATE: 06.20.2023 |
| | CHECKED BY: PR | PROJECT NUMBER: 2772 |
| | CAD File: R:/2772/arch/a-1 0 | D1.DWG |







FIRST FLOOR PLAN
SCALE: 3/16" = 1'-0"

| ROSE •TISO & CO. LLC. |
|---|
| ARCHITECTS • SURVEYORS • ENGINEERS |
| |
| WWW.ROSETISO.COM |
| 35 BRENTWOOD AVENUE, FAIRFIELD, CT 06825 TEL: (203)610-6262 ● FAX: (203)610-6404 |
| 122. (200)010 0202 #1 AX. (200)010-0404 |

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PROJECT TITLE

MULTI-FAMILY RESIDENTIAL DEVELOPMENT

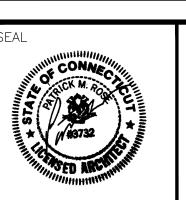
NICHOLS AND EAST MAIN STREET BRIDGEPORT, CT

PREPARED FOR:

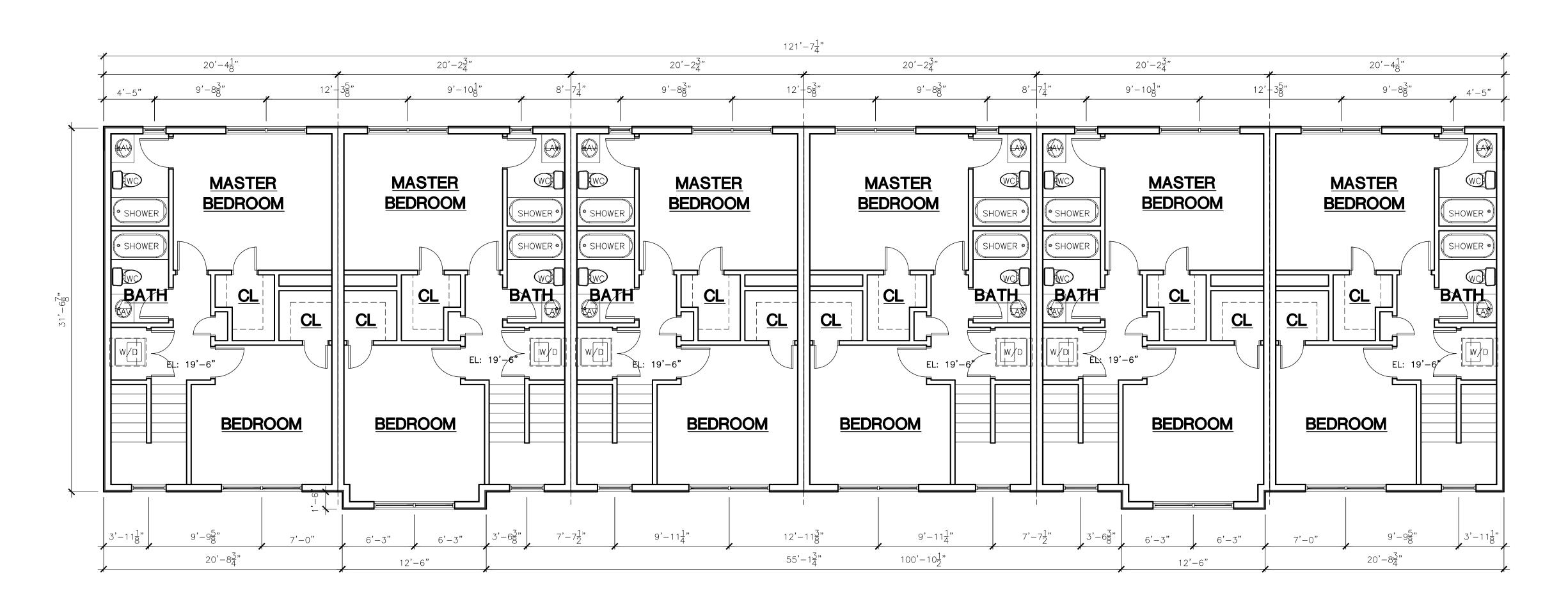
EATON ENTERPRISES, LLC

FLOOR PLAN
6 TOWNHOUSES

| | | DESIGNED BY: KM | SCALE: AS NOTED |
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| | | DRAWN BY: KM | DATE: 06.20.2023 |
| | | CHECKED BY: PR | PROJECT NUMBER: 2772 |
| | CAD File: R:/2772/arch/a-1 0 | D1.DWG | |



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SECOND FLOOR PLAN SCALE: 3/16" = 1'-0"



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MULTI-FAMILY RESIDENTIAL DEVELOPMENT

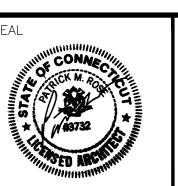
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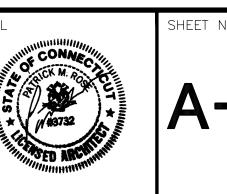
EATON ENTERPRISES, LLC

PREPARED FOR:

FLOOR PLAN 6 TOWNHOUSES

| | | DESIGNED BY: KM | SCALE: AS NOTED |
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| | | DRAWN BY: KM | DATE: 06.20.2023 |
| | | CHECKED BY: PR | PROJECT NUMBER: 2772 |
| | CAD File: R:/2772/arch/a-1 0 | D1.DWG | |







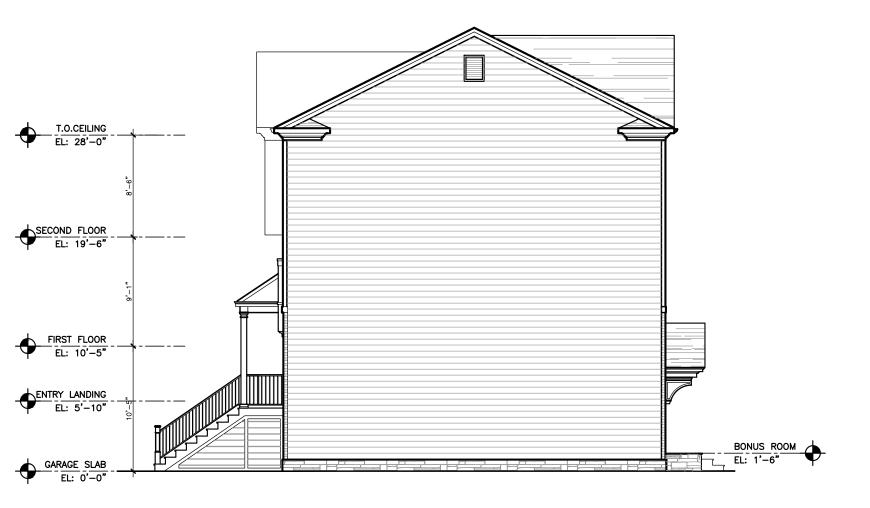
FRONT ELEVATION
SCALE: 1/8" = 1'-0"



REAR ELEVATION
SCALE: 1/8" = 1'-0"



RIGHT ELEVATION
SCALE: 1/8" = 1'-0"



LEFT ELEVATION
SCALE: 1/8" = 1'-0"



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MULTI-FAMILY RESIDENTIAL DEVELOPMENT

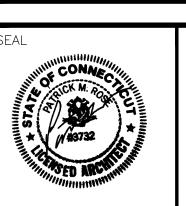
NICHOLS AND EAST MAIN STREET BRIDGEPORT, CT

PREPARED FOR:

EATON ENTERPRISES, LLC

ELEVATIONS
3 TOWNHOUSES

| | DESIGNED BY: KM | SCALE: AS NOTED |
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| | DRAWN BY: KM | DATE: 06.20.2023 |
| | CHECKED BY: PR | PROJECT NUMBER: 2772 |
| | CAD FILE: R:/2772/ARCH/200 S | SERIES.DWG |





FRONT ELEVATION

SCALE: 1/8" = 1'-0"



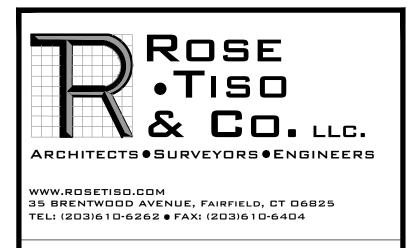
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SCALE: 1/8" = 1'-0"



RIGHT ELEVATION
SCALE: 1/8" = 1'-0"



LEFT ELEVATION
SCALE: 1/8" = 1'-0"



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PROJECT TITLE

MULTI-FAMILY RESIDENTIAL DEVELOPMENT

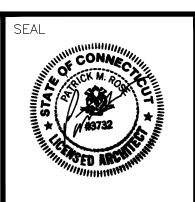
NICHOLS AND EAST MAIN STREET BRIDGEPORT, CT

PREPARED FOR:

EATON ENTERPRISES, LLC

ELEVATIONS
4 TOWNHOUSES

| l | DESIGNED BY: KM | SCALE: AS NOTED |
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| | DRAWN BY: KM | DATE: 06.20.2023 |
| | CHECKED BY: PR | PROJECT NUMBER: 2772 |
| | CAD FILE: R:/2772/ARCH/200 S | SERIES.DWG |



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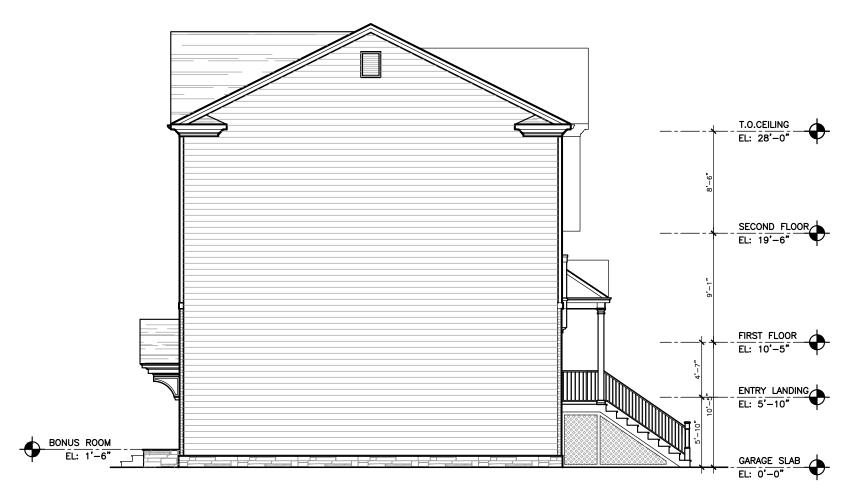


FRONT ELEVATION

SCALE: 1/8" = 1'-0"



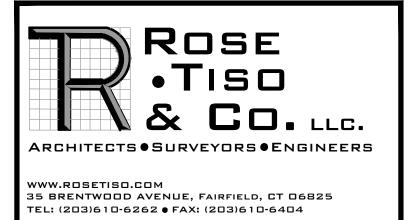
REAR ELEVATION
SCALE: 1/8" = 1'-0"



RIGHT ELEVATION
SCALE: 1/8" = 1'-0"



LEFT ELEVATION
SCALE: 1/8" = 1'-0"



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PROJECT TITLE

MULTI-FAMILY RESIDENTIAL DEVELOPMENT

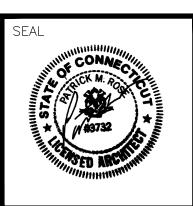
NICHOLS AND EAST MAIN STREET BRIDGEPORT, CT

PREPARED FOR:

EATON ENTERPRISES, LLC

ELEVATIONS
5 TOWNHOUSES

| | DESIGNED BY: KM | SCALE: AS NOTED |
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| | DRAWN BY: KM | DATE: 06.20.2023 |
| | CHECKED BY: PR | PROJECT NUMBER: 2772 |
| | CAD FILE: R:/2772/ARCH/200 S | SERIES.DWG |



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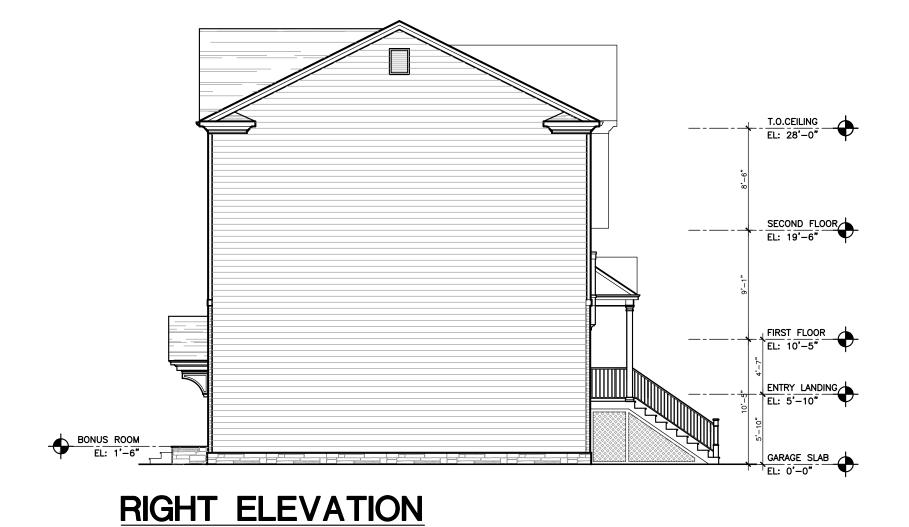
FRONT ELEVATION

SCALE: 1/8" = 1'-0"



REAR ELEVATION
SCALE: 1/8" = 1'-0"

SCALE: 1/8" = 1'-0"







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PROJECT TITLE

MULTI-FAMILY RESIDENTIAL DEVELOPMENT

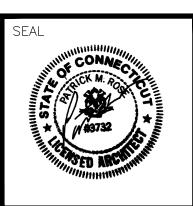
NICHOLS AND EAST MAIN STREET BRIDGEPORT, CT

PREPARED FOR:

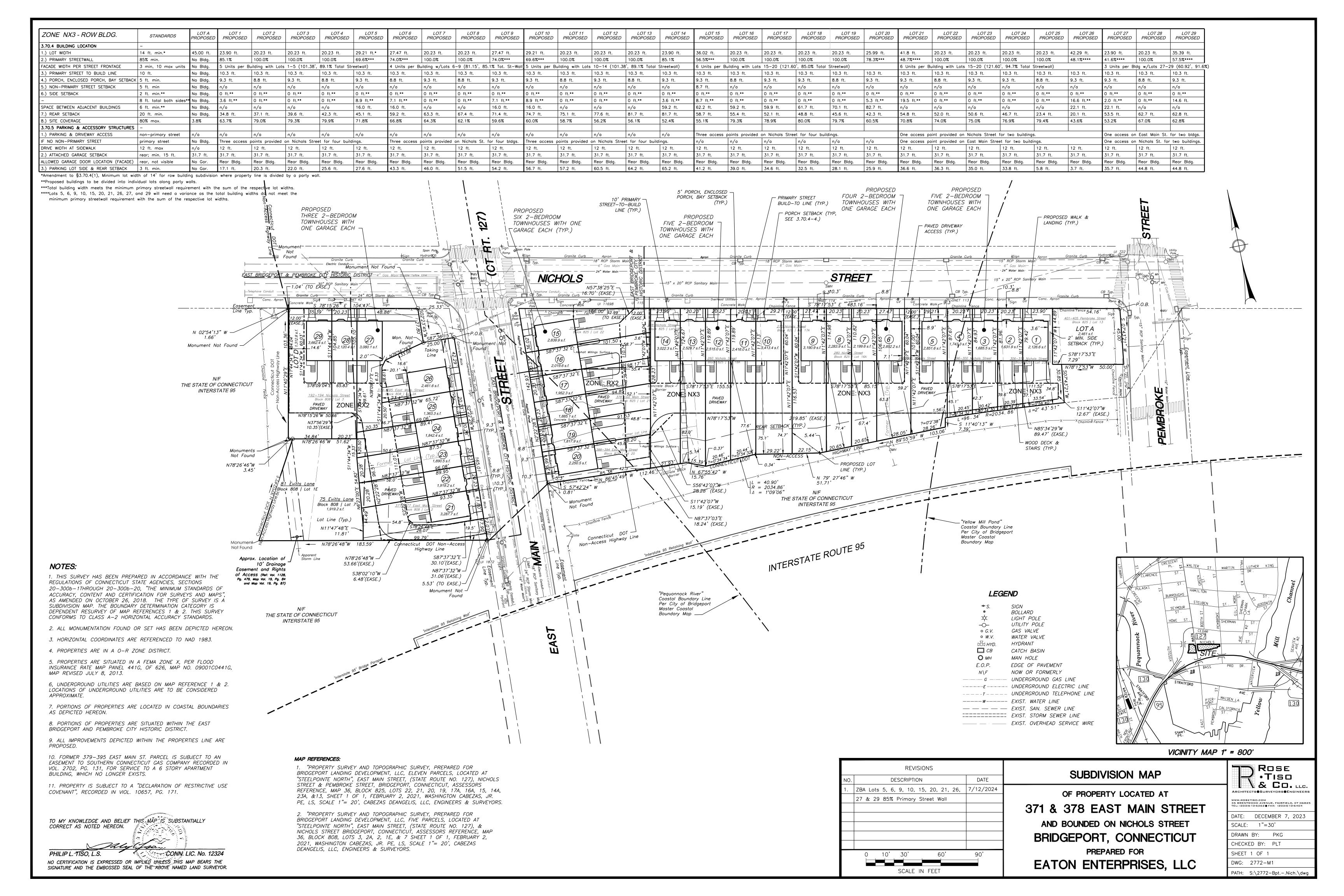
EATON ENTERPRISES, LLC

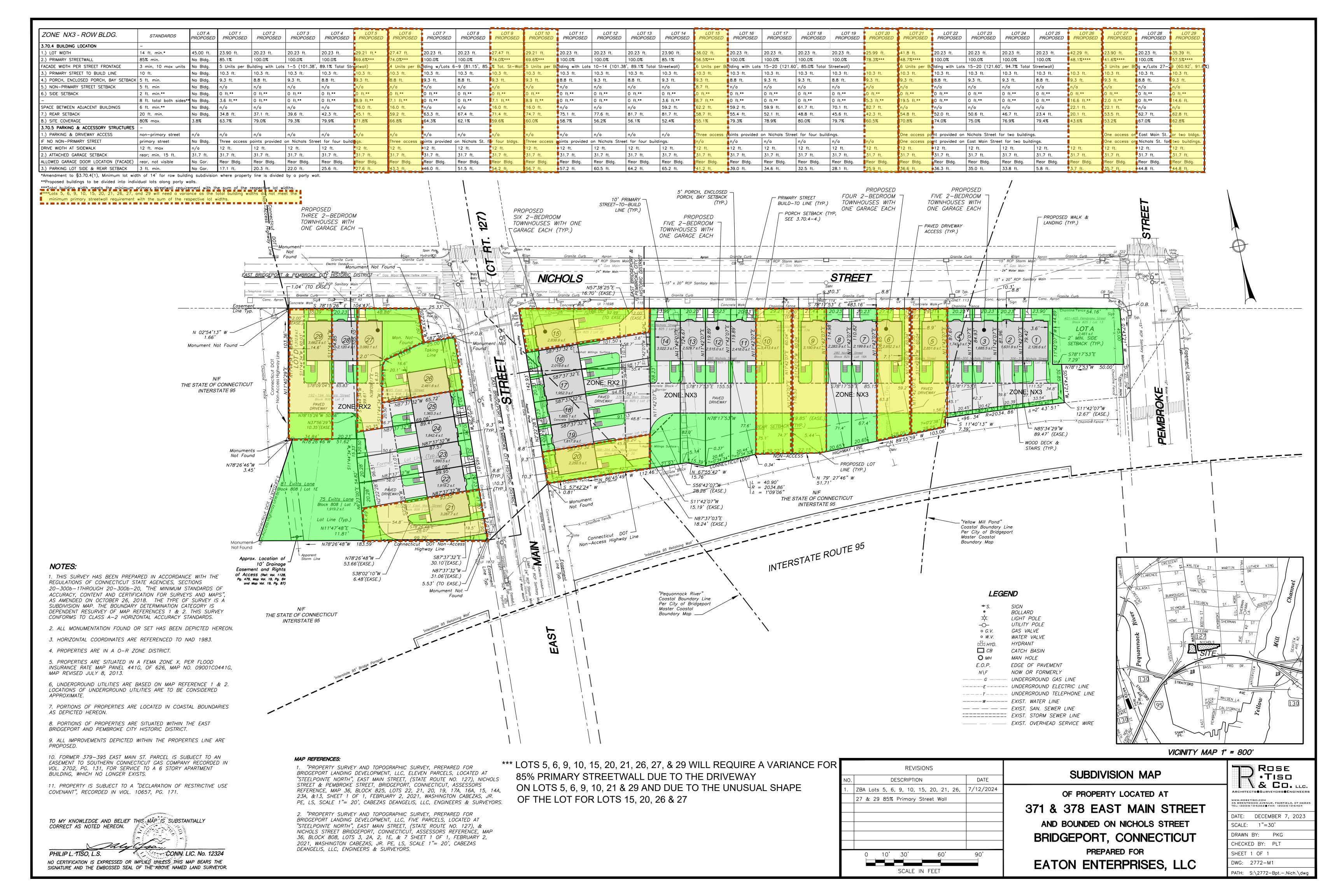
ELEVATIONS
6 TOWNHOUSES

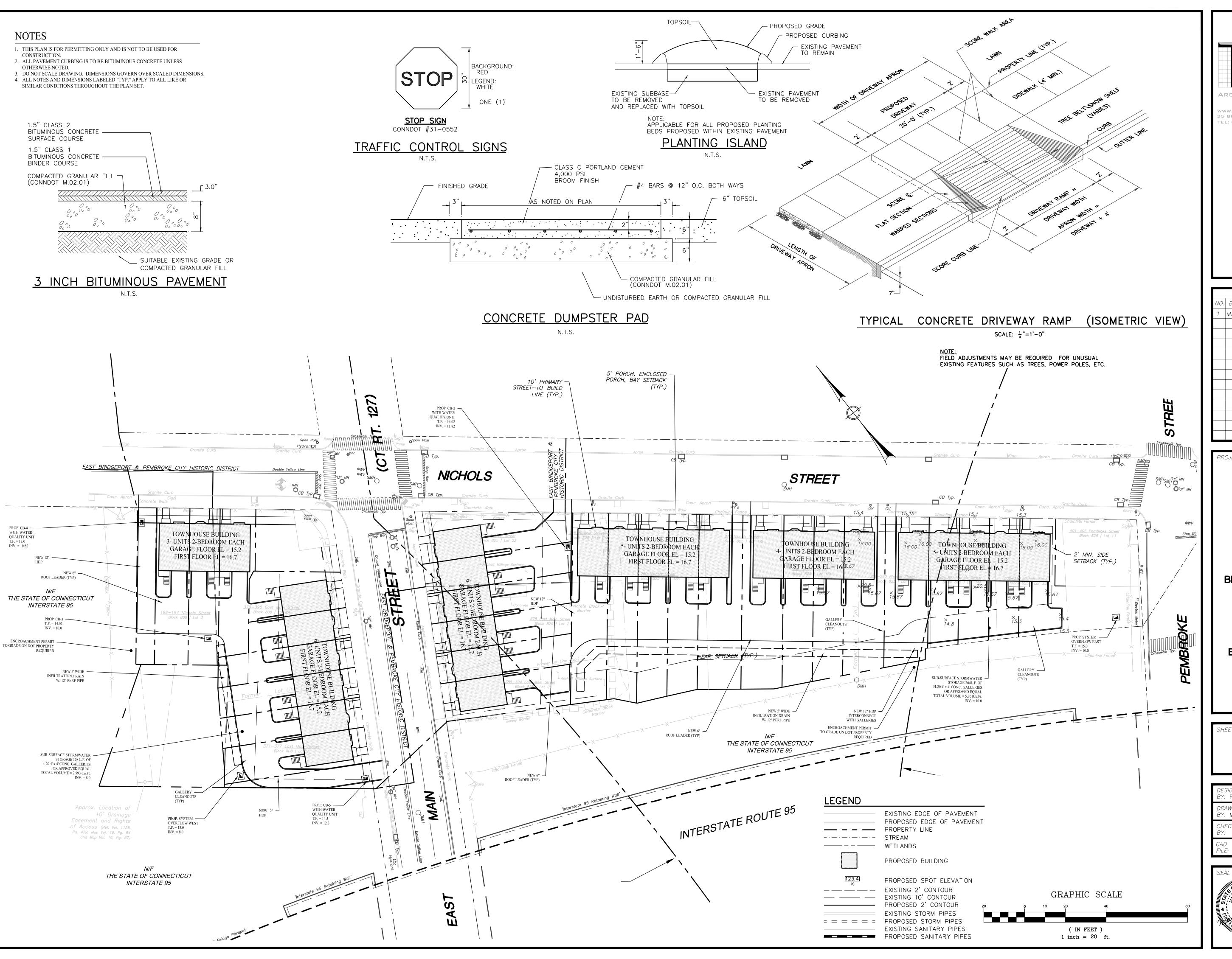
| DESIGNED BY: KM | SCALE: AS NOTED |
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| DRAWN BY: KM | DATE: 06.20.2023 |
| CHECKED BY: PR | PROJECT NUMBER: 2772 |
| CAD FILE: R:/2772/ARCH/200SERIES.DWG | |



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PROPOSED TOWNHOUSES

371 & 378 EAST MAIN STREET BRIDGEPORT, CONNECTICUT

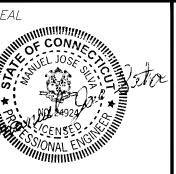
Prepared For:

EATON ENTERPRISES, LLC

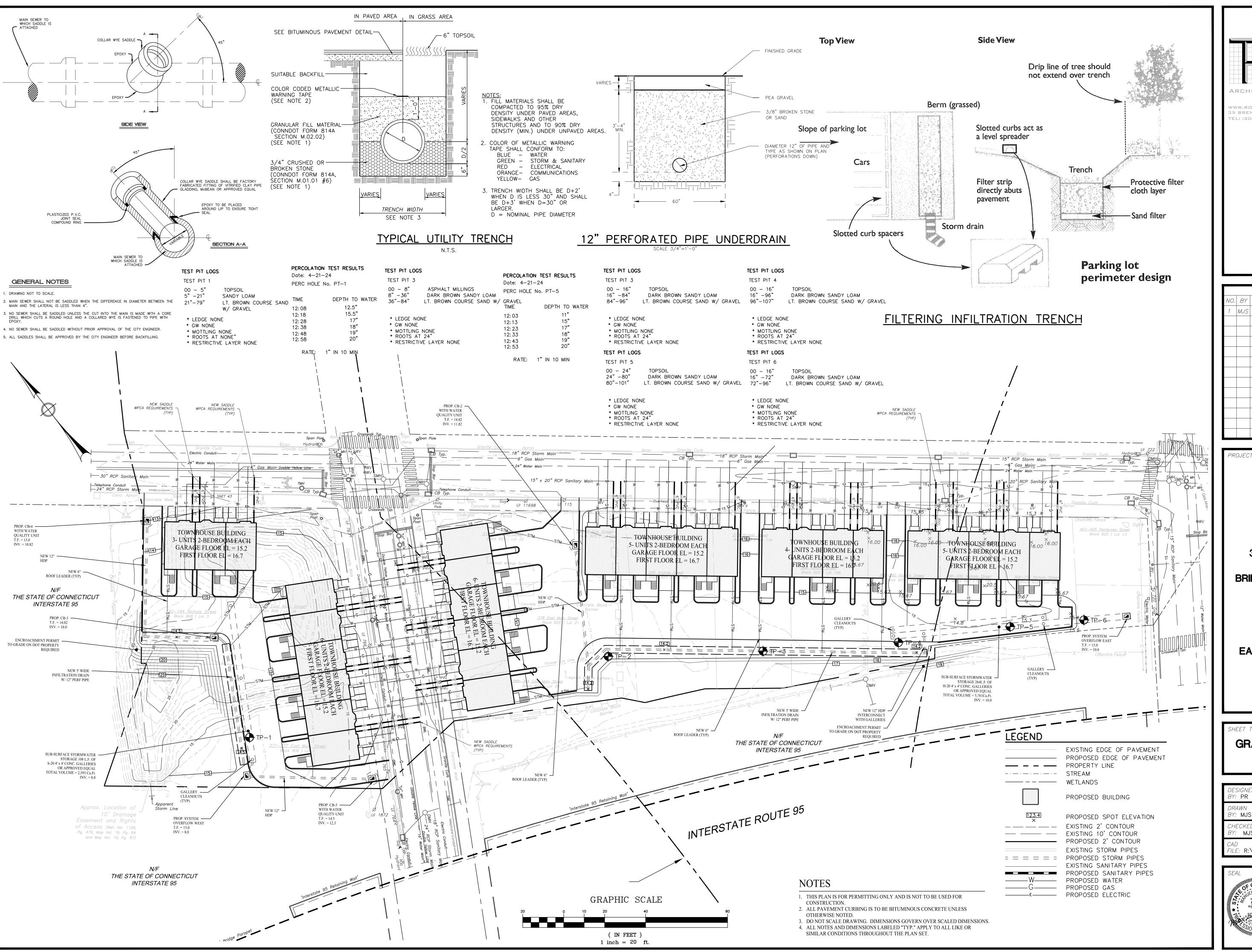
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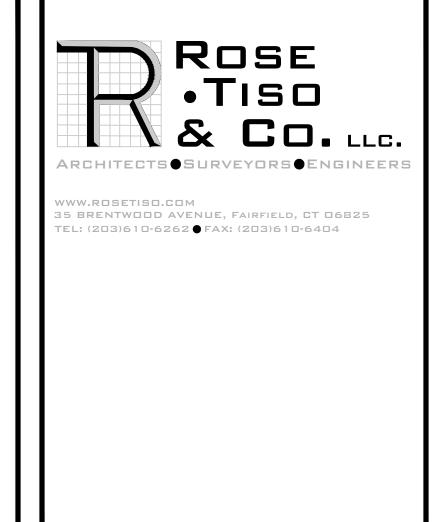
SITE PLAN

| DESIGNED BY: PR | SCALE: 1"=20' |
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| DRAWN BY: M JS | DATE: 05-01-24 |
| CHECKED BY: MJS | PROJECT NUMBER: 2772 |
| <i>CAD</i> <i>FILE:</i> R:\2772\DWG | |









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PROPOSED TOWNHOUSES

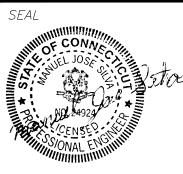
371 & 378 EAST MAIN STREET BRIDGEPORT, CONNECTICUT

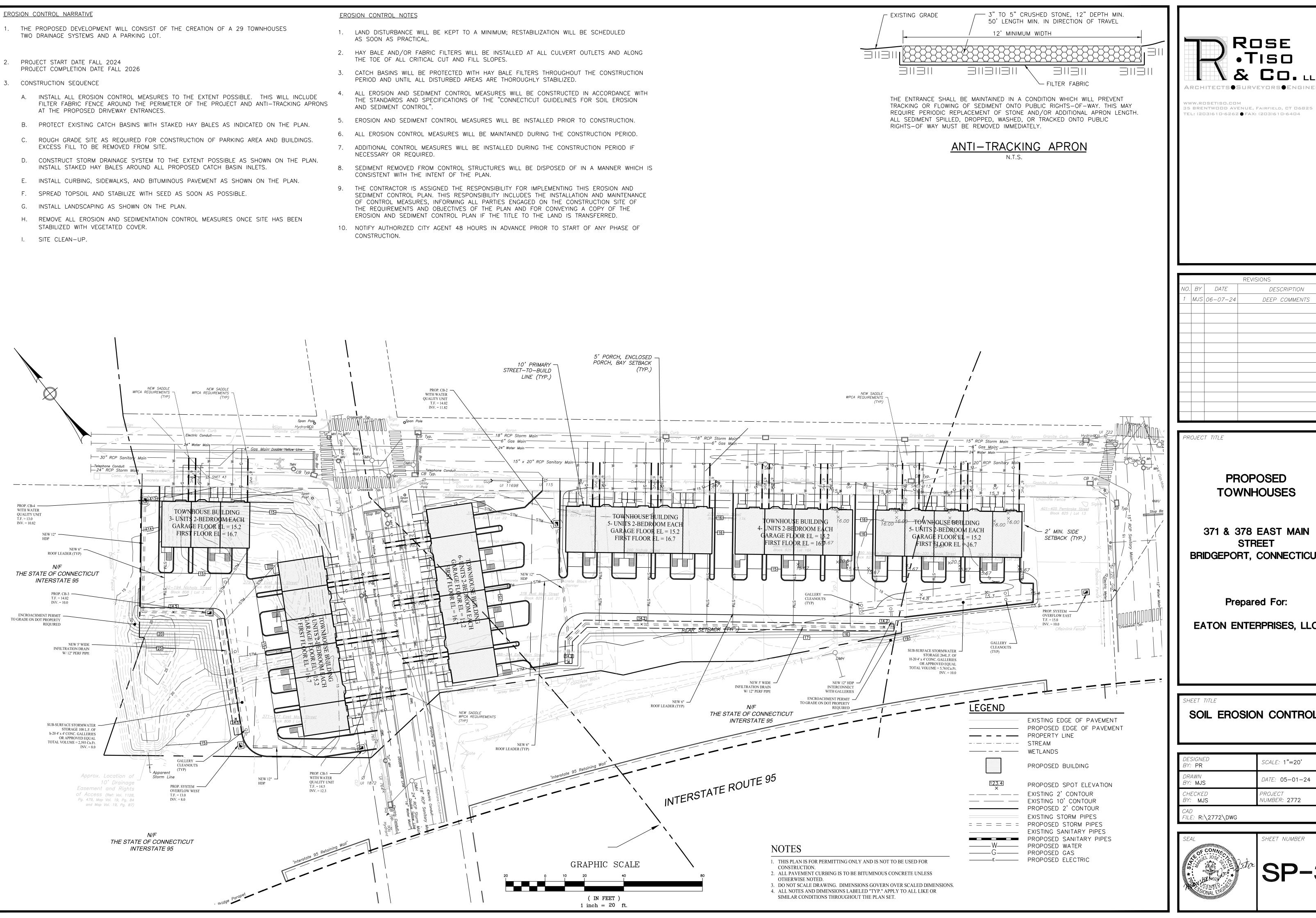
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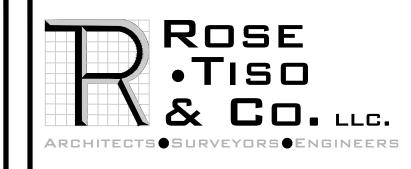
EATON ENTERPRISES, LLC

GRADING & UTILITY PLAN

| ı | DESIGNED BY: PR | SCALE: 1"=20' |
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| ı | DRAWN BY: M JS | DATE: 05-01-24 |
| ı | CHECKED BY: MJS | PROJECT NUMBER: 2772 |
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PROPOSED TOWNHOUSES

371 & 378 EAST MAIN STREET BRIDGEPORT, CONNECTICUT

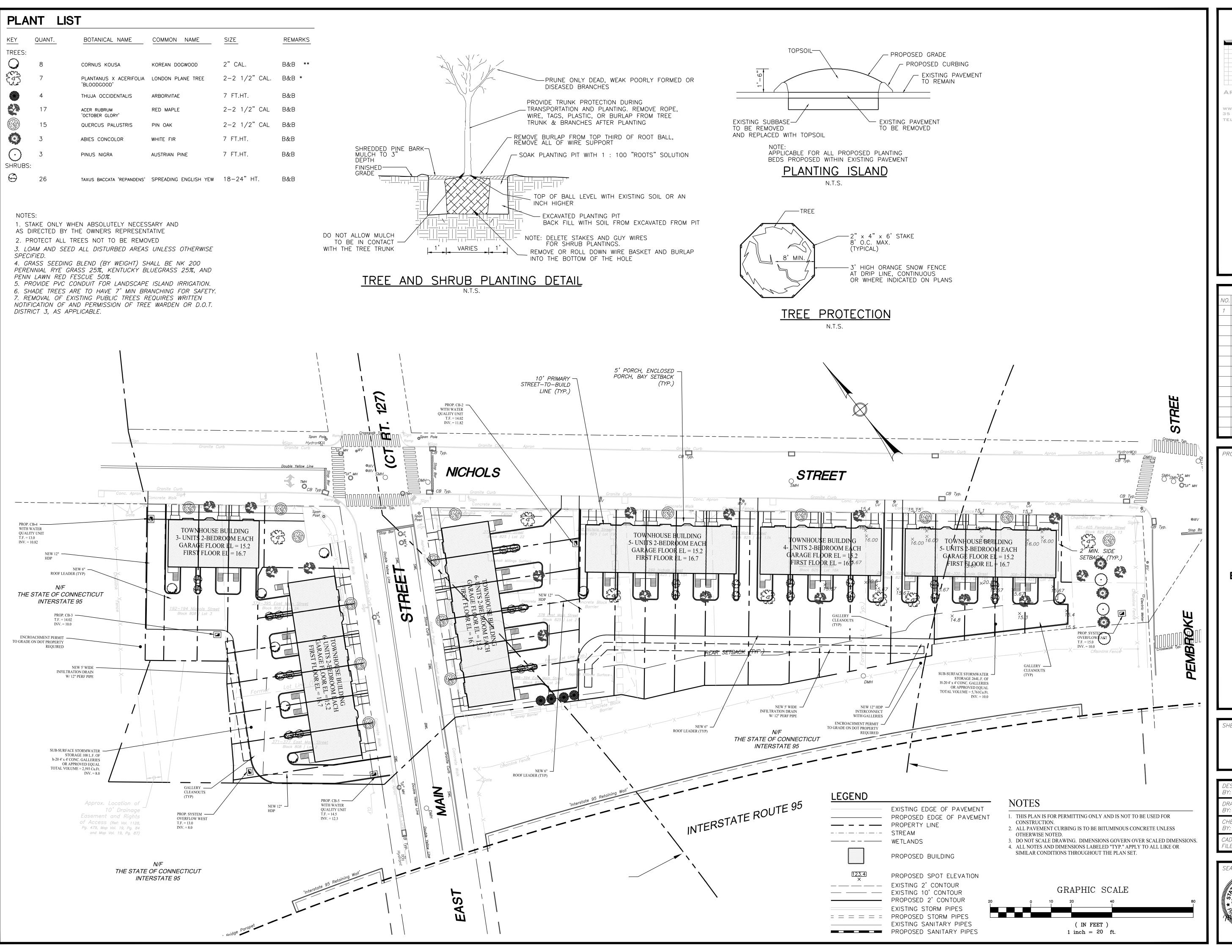
Prepared For:

EATON ENTERPRISES, LLC

SOIL EROSION CONTROL

| DESIGNED BY: PR | SCALE: 1"=20' |
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| DRAWN BY: M JS | DATE: 05-01-24 |
| CHECKED BY: MJS | PROJECT NUMBER: 2772 |
| <i>CAD</i> <i>FILE:</i> R:\2772\DWG | |







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PROPOSED TOWNHOUSES

371 & 378 EAST MAIN STREET BRIDGEPORT, CONNECTICUT

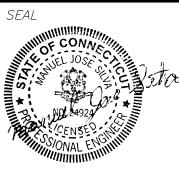
Prepared For:

EATON ENTERPRISES, LLC

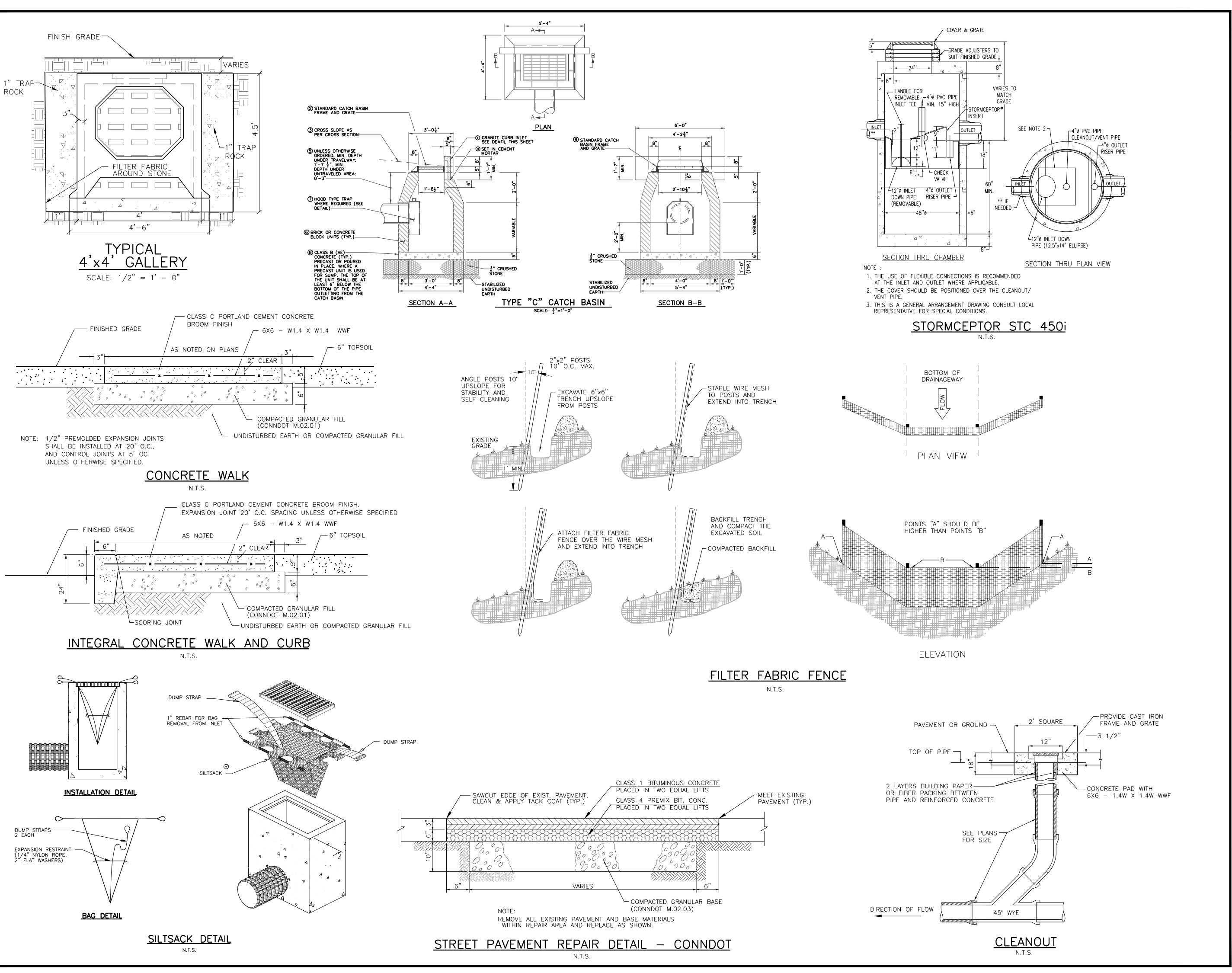
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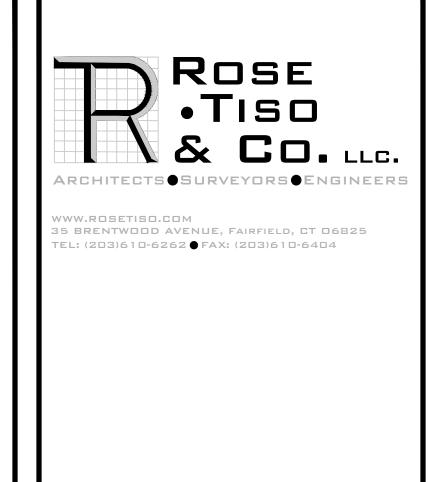
LANDSCAPE PLAN

| DESIGNED BY: PR | SCALE: 1"=20' |
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| DRAWN BY: MJS | DATE: 05-01-24 |
| CHECKED BY: MJS | PROJECT NUMBER: 2772 |
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SP-4





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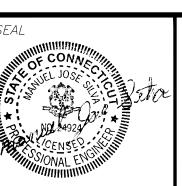
PROPOSED TOWNHOUSES

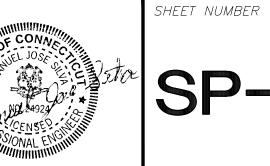
371 & 378 EAST MAIN STREET BRIDGEPORT, CONNECTICUT

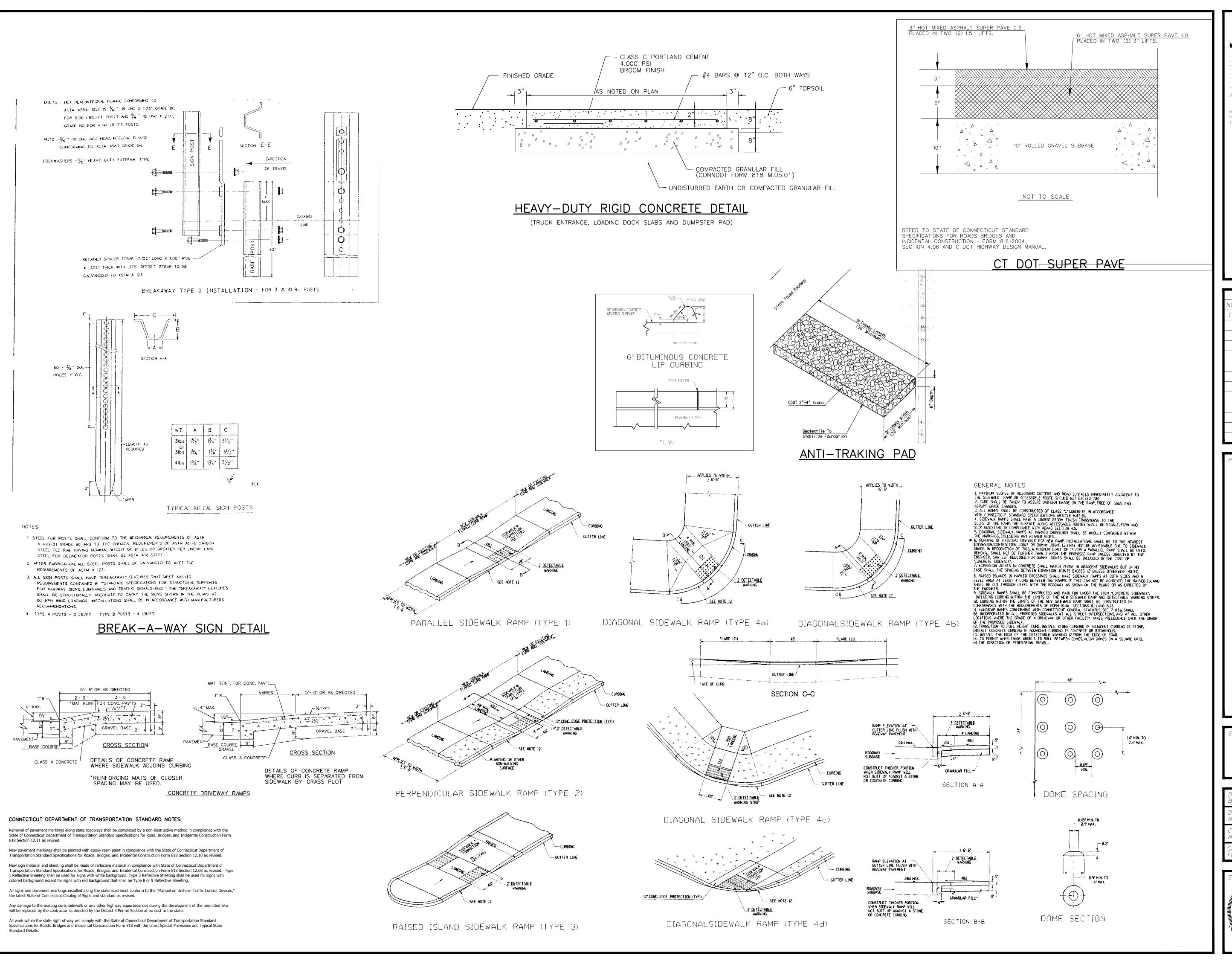
Prepared For: EATON ENTERPRISES, LLC

DETTAILS

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| | | DESIGNED BY: PR | SCALE: 1"=20' |
| | | DRAWN BY: MJS | DATE: 05-01-24 |
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PROPOSED TOWNHOUSES

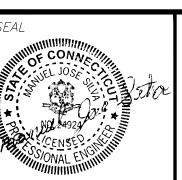
371 & 378 EAST MAIN STREET BRIDGEPORT, CONNECTICUT

Prepared For:

EATON ENTERPRISES, LLC

STATE DETTAILS

| | DESIGNED BY: PR | SCALE: 1"=20' |
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| | <i>DRAWN</i> BY: MJS | DATE: 05-01-24 |
| | CHECKED BY: MJS | PROJECT NUMBER: 2772 |
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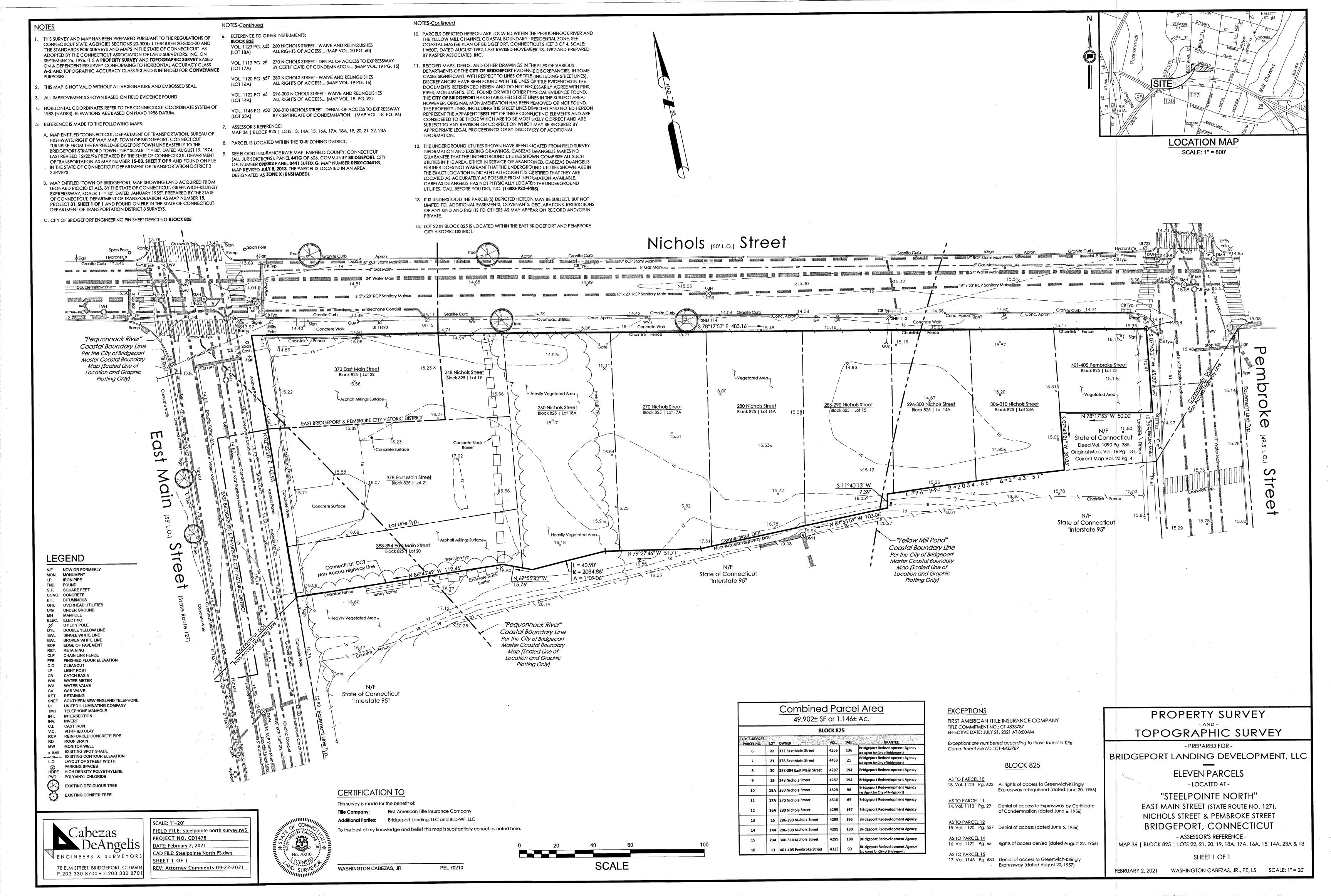
SP-6

371 East Main Street

| Parcel_ID | LOCATION | SLH_OWN_NA | SLH_CO_(SLH_OWN_AD | SLH_CITY | SLH_STT | SLH_ZIP |
|-----------|-----------------------|-------------------|-------------------------|------------|---------|------------|
| 825-21 | 378 EAST MAIN ST | BLD-WF LLC | 10 EAST MAIN ST STE 201 | BRIDGEPORT | CT | 06608 |
| 824-6 | 245 NICHOLS ST #247 | RIVERA SAMUEL | 245 NICHOLS ST #247 | BRIDGEPORT | CT | 06608-2708 |
| 824-3 | 432 EAST MAIN ST #438 | 432 EAST MAIN LLC | 48 DELAWARE RD | EASTON | CT | 06612 |
| 809-11A | 439 EAST MAIN ST #449 | 2068 MAIN LLC | 4403 15TH AVE SUITE 215 | BROOKLYN | NY | 11219 |
| 824-1 | 458 EAST MAIN ST #464 | FOCUS POINTE LLC | 24 LINDEN STREET | MANHASSETT | NY | 11030 |

| 378 | Fact | Main | Stro | ۵t |
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| - 1 | Parcel_ID | LOCATION | SLH_OWN_NA | SLH_CO_OWN | SLH_OWN_AD | SLH_CITY | SLH_STT | SLH_ZIP |
|-----|-----------|-----------------------|-------------------------------|-----------------|-------------------------------|------------|---------|------------|
| 8 | 339-3 | 353 NICHOLS ST #359 | STILLMAN & NICHOLS LLC | | 565 ELLSWORTH AVE | NEW HAVEN | CT _ | 06511 |
| 8 | 308-2 | 371 EAST MAIN ST #377 | BLD-WF LLC | | 10 EAST MAIN STREET SUITE 201 | BRIDGEPORT | CT | 06608 |
| 8 | 339-2 | 444 PEMBROKE ST #446 | RODRIGUEZ JOSE F JR | NATALIE ACEVEDO | 444 PEMBROKE ST #446 | BRIDGEPORT | CT | 06608-2603 |
| 8 | 324-12 | 441 PEMBROKE ST | REBOIRA RAYMOND | | 441 PEMBROKE ST | BRIDGEPORT | CT | 06608 |
| 8 | 309-10 | 411 EAST MAIN ST #425 | EAST MAIN ST | | 320 QUINNIPIAC AVE SUITE 4F | NEW HAVEN | CT | 06513 |
| 8 | 324-3 | 432 EAST MAIN ST #438 | 432 EAST MAIN LLC | | 48 DELAWARE RD | EASTON | CT | 06612 |
| 8 | 324-7B | 263 NICHOLS ST | HOUSING AUTHORITY CITY OF BPT | | 376 EAST WASHINGTON AVE | BRIDGEPORT | CT | 06608 |
| 8 | 309-11A | 439 EAST MAIN ST #449 | 2068 MAIN LLC | | 4403 15TH AVE SUITE 215 | BROOKLYN | NY | 11219 |
| 8 | 339/2A | | | | | | | |



CITY OF BRIDGEPORT

File No. _____



PLANNING & ZONING COMMISSION APPLICATION

| 1. | NAME OF APPLICANT: A.J.V. LLC |
|----|---|
| 2. | Is the Applicant's name Trustee of Record? Yes No X |
| | If yes, a sworn statement disclosing the Beneficiary shall accompany this application upon filing. |
| 3. | Address of Property: 4890 Main Street, 25 & 45 Sequioa Road and 2587 Old Town Road, Bridgeport, CT 06606 |
| | (number) (street) (state) (zip code) |
| 4. | Assessor's Map Information: Block No. 89/2600 Lot No. 4/C, 4/B, B/5 , B/4 |
| 5. | Amendments to Zoning Regulations: (indicate) Article: N/A Section: |
| | (Attach copies of Amendment) |
| 6. | Description of Property (Metes & Bounds): 120' x 136.62' x 65.02' x 176.62' x 185' x 23.56' x 30.35' x 141' |
| | |
| 7. | Existing Zone Classification: N4 |
| 8. | Zone Classification requested: MX2 |
| 9. | Describe Proposed Development of Property: The Application proposes to change the Property from the N4 Zone |
| | to the MX2 Zone |
| | Approval(s) requested: Zone Change |
| | |
| | Signature: Date: 08/12/2024 |
| | |
| | Print Name: |
| | If signed by Agent, state capacity (Lawyer, Developer, etc.) Signature: |
| | Print Name: Chris Russo |
| | Mailing Address: 10 Sasco Hill Rd, Fairfield, CT 06824 |
| | Phone: 203-255-9928 Cell: 203-255-9928 Fax: 203-576-6626 |
| | E-mail Address: Chris@russorizio.com |
| | |
| | \$Fee received |
| | |
| | THIS APPLICATION MUST BE SUBMITTED IN PERSON AND WITH COMPLETED CHECKLIST |
| | ■ Completed & Signed Application Form ■ A-2 Site Survey □ Building Floor Plans |
| | ■ Completed Site / Landscape Plan □ Drainage Plan □ Building Elevations |
| | ■ Written Statement of Development and Use ■ Property Owner's List □ Fee |
| | Cert. of Incorporation & Organization and First Report (Corporations & LLC's) |
| | B Ook of moorporation a organization and the report (corporations a 220 o) |
| | PROPERTY OWNER'S ENDORSEMENT OF APPLICATION |
| | A.J.V. LLC 08/12/2024 |
| | Print Owner's Name Owner's Signature Date |
| | |
| | Print Owner's Name Owner's Signature Date |

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Liam S. Burke Liam@russorizio.com

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Leah M. Parisi

Leah@russorizio.com William M. Petroccio*

WPetro@russorizio.com Raymond Rizio*

- * Also Admitted in NY
- Also Admitted in VT
- + Of Counsel

August 12, 2024

Paul Boucher Zoning Administrator Zoning Department 45 Lyon Terrace Bridgeport, CT 06604 HAND-DELIVERED

Re: Petition for Zone Change - 4890 Main St., 2587 Old Town Rd. and 25 & 45 Sequoia Rd.

Dear Mr. Boucher:

Please accept the following narrative and enclosed application materials as part of an application for a zone change under the Bridgeport Zoning Regulations (the "Regulations") for the properties located at 4890 Main Stret and 25 Sequoia Road (the "Site") to change the zone from N4 Zone to the MX2 Zone.

Narrative

The Site is currently located in the N4 Zone. The Applicant proposes to convert the Site to the MX2 Zone, which is located along the same commercial corridor of Main Street. The Site is located south of the Merritt Parkway and the City's border with Trumbull and contains three street frontages - Main Street, Sequoia Road and Old Town Road. There is a TD Bank located across Main Street and a large medical office building located across Old Town Road.

The Site is located in a transition area with a mix of uses of zones in the area, including the RX1, RX2, MX1 and MX2 Zones. Commercial properties are located directly across and north of the Site, while residential uses are located to the rear and south of the Site. The Site is obviously also located on one of the main commercial corridors in the City. Significant commercial uses are located in the area. Main Street is a vehicle-heavy corridor, but it does have an infrastructure of bus stops and sidewalks that can promote pedestrian activity.

Zone Change

The Petition satisfies the review and approval criteria for a zoning map amendment under Section 11.40.7 of the Regulations. The Petition is in conformity with the comprehensive plan as the Petition appropriately designates the Site within the MX2 Zone to which it conforms under the

Regulations. Commercial zones are located directly across from the Site and the MX2 Zone is in close proximity. The Regulations have put these zones under the umbrella of Mixed-Use & Commercial Zones. The properties along Main Street switch between the zones under this same umbrella. In addition, the Site contains enough lot area to provide a significant buffer between any use of the Site and the neighboring residential areas. Under the Regulations, the MX2 Zone is intended for a mixed-use center, which can serve the region. With its location on Main Street, the Site is easily accessible by City residents as well as regional residents by vehicle. It also makes the Site easily accessible by pedestrian means. The nearby bus stops and sidewalks promote the pedestrian activity that is desired in the City's Plan of Conservation and Development ("POCD"). One of the POCD's Guiding Principles for Bridgeport as a "Livable City" holds that the commercial corridors have to remain "safe and attractive places for walking and bicycling." Currently, there are no sidewalks on the Site because it is a residential zone that breaks up the sidewalks that exist to the north and south of the Site. It disrupts the connectivity desired in the POCD. The Application will help provide this connection. The POCD also acknowledges that economic activity in the City has slowed over the decades that have left Bridgeporters "wanting for businesses that support their daily needs as well as an occasional shopping trip." The Application will promote a continuous commercial corridor that can have the Site host one of these businesses to support the daily needs of Bridgeporters.

For the above-stated reasons, the Application satisfies all the applicable standards for a change in zone under the Regulations and the Applicant respectfully requests its approval.

Sincerely,

Chris Russo

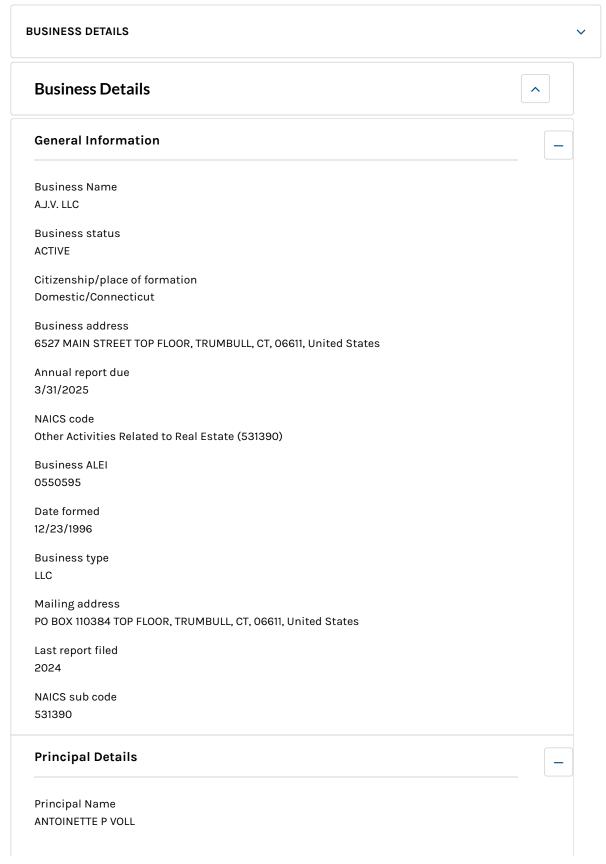
Attorney for Applicant

4890 MAIN ST 2587 OLD TOW ROAD, 25 & 45 SEQUOIA RD - 100 ABUTTERS LIST

| LOCATION | OWNER | OWNER ADDRESS | CITY | STATE | ZIP |
|--------------------|--------------------------|---------------------------|-----------------|-------|------------|
| 25 SEQUOIA RD | MFD LLC | 6527 MAIN ST 2ND FLR | TRUMBULL | CŢ | 06611 |
| 4865 MAIN ST | PT MAIN STREET LLC | 252 ROBBY LANE | MANHASSET HILLS | NY | 11040 |
| 45 SEQUOIA RD | MFD LLC | 6527 MAIN ST 2ND FLR | TRUMBULL | CT | 06611 |
| 4890 MAIN ST | AJVLLC | PO BOX 110384 | TRUMBULL | CT | 06611 |
| 2587 OLD TOWN RD | AJVLLC | PO BOX 110384 | TRUMBULL | 7 | 06611 |
| 2571 OLD TOWN RD | ST. GERMAIN MARIE | 2571 OLD TOWN RD | BRIDGEPORT | C | 06606 |
| 4920 MAIN ST | CENTURION HOLDINGS 1 INC | 4920 MAIN ST | BRIDGEPORT | C | 06606 |
| | FERRANTE JOSEPHINE C/O | | | | |
| 16 MINTURN RD | VICTOR M FERRANTE | 1087 BROAD STREET STE 202 | BRIDGEPORT | CI | 06604 |
| 4840 MAIN ST #4842 | MAIN SEQUOIA LLC | P O BOX 110384 | TRUMBULL | C | 06611 |
| 44 SEQUOIA RD | J G V BUILDERS | P O BOX 110384 | TRUMBULL | C | 06611 |
| | VANSCOY LAVETTE PAUL & | | | | |
| 60 SEQUOIA RD | MARIA VANSCOY | 60 SEQUOIA RD | BRIDGEPORT | CI | 06606 |
| 61 SEQUOIA RD | NOLE COLETTE | 61 SEQUOIA RD | BRIDGEPORT | C) | 06606-1352 |
| 2555 OLD TOWN RD | MACHADO JUVENTINA | 2555 OLD TOWN RD | BRIDGEPORT | CT | 06606 |
| 2543 OLD TOWN RD | OSORIO DAVID & ELIZABETH | 2543 OLD TOWN ROAD | BRIDGEPORT | CI | 06606 |
| 77 SEQUOIA RD | DA COSTA EVANDRO L | 77 SEQUOIA ROAD | BRIDGEPORT | CT | 06606 |
| | ADARKWA ADWOA AKOTO | | | | |
| 76 SEQUOIA RD | NYAMEK | 76 SEQUOIA RD | BRIDGEPORT | CT | 06606 |
| | | | | | |

A.J.V. LLC ACTIVE

6527 MAIN STREET TOP FLOOR, TRUMBULL, CT, 06611, United States



Principal Title
Member

Principal Business address
6527 MAIN STREET, TOP FLOOR, TRUMBULL, CT, 06611, United States

Principal Residence address
17 COLONIAL DRIVE, MONROE, CT, 06468, United States

Agent details

Agent name
JOSEPH G. VOLL

Agent Business address
6527 MAIN STREET, TOP FLOOR, TRUMBULL, CT, 06611, United States

Agent Mailing address
6527 MAIN STREET TOP FLOOR, TRUMBULL, CT, 06611, United States

Filing History

Agent Residence addresss

17 COLONIAL DRIVE, MONROE, CT, 06468, United States

Business
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Certificate of Organization
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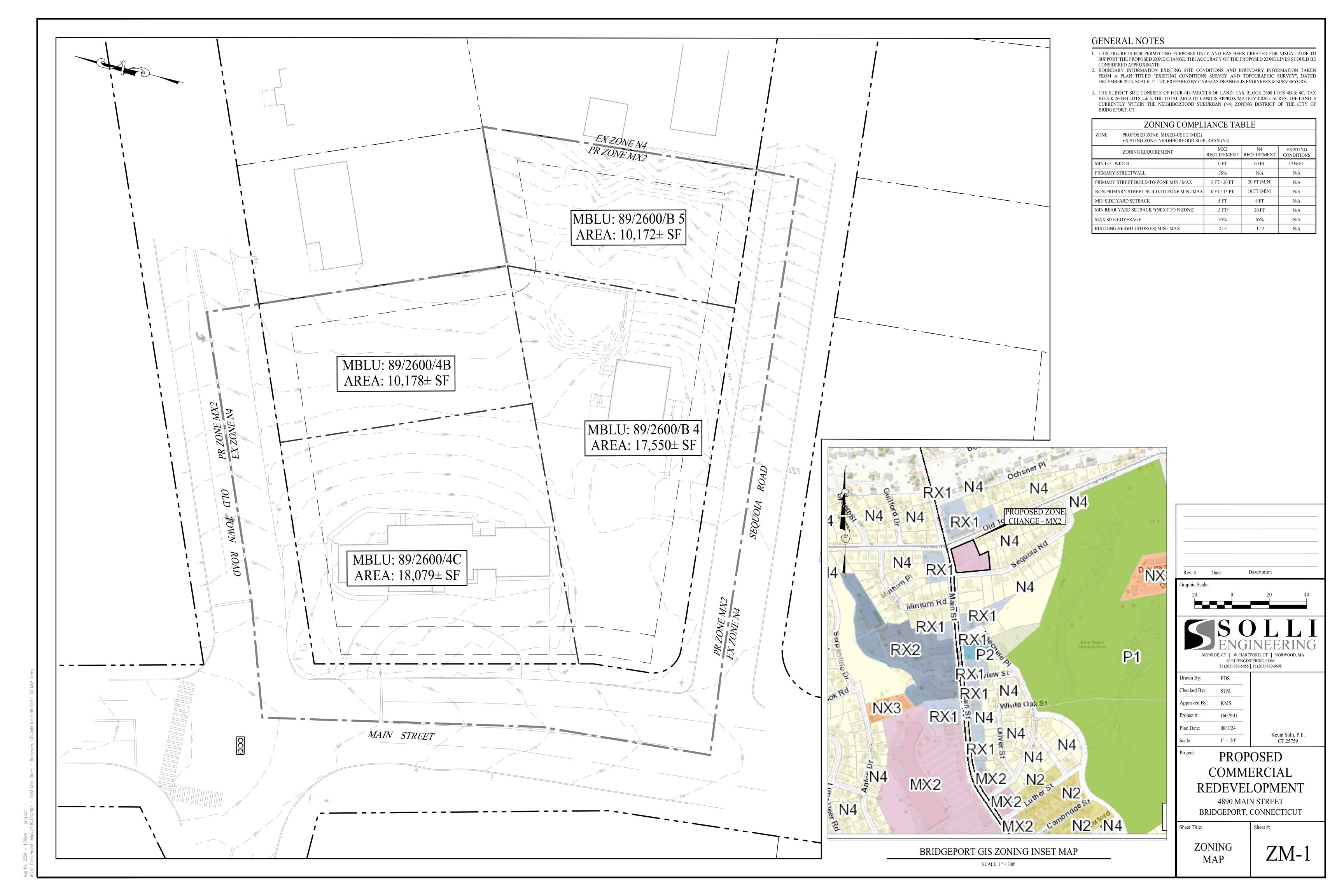
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Digital copy

View as PDF

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CITY OF BRIDGEPORT



File No. _____

PLANNING & ZONING COMMISSION APPLICATION

| 1. | NAME OF APPLICANT: Swanston Family Ventures, LLC and Connecticut Sports Group, LLC |
|----|--|
| 2. | Is the Applicant's name Trustee of Record? Yes No X |
| | If yes, a sworn statement disclosing the Beneficiary shall accompany this application upon filing. |
| 3. | Address of Property: 141 Stratford Ave. and 255 Kossuth St., Bridgeport, CT 06605 |
| | (number) (street) (state) (zip code) |
| 4. | Assessor's Map Information: Block No. 36/804 & 805 Lot No. 1/X & 5/A |
| 5. | Amendments to Zoning Regulations: (indicate) Article: N/A Section: |
| | (Attach copies of Amendment) |
| 3. | Description of Property (Metes & Bounds): See Attached Survey |
| | |
| 7. | Existing Zone Classification: P1, P2 and DX2 |
| 3. | Zone Classification requested: N/A |
| 9. | Describe Proposed Development of Property: To construct a soccer stadium, public plaza and open space, |
| | brewery/restaurant building, off-street parking and associated site improvements |
| | Approval(s) requested: Special Permit, Subdivision, Site Plan Review and Coastal Site Plan Review |
| | |
| | Signature: Date: 07/25/2024 |
| | Print Name: |
| | |
| | If signed by Agent, state capacity (Lawyer, Developer, etc.) Signature: |
| | Print Name: Chris Russo |
| | Mailing Address: 10 Sasco Hill Rd, Fairfield, CT 06824 |
| | Phone: 203-255-9928 Cell: 203-255-9928 Fax: 203-576-6626 |
| | E-mail Address: Chris@russorizio.com |
| | |
| | \$Fee received |
| | |
| | THIS APPLICATION MUST BE SUBMITTED IN PERSON AND WITH COMPLETED CHECKLIST |
| | ■ Completed & Signed Application Form ■ A-2 Site Survey ■ Building Floor Plans |
| | ■ Completed Site / Landscape Plan ■ Drainage Plan ■ Building Elevations |
| | ■ Written Statement of Development and Use ■ Property Owner's List □ Fee |
| | ■ Cert. of Incorporation & Organization and First Report (Corporations & LLC's) |
| | |
| | PROPERTY OWNER'S ENDORSEMENT OF APPLICATION |
| | 255 Kossuth LLC 07/25/2024 |
| | Print Owner's Name Owner's Signature Date |
| | Print Owner's Name Owner's Signature Date |
| | Finit Owner's Name Owner's Signature Date |

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Leah M. Parisi

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* Also Admitted in NY

Also Admitted in VT

+ Of Counsel

July 25, 2024

Paul Boucher Zoning Administrator Bridgeport Zoning Department 45 Lyon Terrace Bridgeport, CT 06604

Re: Application to Bridgeport Planning and Zoning Commission for properties located at 141 Stratford Avenue and 255 Kossuth Street

Dear Mr. Boucher:

Please accept the following narrative and enclosed application materials as part of an application for Subdivision, Special Permit, Site Plan Review and Coastal Site Plan Review under the Bridgeport Zoning Regulations (the "Regulations") for the properties located at 141 Stratford Avenue and 255 Kossuth Street (the "Site") to construct a soccer stadium, public plaza and open space, brewery/restaurant building and associated Site improvements in the P1 & P2 Zone.

Written Statement of Development and Use

The Applicant proposes to construct a soccer stadium, public plaza and open space, brewery/restaurant building and associated Site improvements on the Site. The Site consists of property over three (3) acres and has received the necessary approval for a master plan development ("MPD") from the Commission. This Application marks the first phase of the MPD and is in accordance with that approval.

The Site is the location of a former dog track and jai alai facility on the property identified as 255 Kossuth Street. It contains dog track facilities on its southern end and an existing parking area on its northern half. The property identified as 141 Stratford Avenue is the former location of the AGI Rubber Company. The Applicant proposes to demolish all existing structures on the Site and revitalize the Site with completely new construction. The Site contains a significant frontage on Kossuth Street from its southern end to its northern end. Along its southern boundary line, the Site is bounded by Stratford Avenue. The Pequonnock River is located along its western boundary.

The Applicant proposes to construct a new soccer stadium to be located on the southern portion of 255 Kossuth Street in the location of the existing dog track facilities. The "Civic, Large" use is permitted through a Special Permit under the Civic Building Type in the P2 Zone. Said stadium will be the host of a new minor league soccer team and will contain 7,500 seats. The stadium has been designed with open concourses to provide views onto the field and visibility from I-95. It features a sleek and modern design with a shipping-container-inspired architecture as a reference to Bridgeport's history. Extensive lighting of the stadium in various colors will add vibrancy to the area as depicted in the submitted renderings. It will be a tremendous new landmark for the City of Bridgeport. The stadium will contain its own food and vending options for patrons.

To the south of the stadium, the Applicant proposes a park that will serve as a fan zone for pre- and post-game activities on game-day. This area will contain a number of soccer-related features, including a central plaza in the shape and design of a soccer ball. On days without soccer games, the park will serve as a community asset with public access and recreational use on the proposed multi-sports fields. Children in Bridgeport will be able to play on a soccer field with the backdrop of a professional soccer stadium behind them. This area will also include a restaurant building envisioned for a brewery/restaurant along the Pequonnock River waterfront. The "Retail & Entertainment" use is permitted through a Special Permit under the Civic Building Type in the P1 Zone. The exterior design of the restaurant will consist of glass and metal panels to complement the stadium.

On-site parking in the southwestern corner of the Site will provide daily access from Stratford Avenue to this restaurant as well as parking for patrons to the soccer merchandise store. An existing parking area on the north side of the stadium, which was previously used for the dog track, will be utilized for parking at the stadium. Service access to the stadium will be provided at the northeast corner of the stadium to allow large tractor-trailers and other delivery cans to easily circulate to a loading zone. The loading zone will be screened from the public roadway. The majority of attendees will park in the several parking garages in the nearby vicinity within short walking distance. These garages are well below capacity and can accommodate a large portion of the attendees' vehicles. A parking study has been submitted with this application, which found that there will be an excess of parking during weekday evening games and that additional garages could be utilized for weekend games to ensure there is sufficient parking. The Applicant has been in conversations with the City to make that parking available. Attendees walking to the stadium will utilize the Stratford Avenue Bridge for access. It should also be noted that the Site is in close proximity to the train station, which will also provide easy access for many attendees.

The Application will also provide for a temporary access to the riverfront. The riverfront will not be fully complete until the next phase of the development, but the Applicant has provided this temporary access in the Application to provide access to the public, which has been prevented for decades. Native vegetation will be located throughout the Site. A significant improvement to the Site will be the integration of new stormwater

features. The transformation of the Site, which is currently a brownfield, to a property that contains improvements to current standards and creates public open space is a complete revitalization of a large and underutilized waterfront property. The Site is also located within the floodplain. The Applicant has included a floodplain study with this submission, which concluded that the project would not result in any impact to downriver properties. Retaining walls will be utilized to avoid tidal wetlands associated with the riverbank and ensure there will be no impact to wetlands. The Site will utilize public water and sanitary sewer through newly installed lines.

As part of the Application, the Applicant is requesting to subdivide the property known as 255 Kossuth Street to split the parcel between the area containing the soccer stadium and the area containing the existing parking. For these reasons, the existing parking area will require a Special Permit as it will become a non-accessory parking use. It will support the soccer stadium, which will be on a separate lot. This will also divide the parcel among the zone lines approved in the MPD. The upper portion of 255 Kossuth Street is located within the DX-2 Zone and the lower portion of 255 Kossuth Street is located in the P2 Zone. The proposed lots meet the lot requirements under the Regulations as there is no minimum lot area and the lot proposed to contain the stadium will contain more than 50' of lot width.

Special Permit

The Application satisfies the Sec. 11.50 Special Permit standards of the Regulations. First, the proposed soccer stadium, restaurant/brewery and non-accessory parking uses are consistent with and implement the objectives and policies of the master plan of conservation and development (the "POCD"). The POCD's vision viewed Bridgeport as a regional center in eastern Fairfield County. It is the very first sentence of the Vision Statement. The Application will create a sports and entertainment district unlike any in Fairfield County. The Site will host a professional team in one of the most popular sports in the world. A sport which has experienced gains in popularity year after year. In its goal for Bridgeport to become a regional center, the POCD actually states that there should be an initiative to redevelop the waterfront "with an eye towards the potential to create a recreational attraction unique in the Northeast." The Application clearly satisfies that initiative.

The Application also helps create a livable city with easy access to a major public venue while also growing Bridgeport's economy with the wealth of job opportunities it will provide. It will also create a walkable attraction in the Downtown area with easy access to mass transit thereby reducing the need for vehicles. The transformation of the Site from a vacant and derelict brownfield to a vibrant public attraction providing open space and waterfront access satisfies multiple goals of the POCD, but particularly its goal to improve the environment. One of the main guiding principles for the benefit of the City's economy was the revitalization of the City's waterfront. Vacant parcels and outdated buildings are cited as the significant existing challenge. This Application represents the first phase of a

multi-phase project, which will completely rehabilitate a waterfront that extends over 1,500' from the Stratford Avenue bridge to the railroad tracks.

In accordance with the second Special Permit standard, the Application, including the proposed subdivision and site plan, is fully compliant with all applicable Regulations. Further, the proposed use and site plan will not impair the future development of the surrounding areas. In fact, it will spur development. The proposed use will attract thousands to Downtown Bridgeport and create jobs on- and off-Site. It will utilize existing parking garages which are significantly below capacity. It will encourage the use of mass transit thereby boosting the importance of the Bridgeport train station. The Applicant has submitted a traffic and parking study, which found that the demand from the proposed use will not impair development in the surrounding area.

The proposed uses will not be detrimental to existing development in the surrounding area because of the height, scale, design or method of operation. The proposed buildings are in conformity with the bulk standards of the Regulations. They will be constructed in the manner the Commission deliberately planned through its Regulations. In fact, reopening the waterfront on the Site to the public will be an asset to existing development. It will be an amenity for all in the area, including the residents of the multitude of high-density developments recently approved in the surrounding area. To ensure safety, security cameras and other security measures will be placed throughout the Site. During gamedays, staff will also be utilized off-Site to ensure safe and efficient access of attendees to the Site.

The proposed use is not likely to cause a depreciation in the value of nearby properties. It will cause the opposite. As a vibrant city landmark that will become a sports and entertainment hub for the entire region while still providing a local public amenity with its access to open spaces and the waterfront, the proposed use will increase nearby property values.

Finally, the potential for environmental impacts to Long Island Sound have been appropriately mitigated by the proposed measures under the Application. As stated above, a floodplain study has been submitted with this Application which concluded there will be no impact to downriver properties.

Site Plan Review

The Application satisfies the Sec. 11.70 Site Plan Review standards of the Regulations as it fully complies with the standards of the Regulations. The design of the proposed building and landscaping create a harmonious building-street interaction providing a tremendous improvement to the existing streetscape from the existing vacant site. The scale and proportion of the buildings conform to the P1, P2 and DX-2 Development Standards. The Application proposes significant public access to the Site and waterfront. This is access that has been denied to the residents of Bridgeport for decades. The proposed use will be a

tremendous complement to the surrounding commercial and residential areas as regional landmark. It will also be a significant employer. The Site is located in close proximity to I-95, a major thoroughfare, multiple water access points and the train station, which provides a number of modes of access to the Site. In addition, the Site is in close proximity to underutilized Downtown parking garages. It is an ideal location for this use.

Coastal Site Plan Review

The Application also complies with Section 11.80 of the Regulations regarding coastal site plan review. As stated above, the Application fully complies with the site plan review standards of the Regulations. The Application poses no danger or threat to coastal resources and it has no potential adverse impacts as demonstrated in the submitted materials. While the Application does not propose a water-dependent use, it will provide public access to a waterfront which has not been open for decades. The proposed building and Site improvements will all be constructed in accordance with current codes and regulations, including the appropriate stormwater drainage systems. Sediment and erosion controls, such as silt fencing and anti-tracking aprons, will be utilized during construction. The Applicant has provided for necessary measures, such as the construction of retaining walls, to protect nearby tidal wetlands.

Subdivisions

The Application satisfies the standards of Sec. 11.100 of the Regulations regarding Subdivisions. As stated above, the Application complies with all applicable sections of the Regulations. The Applicant only requests to subdivide the property identified as 255 Kossuth Street. The upper portion of said property is located in the DX-2 Zone and the lower portion is located in the P2 Zone. Neither zone requires a minimum lot area and both lots significantly exceed the 50' minimum lot width requirement. For these reasons, the proposed subdivision is fully compliant.

For all the above-stated reasons, the Application satisfies all the applicable standards of the Regulations and the Applicant respectfully requests approval for the proposed special permit uses, subdivision, coastal site plan review and site plan review.

Sincerely,

christopher Russo

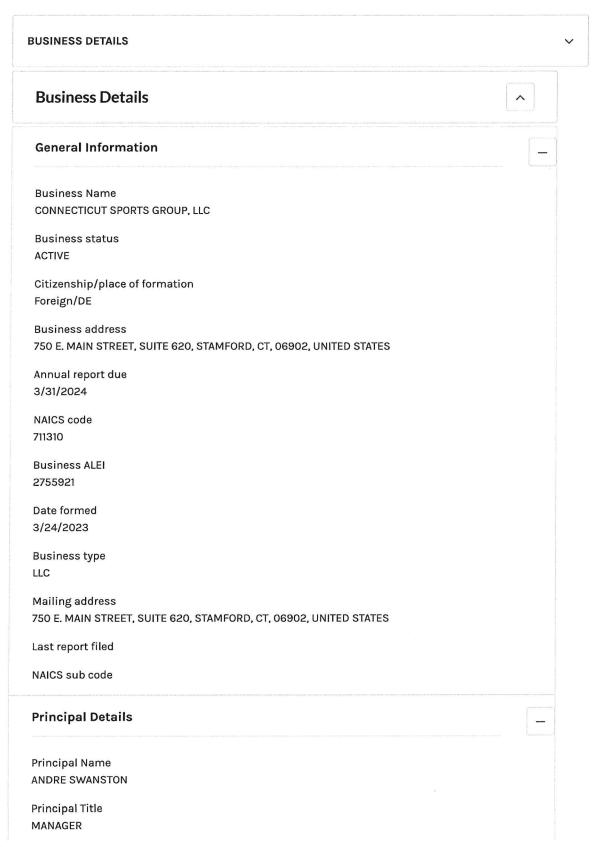
LIST OF PROPERTY WINNERS WITHIN 100' OF 141 STRATFORD AVENUE AND 255 KOSSUTH STREET, BRIDGEPORT, CT

| | | | | | | | | | | 00 | | ١. | _ | | LX | | | EV | _ |
|----------------------|-------------------------|-------------------------|----------------------|----------------------|----------------------|----------------|-----------------|--------------------|-----------------------------|-----------------|-----------------|-----------------|-----------------------|---------------------------------|--------------------------------|-----------------|----------------------------|------------------|---------------|
| 44 CRESCENT AV #52 | 202 NOBLE AV #204 | 155 PULASKI ST #157 | 125 PULASKI ST | 90 PULASKI ST | 110 PULASKI ST | 304 KOSSUTH ST | 100 KOSSUTH ST | 141 STRATFORD AV | 46 SEYMOUR ST | 83 HOWE ST #153 | 150 KOSSUTH ST | 255 KOSSUTH ST | 401 KOSSUTH ST | | 1 NOBLE AV | 363 KOSSUTH ST | 370 KOSSUTH ST #372 | 104 BURROUGHS ST | LOCATION |
| STATE OF CONNECTICUT | MAPLEWOOD AVE LLC | MAPLEWOOD AVE LLC | STATE OF CONNECTICUT | STATE OF CONNECTICUT | STATE OF CONNECTICUT | MAVI GROUP LLC | 255 KOSSUTH LLC | BRIDGEPORT CITY OF | VARGAS BILLING SERVICES LLC | 255 KOSSUTH LLC | 255 KOSSUTH LLC | 255 KOSSUTH LLC | CHRISTIAN ASSOC. INC. | CENTRAL CONNECTICUT COAST MEN'S | CHEMICAL ABUSE SERV AGENCY INC | 255 KOSSUTH LLC | ST MICHAEL ARCHANGEL ROMAN | MAVI GROUP LLC | OWNER |
| PO DRAWER A | 4403 15TH AVE SUITE 215 | 4403 15TH AVE SUITE 215 | 165 CAPITOL AVE | PO DRAWER A | PO DRAWER A | 17 WOODLAWN RD | 133 RIVER RD | 45 LYON TER | 46 SEYMOUR ST | 133 RIVER RD | 133 RIVER ST | 133 RIVER ST | 1240 CHAPEL ST | | 690 ARCTIC STREET | 133 RIVER RD | 310 PULASKI ST | 17 WOODLAWN RD | OWNER ADDRESS |
| WETHERSFIELD | BROOKLYN | BROOKLYN | HARTFORD | WETHERSFIELD | WETHERSFIELD | TRUMBULL | MYSTIC | BRIDGEPORT | BRIDGEPORT | MYSTIC | MYSTIC | MYSTIC | NEW HAVEN | | BRIDGEPORT | MYSTIC | BRIDGEPORT | TRUMBULL | CITY |
| CT | N | N N | 2 | C | 9 | C | 2 | 9 | 2 | 2 | 2 | 2 | 2 | | 7 | 9 | C | 2 | STAT |
| 06109 | 11219 | 11219 | 06106 | 06109 | 06109 | 06611 | 06355 | 06604 | 06608 | 06355 | 06355 | 06355 | 06511 | | 06608 | 06355 | 06608 | 06611 | STATE ZIP |

7

CONNECTICUT SPORTS GROUP, LLC ACTIVE

750 E. MAIN STREET, SUITE 620, STAMFORD, CT, 06902, UNITED STATES



Principal Business address 750 E. MAIN STREET, SUITE 620, STAMFORD, CT, 06902, United States Principal Residence address 122 NOD HILL ROAD, RIDGEFIELD, CT, 06877, United States Agent details Agent name COGENCY GLOBAL INC. Agent Business address 29 WEST HIGH STREET, EAST HAMPTON, CT, 60424, United States Agent Mailing address 29 WEST HIGH STREET, EAST HAMPTON, CT, 60424, United States **Filing History Business** Registration -(https://ctds.my.salesforce.com/sfc/p/t0000000PNLu/a/8y000004HIAQ/6mNQoB.agBp_et2Jw2yoRH.OH_Z8U9wdl_KeL9PpJh8) Foreign Registration Statement 0011751222 Filing Filing date: time: 3/24/202303:30 PM Volume Type Volume Start page Pages Date generated 3/24/2023 Digital copy View as PDF (https://ctds.my.salesforce.com/sfc/p/t0000000PNLu/a/8y000004HIAQ/6mNQoB.agBp_et2Jw2yoRH.OH_Z8U9wdl_KeL9PpJh8) **Name History** None



July 25, 2024

City of Bridgeport Planning and Zoning Commission City Hall 45 Lyon Terrace Bridgeport, Ct. 06604

RE: Technical Submission for Phase 1 Redevelopment of 255 & 363 Kossuth St. and 141 Stratford Avenue in the City of Bridgeport, Connecticut

Dear Commission Members:

On behalf of the Connecticut Sports Group (CTSG) we are pleased to submit this technical submission for Phase 1 of the Bridgeport Waterfront Project, the development of a 7,500 seat soccer stadium and associated facilities

Written Statement of Project Use (Project Description)

The project will redevelop the subject waterfront property into a vibrant, sustainable, stateof-the-art waterfront community. The multi-phased redevelopment program is designed to transform the site from a vacant and underutilized property into an energetic development that will create a sports and entertainment district with an abundance of first-class quality amenities that include (i) commercial retail; (ii) public greenspace/parks; (iii) housing accommodations; (iv) sustainable waterfront condition; (v) a hotel; and (vi) a sports and entertainment facility serving as the cornerstone of the project. The project will serve as a catalyst for economic growth, job creation, and an increased tax base for the City of Bridgeport. This project aligns with all six Guiding Principles of Bridgeport's Plan of Conservation and Development (2019). For example, Principle 1 - Bridgeport is a livable city - Goal 1.2 is to "Encourage density of development in areas that are well served by transit and are within walking distance of places of residence, employment, goods, and services." The site is less than half a mile from the Bridgeport train and bus stations. The project aligns with Principle 5 - Bridgeport values nature - Goal: 5.4: "Improve existing parks and open space network to ensure that functional open space is accessible to residents of all neighborhoods." The current green spaces on the site are not accessible but will be transformed. The project will also create new green spaces, accessible to the public.

The Phase 1 development comprises a 7,500-seat stadium and a park offering three soccer fields and a riverfront retail location and/or cafe. The stadium will showcase open concourses with views to the field, team facilities, party terraces, suites, a pitch club, and stadium club featuring a wide variety of seating and food options.



Submission Materials

The Submission consists of the following materials. A brief description of project components follows.

- 1. Site Plan Application
- 2. Coastal Zone Application
- 3. Property Owners List
- 4. Cert. or Corporation/Org. of First Report
- 5. Site Plans consisting of:
 - a. Cover sheet
 - b. Survey
 - c. Site Plan
 - d. Drainage Plan
 - e. Water/Sewer plan
 - f. Floor plans
 - g. Elevations
- 6. Technical Reports consisting of:
 - a. Parking Study
 - b. Floodplain Study
 - c. Wetlands Report
 - d. Utilities Engineering

Site Design

Phase-1 Site: The initial Phase-1 site development is located on the southern half of the redevelopment site and includes the following development areas:

- Stadium Lot Size: 405,268 SF (9.30 acres)
- Stadium Footprint Area: Approximately 235,000 SF
- South Park and Retail Location and/ or Café Lot Size: 109,107 SF (2.5 acres)
- Retail Location and/ or Cafe Footprint: 4,400 SF
- Total Phase I Area: 514,375 SF (11.8 acres)

Design Approach for Phase-1 Development: The Phase-1 stadium site has been designed to accommodate two possible future scenarios:

- 1. The Phase-1 stadium remains long-term as a permanent stadium and home to an MLS Next Pro soccer team and other potential teams.
- 2. Connecticut Sports Group, the City of Bridgeport, and the State of Connecticut succeed in bringing a Major League Soccer team to Bridgeport, at which point the Phase-1 modular stadium will be disassembled and relocated to another site and replaced with a larger state-of-the-art MLS soccer stadium.

Some elements of the Phase-1 site will be affected during the construction of a possible Phase-2 stadium. Therefore, the site and landscaping materials used in the initial



development will accommodate future construction considerations and site upgrades, ensuring a seamless transition.

Riverfront Development: The Phase-1 development will not encroach on the existing riverfront, thereby minimizing initial construction costs and regulatory reviews. The initial phase envisions a Phase-1 riverwalk set back from the shoreline, extending the full length of the Phase-1 site. It is anticipated that the Phase-2 development will more dramatically impact the shoreline, creating a more extensive and dynamic riverwalk and linear park along the full length of the property, connecting the small pocket park on the north end to the larger park on the south end.

South Park: The park will serve as a community asset for public access, recreational use, and active competition on the multi-sport fields. The southwest corner of the park will include a restaurant, retail location, and/or cafe, which will be open to the public on both gamedays and non-gamedays. The restaurant will include some onsite parking for daily use and provide convenient parking during the week for visitors purchasing tickets or merchandise at the stadium. The south end park will serve as a fan zone on game days for pre- and post-game activities. Most stadium attendees will walk across the Stratford Avenue Bridge from downtown and enter the stadium through the south plaza.

Parking: In addition to new parking adjacent to the restaurant and stadium in the southwest corner of the property, the existing parking lot to the north will be used for VIP parking until further development during Phase-2. Access to the stadium from the north parking lot is provided at several locations on the north endzone. All other parking will be offsite, utilizing existing downtown surface lots and parking garages, along with public transit.

Landscape Design: The stadium's perimeter and park landscape are designed to reflect the shipping container-inspired architecture of the stadium and the hexagonal pattern found on a soccer ball. This enhances the soccer experience and creates a unique thematic and visual cohesion between the structure and the site. The riverfront location offers a unique setting with opportunities to engage with and experience the river's edge on both game days and non-gamedays. Spaces adjacent to the stadium allow for gameday circulation and activities for large groups while maintaining human-scaled pockets for smaller gatherings. Customized shipping containers will be used throughout the site to reinforce the architecture and define spaces. A palette including local materials and native vegetation will pay homage to the natural Connecticut landscape. Additionally, stormwater features will be integrated into the overall design. The park includes active and passive areas, such as open fields for soccer and other activities, a splash pad fountain, a container garden, unique play elements, wide promenades, and a tree bosque plaza. It is designed to provide flexibility for both park and stadium guests, connecting the south end of the stadium to the street network leading to the stadium.



Stadium Service Access: Service access will be provided at the northeast corner of the stadium to allow large tractor-trailers and other delivery vans to easily circulate to a loading zone that will be visually screened from the adjacent roadway and parcels to the east.

Architectural Design

Overview: The Bridgeport Stadium project aims to transform a vacant waterfront property into a vibrant, sustainable, and state-of-the-art community hub. This multi-phased redevelopment will create a dynamic sports and entertainment district, including commercial retail, public greenspace, housing, a hotel, and a sports facility. This development will catalyze economic growth, job creation, and an increased tax base for Bridgeport, aligning with the city's Plan of Conservation and Development.

Phase I Development: Phase I encompasses a 7,500-seat stadium, expandable to 10,000-15,000 seats. The stadium will offer open concourses with field views, team facilities, party terraces, suites, a pitch club, and a third-floor stadium club with diverse seating and food options.

Design Philosophy: Since its advanced ship-building industry in the mid-18th century, Bridgeport has been a city of industry, commerce, and collaboration. With the booming immigrant population that came with the industrial revolution in the 19th century, Bridgeport became a thriving industrial center, shipping products all over the globe with more than 500 factories, including giants like Wheeler and Wilson, Remington UMC, Bridgeport Brass, Columbia Records, General Electric, and the American Graphophone Company.

The Bridgeport Modular Soccer Stadium celebrates this history. On the main West Grandstand and Building, instead of hiding the modularity of the components, modules of different tones are joined and offset to create solids and voids that highlight the stacking effect and industrial nature of the prefabricated "kit of parts." From the riverwalk and downtown views on the west, these modules resemble stacked containers at a port, working together to create an elegant building topped by a crane-like roof canopy structure that silhouettes the skyline and honors the uniqueness of Bridgeport's history.

Construction Details:

- West Building: A 3-story structure using volumetric or modular construction and custom-building exterior designs, capable of supporting all intended uses and significantly reducing construction time.
- **Grandstands**: Aluminum and steel modular grandstands with individual armchair seating, complemented by modular construction for essential facilities like restrooms and concessions.

Restaurant/ Retail Location and/or Cafe: The restaurant/retail location and/ or café will feature a versatile exterior design of glass and metal panels, complementing the stadium architecture and ensuring compatibility with both conventional and modular construction



methods. This venue adds to the vibrant atmosphere, offering an enticing element to visitors and sports enthusiasts alike.

Community Impact: The project is strategically located less than half a mile from Bridgeport train and bus stations, supporting the city's goal of encouraging dense development in transit-friendly areas. The transformation of a brownfield site with inaccessible green spaces into public parks aligns with Bridgeport's vision of improving open space accessibility for all residents.

Access and Parking

The proposed stadium is located on the east side of the Pequonnock River, while the majority of the parking will be located on the west side of the river in the core of Downtown Bridgeport. It is expected that the majority of attendees will park on streets or in lots and garages on the west side of the river and then cross the Stratford Avenue bridge to access the stadium. Therefore, a detailed review of the existing parking options located in Downtown Bridgeport was completed; see attached parking study. This review demonstrated that there will be an excess of parking during weekday evening games and that arrangements should be made to open the Park City Parking Garage and the Harbor Yard Transit Garage during weekend games to ensure that there is sufficient parking. The Applicant is engaged in discussions to do so.

Pedestrians will access the stadium by crossing the Stratford Avenue Bridge. It is likely that temporary lane closures will be required before and after games to accommodate pedestrians. The Applicant will pursue discussions with the State of Connecticut, which owns Stratford Avenue, in this regard.

The Applicant is currently conducting a traffic study to determine if improvements are needed in association with the Phase 1 project. The results will be submitted as soon as they are complete.

<u>Floodplain</u>

Portions of the site are located within the 100-year floodplain of the Pequonnock River. The floodplain on the site is tidal rather than riverine in nature. The attached floodplain study was conducted to determine whether project grading would cause a rise in downriver flood levels. The study concluded that no such rise would occur and that the project would not result in any impact to downriver properties.

Wetlands

A wetland delineation was performed for the project site.; see attached report Tidal wetlands are associated with the Pequonnock Riverbanks. All Phase 1 development will avoid wetlands; retaining walls will be employed to separate site development from the wetlands. The Phase 1 project will avoid the river bank and its associated wetlands and therefore there will be no impact to wetlands.



Utilities Engineering

Water and sanitary sewer are available at the site. The existing utility lines will be removed and new lines installed. Water tests were conducted which demonstrated that there is adequate flow for both potable and fire protection needs. Wastewater will be conveyed to an existing 12" line in Kossuth Avenue and from there to the City's wastewater treatment plant.

Stormwater from the site is directed to the Pequonnock River via three existing outfalls. Some stormwater from the City's system is routed through the site via these outfalls. Because site soils are likely contaminated it is unlikely that stormwater infiltration practices will be utilized. Stormwater is likely to be conveyed off site. Wherever possible impervious parking and related surfaces will be used to minimize stormwater runoff.

Environmental Remediation

Historic utilization and imported urban fill material have impacted soil and groundwater at the Site. The full nature and extent of soil and groundwater contamination is currently under investigation. To this end, CTSG has received \$8,000,000 in Municipal Brownfield Cleanup Grants that will be applied toward investigative and remedial activities. CTSG has also applied for acceptance to the Connecticut Abandoned Brownfields Cleanup (ABC) Program. Upon acceptance, the Site will be entered into the Voluntary Cleanup Plan and CTSG will complete their acquisition of the property.

A Remedial Investigation consisting of a Phase III Environmental Site Assessment will be performed under direct supervision of Connecticut Licensed Environmental Professional and in accordance with Connecticut Department of Energy and Environmental Protection and ABC Program regulations. A comprehensive evaluation of soil, groundwater, and soil vapor will be performed to assess for impacts associated with historic Site utilization, poorquality urban fill materials, and release(s) of petroleum and hazardous materials. Groundwater at the Site will also be evaluated for per- and poly-fluoroalkyl substances (pfas) and 1,4-dioxane, commonly known as "emerging contaminants."

Findings obtained from the completed/approved Site Characterization activities will be used to develop a site-specific Remedial Action Plan (RAP). The RAP will present the remedial alternatives available for implementation and a cost/benefit analysis will be used to select an appropriate remedy. The RAP will identify the appropriate remedial activities and controls selected for implementation during Site redevelopment.

<u>Fee</u>

We understand the City will calculate and advise us of the application fee.

Conclusion

We request that this matter be placed on the next available agenda and look forward to your review.



Respectfully submitted,

LaBella Associates

Michael Woollen, AIA, LEED AP

Nihe Woollen

Vice President, National PLAY Studio Leader

CC: Russ Wheeler

Alexsis Blakely Cristian Petschen Darnel Leader

Stuart Mesinger, AICP John Szarowski, PE

Application Form Municipal Coastal Site Plan Review For Projects Located Fully or Partially Within the Coastal Boundary

Please complete this form in accordance with the attached instructions and submit it with the appropriate plans to appropriate **municipal agency**.

Section I: Applicant Identification

| Applicant: | Date: |
|---|---------------------------------------|
| Address: | Phone: |
| Project Address or | |
| Location: | |
| Interest in Property: Γ fee simple Γ option Γ lessee Γ easement | |
| Γ other (specify) | |
| List primary contact for correspondence if other than applicant: | |
| Name: | · · · · · · · · · · · · · · · · · · · |
| Address: | ···· |
| City/Town: State: | |
| Code: | |
| Business Phone: | |
| e-mail: | |
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Section II: Project Site Plans

Please provide project site plans that clearly and accurately depict the following information, and check the appropriate boxes to indicate that the plans are included in this application:

- Γ Project location
- Γ Existing and proposed conditions, including buildings and grading
- Γ Coastal resources on and contiguous to the site
- Γ High tide line [as defined in CGS Section 22a-359(c)] and mean high water mark elevation contours (for parcels abutting coastal waters and/or tidal wetlands only)
- Γ Soil erosion and sediment controls
- Γ Stormwater treatment practices
- Γ Ownership and type of use on adjacent properties
- Γ Reference datum (i.e., National Geodetic Vertical Datum, Mean Sea Level, etc.)

Section III: Written Project Information

Please check the appropriate box to identify the plan or application that has resulted in this Coastal Site Plan Review: $\Gamma \text{ Site Plan for Zoning Compliance}$

 Γ Subdivision or Resubdivision

 Γ Special Permit or Special Exception

 Γ Variance

Γ Municipal Project (CGS Section 8-24)

Part I: Site Information

| 1. | Street Add | ress or Geographical Description: |
|----|---------------|---|
| | City or Tov | vn: |
| 2. | Is project of | or activity proposed at a waterfront site (includes tidal wetlands frontage)? Γ YES Γ NO |
| 3. | Name of o | n-site, adjacent or downstream coastal, tidal or navigable waters, if applicable: |
| 4. | | d describe the existing land use on and adjacent to the site. Include any existing municipal zoning classification, significant features of the project site: |
| | | |
| 5. | Indicate th | e area of the project site: acres or square feet (circle one) |
| 6. | Check the | appropriate box below to indicate total land area of disturbance of the project or activity |
| | (please als | so see Part II.B. regarding proposed stormwater best management practices): |
| | Γ | Project or activity will disturb 5 or more total acres of land area on the site. It may be |
| | | eligible for registration for the Department of Environmental Protection's (DEP) General |
| | | Permit for the Discharge of Stormwater and Dewatering Wastewaters Associated with |
| | | Construction Activities |
| | Γ | Project or activity will disturb one or more total acres but less than 5 total acres of land |
| | | area. A soil erosion and sedimentation control plan must be submitted to the municipal |
| | | land use agency reviewing this application. |
| | Γ | Project or activity will not disturb 1 acre total of land area. Stormwater management |
| | | controls may be required as part of the coastal site plan review. |
| 7. | Does the p | roject include a shoreline flood and erosion control structure as defined in CGS section |
| | 22a-109(d |) □ Yes □ No |

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Part II.A.: Description of Proposed Project or Activity

| | ribe the proposed project or activity including its purpose and related activities such as site clearing, |
|---------------------------------|---|
| • | ng, demolition, and other site preparations; percentage of increase or decrease in impervious cover |
| | existing conditions resulting from the project; phasing, timing and method of proposed construction; |
| and | new uses and changes from existing uses (attach additional pages if necessary): |
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Part III: Identification of Applicable Coastal Resources and Coastal Resource Policies

Identify the coastal resources and associated policies that apply to the project by placing a check mark in the appropriate box(es) in the following table.

| Coastal Resources | On-site | Adjacent | Off-site but within the influence of project | Not Applicable |
|--|---------|----------|--|-------------------|
| General Coastal Resources* - Definition: CGS Section 22a-93(7); Policy: CGS Section 22a-92(a)(2) | X | x | X | |
| Beaches & Dunes - Definition: CGS Section 22a-93(7)(C); Policies: CGS Sections 22a-92-(b)(2)(C) and 22a-92(c)(1)(K) | | | | |
| Bluffs & Escarpments - Definition: CGS Section 22a-93(7)(A); Policy: CGS Section 22a-92(b)(2)(A) | | | | |
| Coastal Hazard Area - Definition: CGS Section 22a-93(7)(H); Policies: CGS Sections 22a-92(a)(2), 22a-92(a)(5), 22a-92(b)(2)(F), 22a-92(b)(2)(J), and 22a-92(c)(2)(B) | | | | |
| Coastal Waters, Estuarine Embayments, Nearshore Waters, Offshore Waters - Definition: CGS Sections 22a-93(5), 22a-93(7)(G), and 22a-93(7)(K), and 22a-93(7)(L) respectively; Policies: CGS Sections 22a-92(a)(2) and 22a-92(c)(2)(A) | | | | |
| Developed Shorefront - Definition: CGS Section 22a-93(7)(I); Policy: 22a-92(b)(2)(G) | | | | |
| Freshwater Wetlands and Watercourses - Definition: CGS Section 22a-93(7)(F); Policy: CGS Section 22a-92(a)(2) | | | | |
| Intertidal Flats - Definition: CGS Section 22a-93(7)(D); Policies: 22a-92(b)(2)(D) and 22a-92(c)(1)(K) | | | | |
| Islands - Definition: CGS Section 22a-93(7)(J); Policy: CGS Section 22a-92(b)(2)(H) | | | | |
| Rocky Shorefront - Definition: CGS Section 22a-93(7)(B); Policy: CGS Section 22a-92(b)(2)(B) | | | | |
| Shellfish Concentration Areas - Definition: CGS Section 22a-93(7)(N); Policy: CGS Section 22a-92(c)(1)(I) | | | | |
| Shorelands - Definition: CGS Section 22a-93(7)(M); Policy: CGS Section 22a-92(b)(2)(I) | | | | |
| Tidal Wetlands - Definition: CGS Section 22a-93(7)(E); Policies: CGS Sections 22a-92(a)(2), 22a-92(b)(2)(E), and 22a-92(c)(1)(B) | | | | |

^{*} General Coastal Resource policy is applicable to all proposed activities

Part IV: Consistency with Applicable Coastal Resource Policies and Standards

| Describe the location and condition of the coastal resources identified in Part III above and explain how the proposed project or activity is consistent with all of the applicable coastal resource policies and standards; also see adverse impacts assessment in Part VII.A below (attach additional pages if necessary): |
|--|
| |
| |
| |

Part V: Identification of Applicable Coastal Use and Activity Policies and Standards

| Identify all coastal policies and standards in or referenced by CGS Section 22a-92 applicable to the |
|--|
| proposed project or activity: |
| X General Development* - CGS Sections 22a-92(a)(1), 22a-92(a)(2), and 22a-92(a)(9) |
| Water-Dependent Uses** - CGS Sections 22a-92(a)(3) and 22a-92(b)(1)(A); |
| Definition CGS Section 22a-93(16) |
| Ports and Harbors - CGS Section 22a-92(b)(1)(C) |
| Coastal Structures and Filling - CGS Section 22a-92(b)(1)(D) |
| Dredging and Navigation - CGS Sections 22a-92(c)(1)(C) and 22a-92(c)(1)(D) |
| Boating - CGS Section 22a-92(b)(1)(G) |
| Fisheries - CGS Section 22a-92(c)(1)(I) |
| Coastal Recreation and Access - CGS Sections 22a-92(a)(6), 22a-92(C)(1)(j) and 22a-92(c)(1)(K) |
| Sewer and Water Lines - CGS Section 22a-92(b)(1)(B) |
| Fuel, Chemicals and Hazardous Materials - CGS Sections 22a-92(b)(1)(C), 22a-92(b)(1)(E) and |
| 22a-92(c)(1)(A) |
| Transportation - CGS Sections 22a-92(b)(1)(F), 22a-92(c)(1)(F), 22a-92(c)(1)(G), and |
| 22a-92(c)(1)(H) |
| Solid Waste - CGS Section 22a-92(a)(2) |
| Dams, Dikes and Reservoirs - CGS Section 22a-92(a)(2) |
| Cultural Resources - CGS Section 22a-92(b)(1)(J) |
| Open Space and Agricultural Lands - CGS Section 22a-92(a)(2) |

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General Development policies are applicable to all proposed activities

^{**} Water-dependent Use policies are applicable to all activities proposed at waterfront sites, including those with tidal wetlands frontage.

Part VI: Consistency With Applicable Coastal Use Policies And Standards

| Explain how the proposed activity or use is consistent with all of the applicable coastal use and activity policies and standards identified in Part V. For projects proposed at waterfront sites (including those with tidal wetlands frontage), particular emphasis should be placed on the evaluation of the project's consistency with the water-dependent use policies and standards contained in CGS Sections 22a-92(a)(3) and 22a-92(b)(1)(A) also see adverse impacts assessment in Part VII.B below (attach additional pages if necessary): | |
|--|--|
| | |

Part VII.A.: Identification of Potential Adverse Impacts on Coastal Resources

Please complete this section for all projects.

Identify the adverse impact categories below that apply to the proposed project or activity. The Aapplicable≅ column **must** be checked if the proposed activity has the **potential** to generate any adverse impacts as defined in CGS Section 22a-93(15). If an adverse impact may result from the proposed project or activity, please use Part VIII to describe what project design features may be used to eliminate, minimize, or mitigate the potential for adverse impacts.

| Potential Adverse Impacts on Coastal Resources | Applicable | Not Applicable |
|--|------------|----------------|
| Degrading tidal wetlands, beaches and dunes, rocky shorefronts, and bluffs and escarpments through significant alteration of their natural characteristics or functions - CGS Section 22a-93(15)(H) | | |
| Increasing the hazard of coastal flooding through significant alteration of shoreline configurations or bathymetry, particularly within high velocity flood zones - CGS Section 22a-93(15)(E) | | |
| Degrading existing circulation patterns of coastal water through the significant alteration of patterns of tidal exchange or flushing rates, freshwater input, or existing basin characteristics and channel contours - CGS Section 22a-93(15)(B) | | |
| Degrading natural or existing drainage patterns through the significant alteration of groundwater flow and recharge and volume of runoff - CGS Section 22a-93(15)(D) | | |
| Degrading natural erosion patterns through the significant alteration of littoral transport of sediments in terms of deposition or source reduction - CGS Section 22a-93(15)(C) | | |
| Degrading visual quality through significant alteration of the natural features of vistas and view points - CGS Section 22a-93(15)(F) | | |
| Degrading water quality through the significant introduction into either coastal waters or groundwater supplies of suspended solids, nutrients, toxics, heavy metals or pathogens, or through the significant alteration of temperature, pH, dissolved oxygen or salinity - CGS Section 22a-93(15)(A) | | |
| Degrading or destroying essential wildlife, finfish, or shellfish habitat through significant alteration of the composition, migration patterns, distribution, breeding or other population characteristics of the natural species or significant alterations of the natural components of the habitat - CGS Section 22a-93(15)(G) | | |

Part VII.B.: Identification of Potential Adverse Impacts on Water-dependent Uses

Please complete the following two sections only if the project or activity is proposed at a waterfront site:

1. Identify the adverse impact categories below that apply to the proposed project or activity. The Aapplicable≅ column must be checked if the proposed activity has the potential to generate any adverse impacts as defined in CGS Section 22a-93(17). If an adverse impact may result from the proposed project or activity, use Part VIII to describe what project design features may be used to eliminate, minimize, or mitigate the potential for adverse impacts.

| Potential Adverse Impacts on Future Water-dependent Development Opportunities and Activities | Applicable | Not Applicable |
|--|------------|-------------------|
| Locating a non-water-dependent use at a site physically suited for or planned for location of a water-dependent use - CGS Section 22a-93(17) | | |
| Replacing an existing water-dependent use with a non-water-dependent use - CGS Section 22a-93(17) | | |
| Siting a non-water-dependent use which would substantially reduce or inhibit existing public access to marine or tidal waters - CGS Section 22a-93(17) | | |

2. Identification of existing and/or proposed Water-dependent Uses

| Describe the features or characteristics of the proposed activity or project that qualify as water-dependent uses as defined in CGS Section 22a-93(16). If general public access to coastal waters is provided, please identify the legal mechanisms used to ensure public access in perpetuity, and describe any provisions for parking or other access to the site and proposed amenities associated with the access (e.g., boardwalk, benches, trash receptacles, interpretative signage, etc.)*: | | | | | | | | |
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^{*}If there are no water-dependent use components, describe how the project site is not appropriate for the development of a water-dependent use.

Part VIII: Mitigation of Potential Adverse Impacts

| | tential adverse impacts on coastal resources and/or future water-dependent |
|-------------------------------------|--|
| | ortunities and activities identified in Part VII have been avoided, eliminated, or additional pages if necessary): |
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| art IX: Remain | ning Adverse Impacts |
| Explain why any re | emaining adverse impacts resulting from the proposed activity or use have not been |
| Explain why any re | emaining adverse impacts resulting from the proposed activity or use have not been the project as proposed is consistent with the Connecticut Coastal Management Act |
| Explain why any remitigated and why | emaining adverse impacts resulting from the proposed activity or use have not been the project as proposed is consistent with the Connecticut Coastal Management Act |
| Explain why any remitigated and why | emaining adverse impacts resulting from the proposed activity or use have not been the project as proposed is consistent with the Connecticut Coastal Management Act |
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Coastal Site Plan Application Attachment 1

Identification of Applicable Coastal Use and Activity Policies and Standards and Discussion of Consistency With Such Standards

1. General Development

a. CGS Section 22a-92(a)(1) To ensure that the development, preservation or use of the land and water resources of the coastal area proceeds in a manner consistent with the rights of private property owners and the capability of the land and water resources to support development, preservation or use without significantly disrupting either the natural environment or sound economic growth.

Discussion: The project is consistent with City zoning and does not impede on private property owner rights. The project will revitalize an abandoned and underused site and will result in clean-up of contaminated soils, thus improving the environment.

b. CGS Section 22a-92(a)(2) To preserve and enhance coastal resources in accordance with the policies established by chapters 439, 440, 446i, 446k, 447, 474 and 477.

Discussion: The project is consistent with these policies.

c. CGS Section22a-92(a)(9) To give high priority and preference to uses and facilities which are dependent upon proximity to the water or the shorelands immediately adjacent to marine and tidal waters;

Discussion: The project will take advantage of the site's proximity to the Pequonock River by providing views to the River from the stadium and by outdoor play activities and the brewpub in proximity to the river.

2. Sewer and Water Lines

a. CGS Section 22a-92(b)(1)(B) to locate and phase sewer and water lines so as to encourage concentrated development in areas which are suitable for development; and to disapprove extension of sewer and water services into developed and undeveloped beaches, barrier beaches and tidal wetlands except that, when necessary to abate existing sources of pollution, sewers that will accommodate existing uses with limited excess capacity may be used.

Discussion: The site is served by existing water and sewer lines. These lines will be removed and new lines installed. There will be no extension of water and sewer lines into other areas.

3. Transportation

a. CGS Section 22a-92(b)(1)(F) To make use of rehabilitation, upgrading and improvement of existing transportation facilities as the primary means of meeting transportation needs in the coastal area.

Discussion: A traffic study is currently underway. It is not anticipated that new transportation facilities will be required. If necessary, upgrades or improvements to existing transportation will be made to ensure that adequate levels of service are maintained.

4. Tidal Wetlands

a. CGS Section 22a-92(a)(2) To preserve and enhance coastal resources in accordance with the policies established by chapters 439, 440, 446i, 446k, 447, 474 and 477

Discussion: The project will not disturb and will preserve the tidal wetlands on the project site.

b. CGS Section 22a-92(b)(2)(E) to preserve tidal wetlands and to prevent the despoliation and destruction thereof in order to maintain their vital natural functions; to encourage the rehabilitation and restoration of degraded tidal wetlands and where feasible and environmentally acceptable, to encourage the creation of wetlands for the purposes of shellfish and finfish management, habitat creation and dredge spoil disposal.

Discussion: The project will preserve the tidal wetlands on the project site. It is not feasible to develop new wetlands for shellfish or finfish management on the site.

c. CGS Section 22a-92(c)(1)(B) to disallow any filling of tidal wetlands and nearshore, offshore and intertidal waters for the purpose of creating new land from existing wetlands and coastal waters which would otherwise be undevelopable, unless it is found that the adverse impacts on coastal resources are minimal.

Discussion: The project does not propose the filling of any wetlands.



WETLAND AND WATERCOURSE EVALUATION REPORT

Soccer Stadium and Mixed-Use Project

255 & 363 Kossuth Street & 83-153 Howe Street, Bridgeport, CT

Prepared for:

Mr. Stuart Mesinger **LaBella Associates**21 Fox Street

Poughkeepsie, NY 12601

Prepared by:

BL Companies 355 Research Parkway Meriden, CT 06450-7100

Date: September 29, 2023 BL Project No: 2301485

Sagan Simko, CPSS, PWS Senior Project Scientist II Wesley Wolf Senior Project Manager

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APPENDICES

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I. INTRODUCTION

A. PROJECT LOCATION AND DESCRIPTION

The proposed Project is for redevelopment of an existing dog track racing facility and two (2) adjacent parking areas, along with associated site improvements, situated on three (3) parcels in Bridgeport, CT containing a total of approximately 19.7 acres ("Project Area"). The Project Area is located at 255 and 363 Kossuth Street and 83-153 Howe Street, Bridgeport, CT (see **Appendix A, Figure 1**).

LaBella Associates ("Client") has contracted BL Companies ("BL") to characterize existing wetlands and watercourses that may be affected by the Project and describe the habitats and major vegetative cover types within the study area. BL conducted wetland and watercourse field delineations within a study area defined by the Client (see Appendix A) on September 6 & 18, 2023. This study area included the entire 19.7-acre area described above. Investigations were conducted to identify, and delineate if present, the extent and location of jurisdictional wetlands and "Waters of the U.S." within the Project Area pursuant to the Federal Clean Water Act (Sections 401 and 404), and Connecticut regulated activities in non-tidal wetlands regulated under Section 22a-38(15) of the Connecticut General Statutes (CGS). In conjunction with U.S. Army Corps of Engineers (USACE), this program is administered by the Connecticut Department of Energy and Environmental Protection (CT DEEP). Jurisdictional wetlands were defined using the 1987 U.S. Army Corps of Engineers Wetland Delineation Manual (Environmental Laboratory 1987) and subsequent guidance documents including the Regional Supplement to the Corps of Engineers Wetland Delineation Manual: Northcentral and Northeast Region (Version 2.0) (US Corps of Engineers, January 2012). Waters of the U.S., which include all streams, adjacent wetlands, and other waterbodies, are defined in 33 CFR 328.3(a). Professional qualifications of the individual(s) involved in the performance of field surveys and preparation of this report are provided in Appendix D.

B. DESCRIPTION OF STUDY AREA

The Project Area is located at 255 and 363 Kossuth Street and 83-153 Howe Street, Bridgeport, CT.

The Project Area lies within the New England physiographic province, which is a mountainous area that has been subjected to Pleistocene glaciation. Structural features of this province include block-fault basins, large intrusive igneous masses, and shoreline cliffs. (NPS, 2017).

II. METHODOLOGY

A. RECORDS RESEARCH

A desktop analysis of the study area was conducted prior to performing field surveys and included the entire defined area of investigation. Data reviewed included aerial photography, US Geological Survey 7.5-Minute Topographic Quadrangle Maps, US Fish and Wildlife Service (USFWS) National Wetland Inventory Maps (NWI), Flood Insurance Rate Maps (FIRM) provided by the Federal Emergency Management Administration (FEMA), Connecticut's Geographic Information Systems Open Data Website, and soil information from the United States Department of Agriculture (USDA) Natural Resources Conservation Service (NRCS). Other sensitive resource data were reviewed as available. This compiled data was used during field investigations and the subsequent report.

B. FIELD INVESTIGATION

Field investigations were conducted to verify records research and identify land use and plant communities within the Project Area, and to determine the presence or absence of wetland and watercourse features.

1. WETLAND AND WATERCOURSE DELINEATION

Investigations were conducted to identify, and delineate if present, the extent and location of jurisdictional wetlands and "Waters of the U.S." within the Project Area pursuant to the Federal Clean Water Act (Sections 401 and 404). In Connecticut, activities in non-tidal wetlands are regulated under Section 22a-38(15) of the Connecticut General Statutes (CGS), and activities in tidal wetlands are regulated under Section 22a-30-2(h). In conjunction with USACE, these programs are administered by the Connecticut Department of Energy and Environmental Protection (CT DEEP). Jurisdictional wetlands were defined using the 1987 U.S. Army Corps of Engineers Wetland Delineation Manual (Environmental Laboratory 1987) and subsequent guidance documents including the Regional Supplement to the Corps of Engineers Wetland Delineation Manual: Northcentral and Northeast Region (Version 2.0) (US Corps of Engineers, January 2012). Waters of the U.S., which include all streams, adjacent wetlands, and other waterbodies, are defined in 33 CFR 328.3(a). Connecticut state wetlands are defined as areas containing poorly drained soils, very poorly drained soils, and alluvial / floodplain soils (i.e., soils occurring along watercourses occupying nearly all level areas subject to periodic flooding).

When identified, wetland sampling was conducted along the gradient between wetland and adjacent upland areas to identify the location of the wetland boundary based upon the above criteria. Sample Points (and/or data points) were placed within selected locations of wetland areas to identify important, defining characteristics and to resolve obscure transitions between mixed wetlands and uplands. Visual estimates of percent vegetation cover by species, indicators of hydrology, and a soil profile were recorded on Wetland Determination Data Forms.

When identified, waterbody data collection included various physical parameters such as height of banks, top of bank to top of bank width, ordinary high water, water depth, presence of aquatics, substrate characteristics, and flow regime.

Mapping of any wetland boundaries and watercourse ordinary high-water marks ("OHWM") was supplemented using a Trimble[®] TDC150 Global Positioning System (GPS) unit with sub-foot accuracy.

2. WETLAND AND WATERCOURSE CLASSIFICATION

Identified wetlands were classified in accordance with the methods of Cowardin *et al.* (1979), which categorizes wetlands based on dominant (>30 percent cover within a single stratum) vegetation: palustrine emergent ("PEM"), palustrine scrub-shrub ("PSS"), palustrine forested ("PFO"), or some combination of these wetland types. Inundated features, such as ponds and lakes, were classified as palustrine unconsolidated bottom ("PUB"). Wetlands were also classified with the Hydrogeomorphic Method (HGM) of wetland classification (Brinson, 1993).

Hydrology was considered present when a minimum of one (1) primary or two (2) secondary indicators were identified. Indicators of wetland hydrology (saturated or inundated soils) along with signs of previous prolonged inundation within the upper 12 inches of the surface were noted at each sample location where observed. Other positive primary indicators of hydrology include high water table, watermarks, sediment deposits, drift deposits, algal mat or crust, iron deposits, inundation visible on aerial imagery, sparsely vegetated concave surface, water-stained leaves,

aquatic fauna, marl deposits, hydrogen sulfide odor, oxidized rhizospheres on living roots, presence of reduced iron, recent iron reduction in tilled soils, or thin muck surface. Additionally, secondary indicators of hydrology include surface soil cracks, drainage patterns, moss trim lines, dry-season water table, crayfish burrows, saturation visible on aerial imagery, stunted or stressed plants, geomorphic position, shallow aquitard, and microtopographic relief. A positive FAC-neutral test which was evaluated as a hydrophytic vegetation indicator is also considered a secondary indicator of hydrology.

Dominant species in a stratum (tree, shrub, herbaceous or vine) were determined by visually estimating the percent cover of each species within a plot of an approximately 30-foot (ft.) radius for trees, 15-ft. radius for saplings/shrubs, 5-ft. radius for herbs, and a 30-ft. radius for woody vines. Dominant vegetation was determined by the 50/20 Rule; by establishing the plant species that individually or collectively account for more than 50 percent of the total coverage of vegetation in the stratum, plus any other species that, by itself, accounts for at least 20 percent of the total. Species nomenclature and wetland indicator status follows that of the USACE National Wetland Plant List (2020, Version 3.5). Hydrophytic species are those wetland plants with an indicator status of OBL (obligate wetland), FACW (facultative wetland), or FAC (facultative). Species listed as FACU (facultative upland) or UPL (upland) are more indicative of upland areas and generally do not occur in wetlands. The hydrophytic vegetation criterion was determined to be present if the following tests were met including the Rapid Test, the Dominance Test or the Prevalence Index. All wetland habitats were classified according to the USFWS, and Classification of Wetlands and Deepwater Habitats of the United States (Cowardin *et al.* 1979).

As outlined in the National Technical Committee for Hydric Soils Version 8.2 (2018), soils were examined and sampled by using a hand auger or sharpshooter shovel to dig to a depth of approximately 16 to 20 inches or to refusal. Soil colors were determined using the 2010 Munsell® Soil Color Chart and taken while moist, or were wetted. Observations of redoximorphic (redox) concentrations, the apparent accumulation of iron (Fe) and manganese (Mn) oxides within the soil profile were noted as appropriate. Redox depletions, bodies of low chroma and value of four (4) or more where Fe-Mn oxides have been stripped were also noted, where observed. These features are usually an indication of periodic, seasonal, or permanent saturated soil conditions (Vepraskas 1994). Observations of hydric soil characteristics were based on the United States Department of Agriculture (USDA) textures, and hydric soil was considered present if one or more of the indicators were identified.

Biophysical elements such as a wetland's landscape position, geology, hydrology, substrate, and vegetation determine the wetland's functions and to what capacity they are performed. Due to the differing biophysical characteristics between on-site wetlands, the functions the wetlands provide and the capacity to perform those functions can vary. To better understand these differences, a description of the assessed wetland functions and values is completed based on the 1999 USACE Highway Methodology Workbook Supplement. This method requires describing each of the wetland communities and indicating the functions and values they provide. Biological, physical, chemical, and anthropogenic variables are all considered in the assessment. Wetland functions are defined as self-sustaining properties of a wetland ecosystem that exist in the absence of society. Wetland values are defined as benefits derived from one or more wetland functions and the physical characteristics that are associated with the wetland.

Field investigations also included the identification of watercourses based on flow regime: perennial (PER), intermittent (INT), or ephemeral (EPH). Perennial watercourses contain base flow supported with ground water throughout the year. Intermittent watercourses are those that contain base flow supported by ground water at least seasonally. Ephemeral waterbodies are primarily supported by precipitation. Watercourses were also classified in accordance with Cowardin *et al.* (1979). Riverine Systems include all wetlands and deep-water habitats contained

within a channel. A channel is defined as "an open conduit either naturally or artificially created which periodically or continuously contains moving water, or which forms a connecting link between two bodies of standing water." There are six (6) subsystems: Tidal, Lower Perennial, Upper Perennial, Intermittent, Unknown Perennial, and Ephemeral. Jurisdiction is ultimately determined through the USACE's Jurisdictional Determination process.

III. RESULTS

A. RECORDS RESEARCH

The USGS Bridgeport, Connecticut 7.5-Minute Topographic Quadrangle (see **Appendix A**, **Figure 2**), and Google Earth, indicate the Project Area has an elevation range between approximately 3 feet and 20 feet above mean sea level (AMSL).

According to the NRCS Web Soil Survey, one (1) soil series was identified within the Project Area. Table 1 includes the soil series and its physical characteristics and limitations. Soils mapping for the Project Area is provided in **Appendix A, Figure 3**.

Depth to **Hvdric Soil** Map Depth to Drainage Water Unit **Soil Unit Name** Components Restrictive Class Table Symbol Laver (inches) (%) (inches) 307 Urban land 0 N/A N/A N/A

Table 1. Soil Series within the Project Area

The Connecticut state wetlands mapping with integrated USFWS NWI wetlands indicated the presence of one (1) mapped feature within the Project Area: an Estuarine, Subtidal, Unconsolidated Bottom, Subtidal (E1UBL) estuary area (see **Appendix A, Figure 4**).

Review of the Federal Emergency Management Agency (FEMA) map indicates that the western boundary of the Project Area falls within Special Flood Hazard Areas, Zone AE (With BFE or Depth) and a regulatory Floodway. Approximately half of the Project Area falls within an Area of Minimal Flood Hazard, Zone X (see **Appendix A, Figure 5**).

Aerial photography indicates the study area is mainly comprised of paved parking areas, two (2) commercial sized buildings, a race track, maintained (mowed) lawn areas and shrubby areas. The commercial buildings are located in the central and southern portions of the Project Area. Shrubby areas exist along the western boundary of the Project Area as well as certain areas near the dog racing track (see **Appendix A, Figure 6**).

B. FIELD INVESTIGATION

Field observations reflected similar land use as observed during the desktop review.

Based on field observations, it has been determined that one (1) wetland area was present within and along the western boundary of the Project Area (see **Appendix A, Figure 7**). Field Data Location Mapping, photographs of the Project Area, and Wetland Determination Data Forms are provided in **Appendices A**, **B**, and **C**, respectively.

1. WETLANDS

One wetland area, Wetland A, was located within and along the western boundary of the Project Area. Wetland A is an Estuarine, Subtidal, Unconsolidated Bottom, Subtidal (E1UBL) estuary area, and flows north to south within and along the western boundary of the Project Area. The substrate of Wetland A consisted primarily of muck and sand, with cobble along the shoreline of the entire reach of Wetland A. The depth of the wetland varied at the time of investigation with slow flow. The wetland varied in width from 310 to 450 feet along the Project Area. Contributing flow to the wetland includes high ground water discharge from the surrounding areas, surface water runoff, and inputs from the Pequonnock River, located immediately north of the Project Area.

2. WATERCOURSES

No watercourses were observed within the Project Area during the time of the site reconnaissance.

C. FUNCTIONS & VALUES

The functions and values of Wetland A include ground water recharge/discharge, floodflow alteration, fish and shellfish habitat, sediment/toxicant retention, sediment/shoreline stabilization, and wildlife habitat. Nutrients and sediments from the adjacent commercial properties, as well as roadways, can be absorbed and retained within the wetland. This wetland also provides a contrasting habitat to the surrounding commercial and upland areas.

IV. SUMMARY

Based upon these observations and best professional judgement, it has been determined that one (1) wetland area (Wetland A) that constitutes a potential jurisdictional feature is located within/immediately adjacent to the Project Area.

The findings of this investigation represent a study of the proposed project for non-tidal wetlands and watercourses. This type of study depends on the time of year, the conditions at that time of year, site-specific influences (e.g., artificial disturbance), and individual professional judgment. It is, therefore, a professional estimate of the study area's wetlands and watercourses based upon available information and techniques.

The data that is the basis for this report is on file at BL Companies' Meriden, CT office.

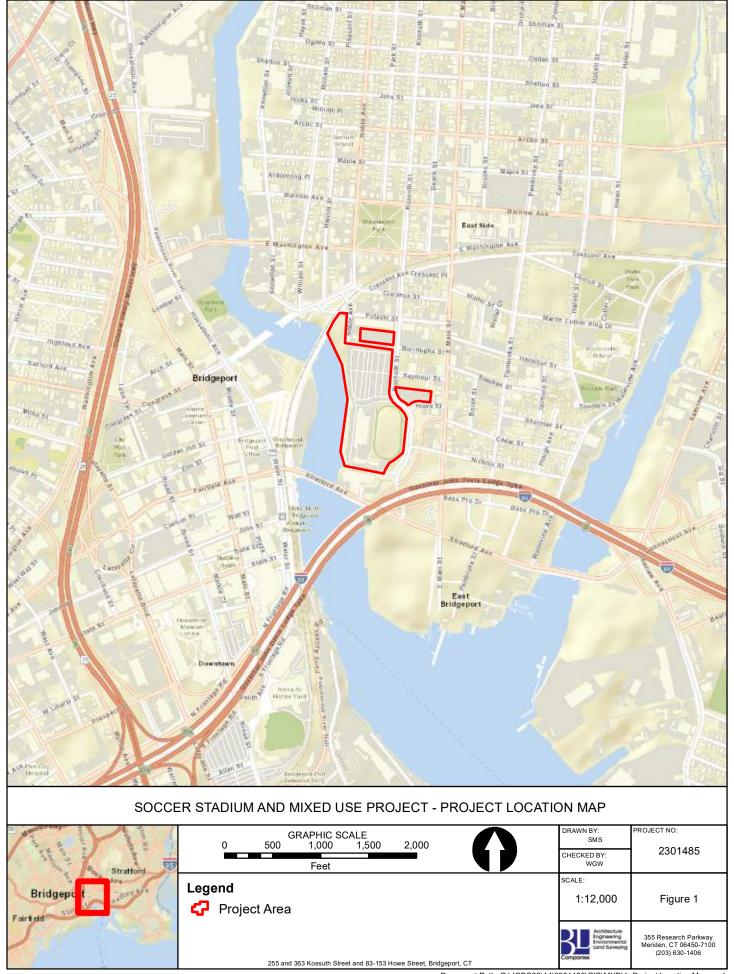
V. REFERENCES

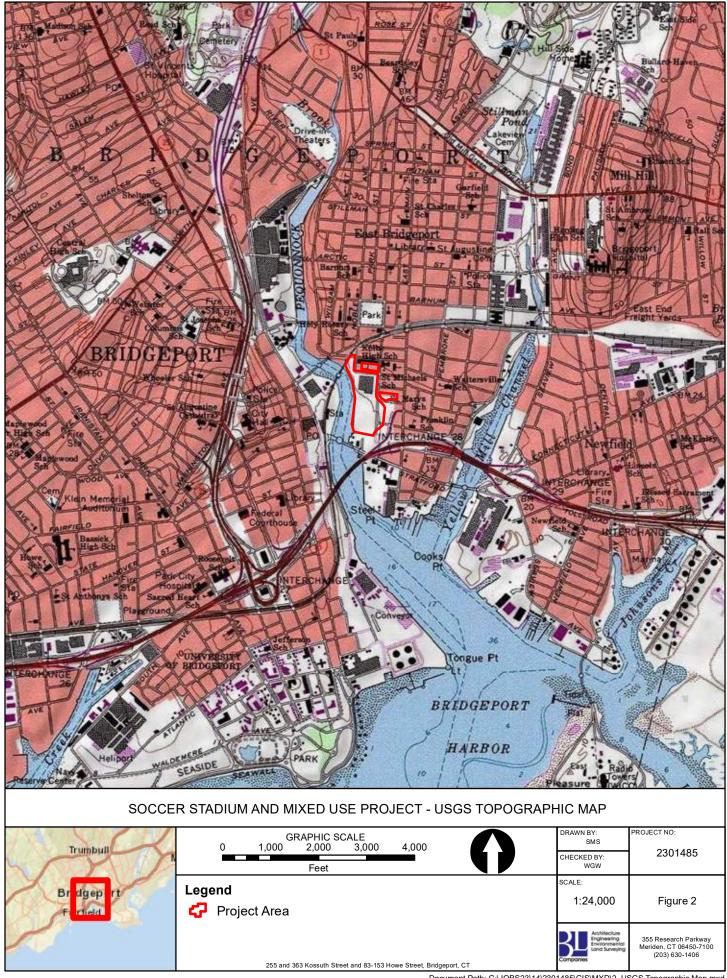
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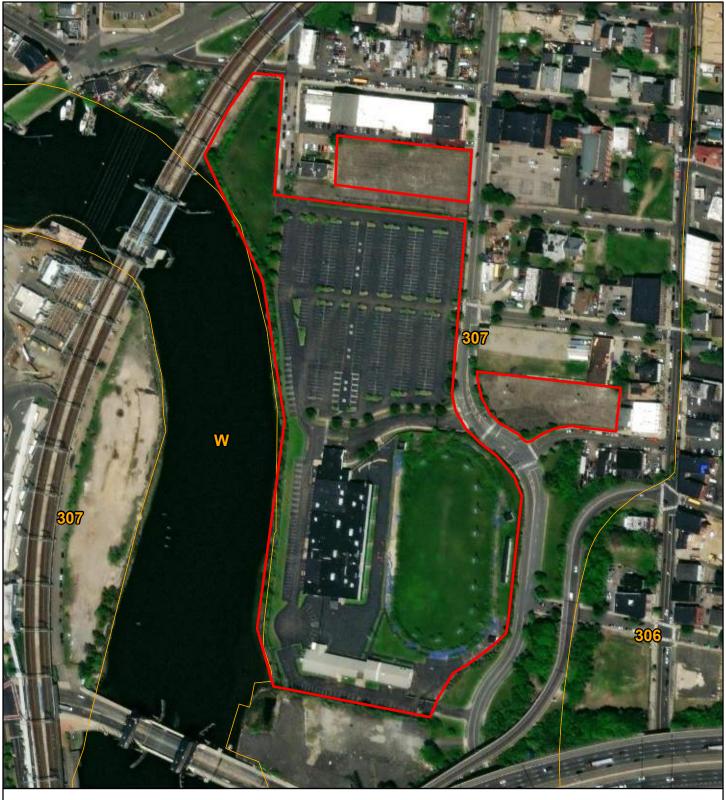
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APPENDIX A

Wetland and Watercourse Delineation Mapping







SOCCER STADIUM AND MIXED USE PROJECT - SOILS MAP



| | G | RAPHIC SO | CALE | |
|---|-----|-----------|------|-----|
| 0 | 125 | 250 | 375 | 500 |
| | | | | |
| | | Feet | | |



PROJECT NO: 2301485

Legend





Project Area Soils Type / Boundary

1:3,000

CHECKED BY: WGW

355 Research Parkway Meriden, CT 06450-7100 (203) 630-1406

Figure 3

255 and 363 Kossuth Street and 83-153 Howe Street, Bridgeport, CT



SOCCER STADIUM AND MIXED USE PROJECT - NATIONAL WETLAND INVENTORY & CT WETLANDS MAP

255 and 363 Kossuth Street and 83-153 Howe Street, Bridgeport, CT



| | G | RAPHIC SO | CALE | |
|---|-----|-----------|------|-----|
| 0 | 125 | 250 | 375 | 500 |
| | | | | |
| | | Feet | | |



PROJECT NO: 2301485 CHECKED BY: WGW SCALE:

Legend



Project Area



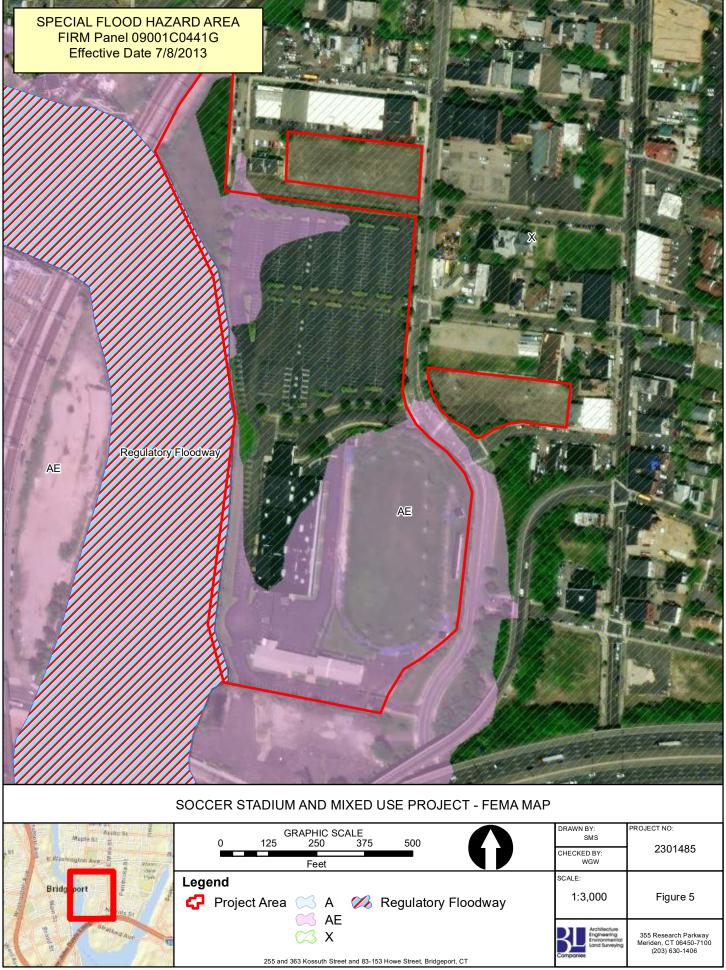
CT Wetlands (Soils)

NWI / CT Wetlands

1:3,000

355 Research Parkway Meriden, CT 06450-7100 (203) 630-1406

Figure 4





SOCCER STADIUM AND MIXED USE PROJECT - AERIAL IMAGERY MAP

255 and 363 Kossuth Street and 83-153 Howe Street, Bridgeport, CT



| | G | RAPHIC SO | CALE | |
|---|-----|-----------|------|-----|
| 0 | 125 | 250 | 375 | 500 |
| | | | | |
| | | Feet | | |

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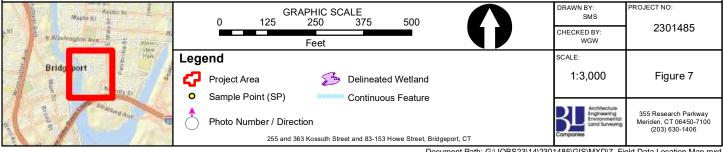
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Project Area

Architecture Engineering Environmental Land Surveying

355 Research Parkway Meriden, CT 06450-7100 (203) 630-1406





APPENDIX B

Color Photographs



Soccer Stadium & Mixed-Use Project Bridgeport, Connecticut Photographic Documentation

Photo #1

Date: September 6, 2023

Direction: North

Description

Northern view of Sample Point 1 in an herbaceous, upland point, located in the northwestern portion of the Project Area.



Photo # 2

Date: September 6, 2023

Direction: South

Description

Southern view of Sample Point 2 in an herbaceous, upland point, located in the central-western portion of the Project Area.





Soccer Stadium & Mixed-Use Project Bridgeport, Connecticut Photographic Documentation

Photo #3

Date: September 6, 2023 Direction: Northeast

Description

Northeastern view of Sample Point 3 in an herbaceous, upland point, located in the southeastern portion of the Project Area.



Photo #4

Date: September 18, 2023

Direction: North

Description

Northern view of the herbaceous, upland area, located within the dog track portion of the Project Area.





Soccer Stadium & Mixed-Use Project Bridgeport, Connecticut Photographic Documentation

Photo #5

Date: September 6, 2023

Direction: East

Description

Eastern view of parking lot area, located on the eastern side of Kossuth Road.



Photo #6

Date: September 6, 2023

Direction: West

Description

Western view of parking lot area, located on the western side of Kossuth Road.



APPENDIX C

Data Forms

WETLAND DETERMINATION DATA FORM - Northcentral and Northeast Region

| Project/Site: | Soccer Stadiun | n and Mixed-U | lse | City/County: | Bridgeport, Fairf | field County | Sampling D | ate: | 9/6/2023 |
|---------------------------------|--------------------|------------------|--------------------|---------------------|---------------------|----------------|------------------|-----------------|---------------|
| | | | | _ · · _ | State: | | | oint: | SP 1 |
| Investigator(s): | | | PWS | Section, To | wnship, Range: | | | | |
| Landform (hillslope, terrace, e | | | | | (concave, convex, | none): | None | Slope (%): | 0-1 |
| Subregion (LRR or MLRA): | | LRR R, MLI | | | 41.18339 | | | | |
| Soil Map Unit Name: | | , | Urban land (3 | | | | lassification: | | |
| Are climatic / hydrologic cond | itions on the site | typical for this | s time of year? | (Yes / No) | Yes | | explain in Rem | | |
| Are Vegetation No | | or Hydrology | • | ficantly disturbed? | | | tances" preser | - | X No |
| Are Vegetation No | ,Soil No | or Hydrology | No natur | ally problematic? | | (If needed, e | explain any ans | swers in Rem | arks.) |
| CUMMARY OF FIND | NOO Attac | | | | :4 4: | 4 | | 4 &4 | |
| SUMMARY OF FINDI | NGS - Attac | in site ma | p snowing s | sampling po | int locations | , transect | s, importa | int reature | es, etc. |
| | | | | | | | | | |
| Hydrophytic Vegetation Pres | ent? Yes | 3 | No X | | | | | | |
| Hydric Soil Present? | | | No X | Is the | Sampled Area | | | | |
| Wetland Hydrology Present? | Yes | | No X | | a Wetland? | Ye | es | No | X |
| , 0, | | | | | | | | | |
| Remarks: (Explain alternative | nrocoduros hor | ro or in a cona | rato roport) | | ır yes | , optional vve | tland Site ID: | | |
| Sample Point 1 is located | d within an herba | aceous, upland | d area located wi | ithin the northwes | tern portion of the | Project Area. | | | |
| HYDROLOGY | | | | | | | | | |
| Wetland hydrology Indi | cators: | | | | | Second | dary Indicators | (minimum of | two required) |
| Primary Indicators (minir | num of one is re | quired; check | all that apply) | | | 8 | Surface Soil Cr | acks (B6) | <u> </u> |
| Surface Water (A1 |) | | Water-Staine | d Leaves (B9) | | | Orainage Patte | rns (B10) | |
| High Water Table | (A2) | | Aquatic Fauna | a (B13) | | \ | Moss Trim Line | es (B16) | |
| Saturation (A3) | | | _ Marl Deposits | (B15) | | [| Ory-Season Wa | ater Table (C | 2) |
| Water Marks (B1) | | | Hydrogen Sul | fide Odor (C1) | | 0 | Crayfish Burrov | vs (C8) | |
| Sediment Deposits | s (B2) | | Oxidized Rhiz | ospheres on Livin | g Roots (C3) | s | Saturation Visil | ole on Aerial I | magery (C9) |
| Drift Deposits (B3) | | | Presence of F | Reduced Iron (C4) | | | Stunted or Stre | ssed Plants (| D1) |
| Algal Mat or Crust | (B4) | | Recent Iron R | eduction in Tilled | Soils (C6) | | Geomorphic Po | osition (D2) | |
| Iron Deposits (B5) | | | Thin Muck Su | rface (C7) | | | Shallow Aquita | rd (D3) | |
| Inundation Visible | on Aerial Image | ry (B7) | Other (Explain | n in Remarks) | | | //dicrotopograph | nic Relief (D4) |) |
| Sparsely Vegetate | _ | | _ ` ` | • | | | AC-Neutral Te | | |
| | | | | | | | | | |
| | | | | | | | | | |
| Field Observations: | | | | | | | | | |
| Surface Water Present? | Yes | No X | Depth (| inches): | | | | | |
| Water Table Present? | Yes | No X | Depth (| inches): | _ | | | | |
| Saturation Present? | Yes | No X | Depth (| inches): | Wetland | d Hydrology | Present? | Yes | No X |
| (includes capillary fringe) | | _ | | | _ | | | | |
| Describe Recorded Data (str | ream gauge, mo | nitoring well, a | aerial photos, pre | vious inspections |), if available: | | | | |
| | | _ | | • | | | | | |
| | | | | | | | | | |
| Remarks: | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
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| | | | | | | | | | |
| No primary or secondary | indicators were | present; there | fore, the hydrolo | gy criterion has no | ot been met. | | | | |
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US Army Corps of Engineers Northcentral and Northeast - Version 2.0

VEGETATION (Four Strata) - Use scientific names of plants.

| ree Stratum (Plot size: 30 ft.) | | | Dominance Test worksheet: |
|--|-------------------|----------|---|
| roo Stratum (Diataiza: 20 ft) | Absolute Dominan | | |
| | % cover Species? | Status | Number of Dominant Species |
| 1. None observed | | _ | That Are OBL, FACW, or FAC: (A) |
| 2 | | _ | |
| 3 | | | Total Number of Dominant |
| 4 | | <u> </u> | Species Across All Strata:1 (B) |
| 5 | | | |
| 6. | | | Percent of Dominant Species |
| 7. | | | That Are OBL, FACW, or FAC: 0 (A/B) |
| · | 0 = Total Cover | _ | (**=) |
| | | | Prevalence Index Worksheet: |
| sapling/Shrub Stratum (Plot size: 15 ft. | \ | | |
| | | NII | |
| 1. Elaeagnus umbellata | 10Yes | NI | |
| 2 | | | |
| 3 | | | FAC species 0 x 3 = 0 |
| 4 | | _ | FACU species 90 x 4 = 360 |
| 5 | | | UPL species 10 x 5 = 50 |
| 6 | | <u> </u> | Column Totals: (A) (B) |
| 7 | | <u></u> | |
| | 10 = Total Cover | | Prevalence Index = B/A = 4.10 |
| | | | |
| Herb Stratum (Plot size: 5 ft.) | | | Hydrophytic Vegetation Indicators: |
| 1. Poa pratensis | 80 Yes | FACU | 1 - Rapid Test for Hydrophytic Vegetation |
| 2. Daucus carota | 10 No | UPL | 2 - Dominance Test is >50% |
| 3. Taraxacum officinale | 10 No | FACU | 3 - Prevalence Index is ≤ 3.0¹ |
| | 10 110 | FACU | 4 - Morphological Adaptations ¹ (Provide supporting |
| 4 | | | |
| 5 | | | data in Remarks or on a separate sheet) |
| 6 | | | Problematic Hydrophytic Vegetation ¹ (Explain) |
| 7 | | | |
| 8 | | <u> </u> | ¹ Indicators of hydric soil and wetland hydrology must |
| 9 | | | be present, unless disturbed or problematic. |
| 0. | | <u> </u> | Definitions of Five Vegetation Strata: |
| 1. | | | Tree - Woody plants 3 in. (7.6 cm) or more in diameter |
| 2. | | | at breast height (DBH) regardless of height. |
| | 100 = Total Cover | | at 21 out 11 oignit (2 21.1) regulations of morginal |
| | | | Sapling/Shrub - Woody plants less than 3 in. DBH |
| M | | | and greater than or equal to 3.28 ft (1 m) tall. |
| Woody Vine Stratum (Plot size: 30 ft.) | | | and grouter than or equal to 0.25 ft (1 ff) tail. |
| | | | Herb - All herbaceous (non-woody) plants, regardless |
| | | | |
| | | | , , , , , |
| 2. | | | of size, and woody plants less than 3.28 ft tall. |
| 2. | | | of size, and woody plants less than 3.28 ft tall. |
| 2. | 0 = Total Cover | | , ,,, |
| 2. | 0 = Total Cover | | of size, and woody plants less than 3.28 ft tall. |
| 2. | 0 = Total Cover | | of size, and woody plants less than 3.28 ft tall. |
| 2. | 0 = Total Cover | | of size, and woody plants less than 3.28 ft tall. Woody vine - All woody vines greater than 3.28 ft in height. |
| 2. | 0 = Total Cover | | of size, and woody plants less than 3.28 ft tall. Woody vine - All woody vines greater than 3.28 ft in height. Hydrophytic Vegetation |
| 1. None observed 2 3 4 | 0 = Total Cover | | of size, and woody plants less than 3.28 ft tall. Woody vine - All woody vines greater than 3.28 ft in height. Hydrophytic Vegetation |
| 2 | 0 = Total Cover | | of size, and woody plants less than 3.28 ft tall. Woody vine - All woody vines greater than 3.28 ft in height. Hydrophytic Vegetation |
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| 2 | | | of size, and woody plants less than 3.28 ft tall. Woody vine - All woody vines greater than 3.28 ft in height. Hydrophytic Vegetation |

Sampling Point: SP 1

SOIL Sampling Point: SP 1

| Color (moist) % Color (moist) % Type¹ Loc² Texture Remarks 0.3 10YR 4/3 100 Silt Loam 3.18 10YR 5/3 100 Silt Loam Address of Problematic Hydric Soils³: Indicators for Problematic Hydric Soils³: Histosol (A1) Polyvalue Below Surface (S8) (LRR R, 2 cm Muck (A10) (LRR K, L, MLRA 149B) Black Histic (A3) Thin Dark Surface (S9) (LRR R, MLRA 149B) Some Sulfide (A4) Loamy Mucky Mineral (F1) (LRR K, L) Stratified Layers (A5) Loamy Gleyed Matrix (F2) Polyvalue Below Surface (S8) (LRR K, L) Depleted Below Dark Surface (A11) Depleted Matrix (F3) Sandy Mucky Mineral (S1) Depleted Dark Surface (F6) Sandy Mucky Mineral (S1) Depleted Dark Surface (F7) Sandy Mucky Mineral (S1) Redox Depressions (F8) Redox Depressions (F8) Mesic Spodic (TA6) (MLRA 144A, 145, 149 Sandy Redox (S5) Stripped Matrix (S4) Redox Depressions (F8) Mesic Spodic (TA6) (MLRA 144A, 145, 149 Sandy Redox (S5) This Dark Surface (F2) (LRR R, MLRA 149B) Mesic Spodic (TA6) (MLRA 144A, 145, 149 Sandy Redox (S5) Stripped Matrix (S4) Redox Depressions (F8) Redox Depressions (F8) Mesic Spodic (TA6) (MLRA 144A, 145, 149 Sandy Redox (S5) Dark Surface (S7) (LRR R, MLRA 149B) Mesic Spodic (TA6) (MLRA 144A, 145, 149 Sandy Redox (S5) Type: | Denth Matrix | Redox Features | | | |
|--|---|--|------------------|-----------------------|---------------------------------------|
| 9.3 10YR 4/3 100 Silt Loam 3-18 10YR 5/3 100 Silt Loam 3-18 10YR 5/3 100 Silt Loam 3-18 10YR 5/3 100 Silt Loam 3-18 Silt Loam | | | Loc ² | Texture | Remarks |
| ype: C=Concentration, D=Depletion, RM=Reduced Matrix, MS=Masked Sand Grains. Variable Variable | | olor (molect) 70 | | | romano |
| ype: C=Concentration, D=Depletion, RM=Reduced Matrix, MS=Masked Sand Grains. PL=Pore Lining, M=Matrix. | | | | | |
| Artic Soils Indicators: Histosol (A1) Polyvalue Below Surface (S8) (LRR R, Histosol (A2) MLRA 149B) Coast Prairie Redox (A16) (LRR K, L, MLRA 149B) Black Histic Epipedon (A2) Black Histic (A3) Thin Dark Surface (S9) (LRR R, MLRA 149B) Thin Dark Surface (S9) (LRR R, MLRA 149B) Stratified Layers (A5) Loamy Mucky Mineral (F1) (LRR K, L) Depleted Below Dark Surface (A11) Depleted Below Dark Surface (A11) Depleted Below Dark Surface (A12) Sandy Mucky Mineral (S1) Sandy Mucky Mineral (S1) Sandy Gleyed Matrix (S4) Sandy Gleyed Matrix (S4) Sandy Gleyed Matrix (S4) Sandy Gleyed Matrix (S4) Sandy Redox (S5) Stripped Matrix (S6) Dark Surface (A12) Sandy Redox (S5) Stripped Matrix (S6) Dark Surface (S9) (LRR K, L) Wery Shallow Dark Surface (F22) Dark Surface (S7) (LRR R, MLRA 149B) Are Parent Material (F12) Depleted Dark Surface (S7) (LRR R, MLRA 149B) Are personal material (F12) Depleted Dark Surface (S7) (LRR R, MLRA 149B) Are personal material (F12) Depleted Dark Surface (S7) (LRR R, MLRA 149B) Are personal material (F12) Depleted Dark Surface (S7) (LRR R, MLRA 149B) Are personal material (F12) Depleted Dark Surface (S7) (LRR R, MLRA 149B) Are personal material (F12) Depleted Dark Surface (S7) (LRR R, MLRA 149B) Are personal material (F12) Depleted Dark Surface (S7) (LRR R, MLRA 149B) Are personal material (F12) Depleted Dark Surface (F2) Depleted Dark Surface (F3) Depleted D | 3-16 101K 3/3 100 | | | Siit Luaiii | |
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| Artic Soils Indicators: Histosol (A1) Polyvalue Below Surface (S8) (LRR R, Histosol (A2) MLRA 149B) Coast Prairie Redox (A16) (LRR K, L, MLRA 149B) Black Histic Epipedon (A2) Black Histic (A3) Thin Dark Surface (S9) (LRR R, MLRA 149B) Thin Dark Surface (S9) (LRR R, MLRA 149B) Stratified Layers (A5) Loamy Mucky Mineral (F1) (LRR K, L) Depleted Below Dark Surface (A11) Depleted Below Dark Surface (A11) Depleted Below Dark Surface (A12) Sandy Mucky Mineral (S1) Sandy Mucky Mineral (S1) Sandy Gleyed Matrix (S4) Sandy Gleyed Matrix (S4) Sandy Gleyed Matrix (S4) Sandy Gleyed Matrix (S4) Sandy Redox (S5) Stripped Matrix (S6) Dark Surface (A12) Sandy Redox (S5) Stripped Matrix (S6) Dark Surface (S9) (LRR K, L) Wery Shallow Dark Surface (F22) Dark Surface (S7) (LRR R, MLRA 149B) Are Parent Material (F12) Depleted Dark Surface (S7) (LRR R, MLRA 149B) Are personal material (F12) Depleted Dark Surface (S7) (LRR R, MLRA 149B) Are personal material (F12) Depleted Dark Surface (S7) (LRR R, MLRA 149B) Are personal material (F12) Depleted Dark Surface (S7) (LRR R, MLRA 149B) Are personal material (F12) Depleted Dark Surface (S7) (LRR R, MLRA 149B) Are personal material (F12) Depleted Dark Surface (S7) (LRR R, MLRA 149B) Are personal material (F12) Depleted Dark Surface (S7) (LRR R, MLRA 149B) Are personal material (F12) Depleted Dark Surface (F2) Depleted Dark Surface (F3) Depleted D | | | | | _ |
| Artic Soils Indicators: Histosol (A1) Polyvalue Below Surface (S8) (LRR R, Histosol (A2) MLRA 149B) Coast Prairie Redox (A16) (LRR K, L, MLRA 149B) Black Histic Epipedon (A2) Black Histic (A3) Thin Dark Surface (S9) (LRR R, MLRA 149B) Thin Dark Surface (S9) (LRR R, MLRA 149B) Stratified Layers (A5) Loamy Mucky Mineral (F1) (LRR K, L) Depleted Below Dark Surface (A11) Depleted Below Dark Surface (A11) Depleted Below Dark Surface (A12) Sandy Mucky Mineral (S1) Sandy Mucky Mineral (S1) Sandy Gleyed Matrix (S4) Sandy Gleyed Matrix (S4) Sandy Gleyed Matrix (S4) Sandy Gleyed Matrix (S4) Sandy Redox (S5) Stripped Matrix (S6) Dark Surface (A12) Sandy Redox (S5) Stripped Matrix (S6) Dark Surface (S9) (LRR K, L) Wery Shallow Dark Surface (F22) Dark Surface (S7) (LRR R, MLRA 149B) Are Parent Material (F12) Depleted Dark Surface (S7) (LRR R, MLRA 149B) Are personal material (F12) Depleted Dark Surface (S7) (LRR R, MLRA 149B) Are personal material (F12) Depleted Dark Surface (S7) (LRR R, MLRA 149B) Are personal material (F12) Depleted Dark Surface (S7) (LRR R, MLRA 149B) Are personal material (F12) Depleted Dark Surface (S7) (LRR R, MLRA 149B) Are personal material (F12) Depleted Dark Surface (S7) (LRR R, MLRA 149B) Are personal material (F12) Depleted Dark Surface (S7) (LRR R, MLRA 149B) Are personal material (F12) Depleted Dark Surface (F2) Depleted Dark Surface (F3) Depleted D | | | | | |
| Artic Soils Indicators: Histosol (A1) Polyvalue Below Surface (S8) (LRR R, Histosol (A2) MLRA 149B) Coast Prairie Redox (A16) (LRR K, L, MLRA 149B) Black Histic Epipedon (A2) Black Histic (A3) Thin Dark Surface (S9) (LRR R, MLRA 149B) Thin Dark Surface (S9) (LRR R, MLRA 149B) Stratified Layers (A5) Loamy Mucky Mineral (F1) (LRR K, L) Depleted Below Dark Surface (A11) Depleted Below Dark Surface (A11) Depleted Below Dark Surface (A12) Sandy Mucky Mineral (S1) Sandy Mucky Mineral (S1) Sandy Gleyed Matrix (S4) Sandy Gleyed Matrix (S4) Sandy Gleyed Matrix (S4) Sandy Gleyed Matrix (S4) Sandy Redox (S5) Stripped Matrix (S6) Dark Surface (A12) Sandy Redox (S5) Stripped Matrix (S6) Dark Surface (S9) (LRR K, L) Wery Shallow Dark Surface (F22) Dark Surface (S7) (LRR R, MLRA 149B) Are Parent Material (F12) Depleted Dark Surface (S7) (LRR R, MLRA 149B) Are personal material (F12) Depleted Dark Surface (S7) (LRR R, MLRA 149B) Are personal material (F12) Depleted Dark Surface (S7) (LRR R, MLRA 149B) Are personal material (F12) Depleted Dark Surface (S7) (LRR R, MLRA 149B) Are personal material (F12) Depleted Dark Surface (S7) (LRR R, MLRA 149B) Are personal material (F12) Depleted Dark Surface (S7) (LRR R, MLRA 149B) Are personal material (F12) Depleted Dark Surface (S7) (LRR R, MLRA 149B) Are personal material (F12) Depleted Dark Surface (F2) Depleted Dark Surface (F3) Depleted D | | | | | |
| Artic Soils Indicators: Histosol (A1) Polyvalue Below Surface (S8) (LRR R, Histosol (A2) MLRA 149B) Coast Prairie Redox (A16) (LRR K, L, MLRA 149B) Black Histic Epipedon (A2) Black Histic (A3) Thin Dark Surface (S9) (LRR R, MLRA 149B) Thin Dark Surface (S9) (LRR R, MLRA 149B) Stratified Layers (A5) Loamy Mucky Mineral (F1) (LRR K, L) Depleted Below Dark Surface (A11) Depleted Below Dark Surface (A11) Depleted Below Dark Surface (A12) Sandy Mucky Mineral (S1) Sandy Mucky Mineral (S1) Sandy Gleyed Matrix (S4) Sandy Gleyed Matrix (S4) Sandy Gleyed Matrix (S4) Sandy Gleyed Matrix (S4) Sandy Redox (S5) Stripped Matrix (S6) Dark Surface (A12) Sandy Redox (S5) Stripped Matrix (S6) Dark Surface (S9) (LRR K, L) Wery Shallow Dark Surface (F22) Dark Surface (S7) (LRR R, MLRA 149B) Are Parent Material (F12) Depleted Dark Surface (S7) (LRR R, MLRA 149B) Are personal material (F12) Depleted Dark Surface (S7) (LRR R, MLRA 149B) Are personal material (F12) Depleted Dark Surface (S7) (LRR R, MLRA 149B) Are personal material (F12) Depleted Dark Surface (S7) (LRR R, MLRA 149B) Are personal material (F12) Depleted Dark Surface (S7) (LRR R, MLRA 149B) Are personal material (F12) Depleted Dark Surface (S7) (LRR R, MLRA 149B) Are personal material (F12) Depleted Dark Surface (S7) (LRR R, MLRA 149B) Are personal material (F12) Depleted Dark Surface (F2) Depleted Dark Surface (F3) Depleted D | Type: C=Concentration D=Depletion BM=Bod | used Matrix MS=Masked Sand Crains | 2l postion: DI - | -Doro Lining M-Matrix | |
| Histosol (A1) | | uced Matrix, MS-Masked Sand Grains. | LOCALION. PL- | | |
| Histic Epipedon (A2) Black Histic (A3) Thin Dark Surface (S9) (LRR R, MLRA 149B) Evaluation of the post of the | <u>-</u> | Deberatus Balance Confess (SQ) / DD D | | | |
| Black Histic (A3) | | ' | | | |
| Hydrogen Sulfide (A4) Loamy Mucky Mineral (F1) (LRR K, L) Stratified Layers (A5) Depleted Below Dark Surface (A11) Depleted Matrix (F2) Thick Dark Surface (A12) Sandy Mucky Mineral (S1) Sandy Mucky Mineral (S1) Sandy Gleyed Matrix (S4) Sandy Gleyed Matrix (S6) Dark Surface (S7) (LRR K, L) Polyvalue Below Surface (S8) (LRR K, L) Thin Dark Surface (S9) (LRR K, L) Iron-Manganese Masses (F12) (LRR K, L, L) Piedmont Floodplain Soils (F19) (MLRA 14 Sandy Gleyed Matrix (S4) Sandy Redox (S5) Stripped Matrix (S6) Dark Surface (S7) (LRR R, MLRA 149B) Soldicators of hydrophytic vegetation and wetland hydrology must be present, unless disturbed or problematic. Setrictive Layer (if observed): Type: Depth (inches): Hydric Soil Present? Yes No X | Histic Epipedon (A2) | • | | | |
| Stratified Layers (A5) | Black Histic (A3) | Thin Dark Surface (S9) (LRR R, MLRA | 149B) | 5 cm Mucky | Peat or Peat (S3) (LRR K, L, R |
| Depleted Below Dark Surface (A11) Depleted Matrix (F3) Thin Dark Surface (S9) (LRR K, L) Thick Dark Surface (A12) Redox Dark Surface (F6) Iron-Manganese Masses (F12) (LRR K, L, L, L, L) Sandy Mucky Mineral (S1) Depleted Dark Surface (F7) Piedmont Floodplain Soils (F19) (MLRA 14 Sandy Gleyed Matrix (S4) Sandy Redox (S5) Stripped Matrix (S6) Dark Surface (S7) (LRR R, MLRA 149B) Addicators of hydrophytic vegetation and wetland hydrology must be present, unless disturbed or problematic. Setrictive Layer (if observed): Type: Depth (inches): Hydric Soil Present? Yes No X | Hydrogen Sulfide (A4) | Loamy Mucky Mineral (F1) (LRR K, L) | | Dark Surface | e (S7) (LRR K, L) |
| Depleted Below Dark Surface (A11) Depleted Matrix (F3) Thin Dark Surface (S9) (LRR K, L) Thick Dark Surface (A12) Redox Dark Surface (F6) Iron-Manganese Masses (F12) (LRR K, L, L, L, L) Sandy Mucky Mineral (S1) Depleted Dark Surface (F7) Piedmont Floodplain Soils (F19) (MLRA 14 Sandy Gleyed Matrix (S4) Sandy Redox (S5) Stripped Matrix (S6) Dark Surface (S7) (LRR R, MLRA 149B) Addicators of hydrophytic vegetation and wetland hydrology must be present, unless disturbed or problematic. Setrictive Layer (if observed): Type: Depth (inches): Hydric Soil Present? Yes No X | Stratified Layers (A5) | Loamy Gleyed Matrix (F2) | | Polyvalue Be | low Surface (S8) (LRR K, L) |
| Thick Dark Surface (A12) Redox Dark Surface (F6) Iron-Manganese Masses (F12) (LRR K, L, I, I Sandy Mucky Mineral (S1) Depleted Dark Surface (F7) Piedmont Floodplain Soils (F19) (MLRA 144 Sandy Gleyed Matrix (S4) Redox Depressions (F8) Mesic Spodic (TA6) (MLRA 144A, 145, 149 Sandy Redox (S5) Red Parent Material (F12) Very Shallow Dark Surface (F22) Dark Surface (S7) (LRR R, MLRA 149B) Other (Explain in Remarks) Indicators of hydrophytic vegetation and wetland hydrology must be present, unless disturbed or problematic. Indicators of hydrophytic vegetation and wetland hydrology must be present, unless disturbed or problematic. Indicators of hydrophytic vegetation and wetland hydrology must be present, unless disturbed or problematic. Indicators of hydrophytic vegetation and wetland hydrology must be present, unless disturbed or problematic. Indicators of hydrophytic vegetation and wetland hydrology must be present, unless disturbed or problematic. Indicators of hydrophytic vegetation and wetland hydrology must be present, unless disturbed or problematic. Indicators of hydrophytic vegetation and wetland hydrology must be present, unless disturbed or problematic. Indicators of hydrophytic vegetation and wetland hydrology must be present, unless disturbed or problematic. Indicators of hydrophytic vegetation and wetland hydrology must be present, unless disturbed or problematic. Indicators of hydrophytic vegetation and wetland hydrology must be present, unless disturbed or problematic. Indicators of hydrophytic vegetation and wetland hydrology must be present, unless disturbed or problematic. | | | | | |
| Sandy Mucky Mineral (S1) Depleted Dark Surface (F7) Piedmont Floodplain Soils (F19) (MLRA 144 Sandy Gleyed Matrix (S4) Sandy Redox (S5) Stripped Matrix (S6) Dark Surface (S7) (LRR R, MLRA 149B) Addicators of hydrophytic vegetation and wetland hydrology must be present, unless disturbed or problematic. Setrictive Layer (if observed): Type: Depth (inches): Type: Depth (inches): Demarks: | | | | | . , . |
| Sandy Gleyed Matrix (S4) Redox Depressions (F8) Mesic Spodic (TA6) (MLRA 144A, 145, 149 Sandy Redox (S5) Red Parent Material (F12) Stripped Matrix (S6) Very Shallow Dark Surface (F22) Dark Surface (S7) (LRR R, MLRA 149B) Other (Explain in Remarks) Addicators of hydrophytic vegetation and wetland hydrology must be present, unless disturbed or problematic. Sestrictive Layer (if observed): Type: Depth (inches): Hydric Soil Present? Yes No X Pemarks: | | | | | |
| Sandy Redox (S5) Stripped Matrix (S6) Dark Surface (S7) (LRR R, MLRA 149B) Other (Explain in Remarks) diciators of hydrophytic vegetation and wetland hydrology must be present, unless disturbed or problematic. patrictive Layer (if observed): Type: Depth (inches): Depth (inches): Type: Depth (inches): Depth (inches): | | | | | . , , , |
| Stripped Matrix (S6) Dark Surface (S7) (LRR R, MLRA 149B) Other (Explain in Remarks) dicators of hydrophytic vegetation and wetland hydrology must be present, unless disturbed or problematic. estrictive Layer (if observed): Type: Depth (inches): Type: Depth (inches): Depth (inches): | | Redox Depressions (F8) | | | |
| Dark Surface (S7) (LRR R, MLRA 149B) Other (Explain in Remarks) Indicators of hydrophytic vegetation and wetland hydrology must be present, unless disturbed or problematic. Destrictive Layer (if observed): Type: Depth (inches): Depth (inches): Depth (sinches): Depth (sinche | Sandy Redox (S5) | | | Red Parent I | Material (F12) |
| adicators of hydrophytic vegetation and wetland hydrology must be present, unless disturbed or problematic. Type: Depth (inches): Hydric Soil Present? Yes No X emarks: | Stripped Matrix (S6) | | | Very Shallow | Dark Surface (F22) |
| Type: Depth (inches): Hydric Soil Present? Yes No X Pemarks: | Dark Surface (S7) (LRR R, MLRA 149B) | | | Other (Expla | in in Remarks) |
| Type: Depth (inches): Hydric Soil Present? Yes No X Pemarks: | | | | | |
| Type: Depth (inches): Hydric Soil Present? Yes No X Pemarks: | ndicators of hydrophytic vegetation and wetland | hydrology must be present, unless disturbed of | r problematic. | | |
| Type: Hydric Soil Present? Yes NoX emarks: | | | | | |
| Depth (inches): NoX emarks: | _ | | | | |
| emarks: | | | | ". B | N . V |
| | Depth (inches): | | Hydric Sc | on Present? Yes_ | NOX |
| | | | | | |
| No positive indication of hydric soils was observed. | | | l . | | |
| No positive indication of hydric soils was observed. | emarks: | | l . | | |
| No positive indication of hydric soils was observed. | emarks: | | - | | |
| to positive indication of rightic soils was observed. | emarks: | | 1 | | |
| | | | 1 | | |
| | | served. | | | |

WETLAND DETERMINATION DATA FORM - Northcentral and Northeast Region

| Project/Site: | Soccer Stadium and I | Mixed-Use | City/County: | Bridgeport, Fairfi | ield County | Sampling D | ate: | 9/6/2023 |
|---|---------------------------|--------------------------|------------------------|--------------------|---------------|------------------|-------------|---------------|
| Applicant/Owner: | LaBe | ella Associates, D.P.C |). | State: | СТ | Sample Po | int: | SP 2 |
| Investigator(s): | Sagan M. Simko, 0 | CPSS, PWS | Section, To | wnship, Range: | | | | |
| Landform (hillslope, terrace, e | etc.): | Terrace | Local relief | (concave, convex, | none): | None | Slope (%): | 0-1 |
| Subregion (LRR or MLRA): | LRF | R R, MLRA 144A | Lat: | 41.18127 | Long: | -73.18472 | Datum: | NAD83 |
| Soil Map Unit Name: | | Urban land | I (307) | | NWI C | lassification: | | None |
| Are climatic / hydrologic cond | itions on the site typica | I for this time of year? | ? (Yes / No) | Yes | (if no, e | explain in Rema | arks.) | |
| Are Vegetation No | ,Soil No ,or Hy | drology No sig | nificantly disturbed? | Are "Norr | mal Circumst | tances" presen | t? Yes | X No |
| Are Vegetation No | ,Soil No ,or Hy | drology No nat | turally problematic? | | (If needed, e | explain any ans | wers in Rem | arks.) |
| SUMMARY OF FINDI | MGS Attach eif | to man chowing | a camplina poi | int locations | transact | e importa | nt foatur | os oto |
| SOMINART OF FINDI | NGS - Attach Sit | e map snowing | g samping poi | iiit iocations, | lialisect | .s, illiporta | iii ieatui | es, etc. |
| | | | | | | | | |
| Hydrophytic Vegetation Pres | sent? Yes | No X | | | | | | |
| Hydric Soil Present? | Yes | No X | Is the S | Sampled Area | | | | |
| Wetland Hydrology Present? | | | | a Wetland? | Ye | es | No | X |
| | | | | If you | antional Ma | tland Site ID: | | |
| Remarks: (Explain alternative | nrocedures here or in | a senarate report) | | ıı yes, | optional we | tiand Site ID. | | |
| itemarks. (Explain alternative | , procedures here or in | a separate report) | | | | | | |
| HYDROLOGY Wetland hydrology Ind | icators: | | | | Sacono | dary Indicators | (minimum of | two required) |
| Primary Indicators (minir | | · abook all that apply) | | | | | | two required) |
| | | 11.27 | | | | Surface Soil Cra | ` ' | |
| Surface Water (A1 | • | | ned Leaves (B9) | | | Orainage Patter | | |
| High Water Table | (A2) | Aquatic Fat | | | | Moss Trim Line | | 2) |
| Saturation (A3) | | Marl Depos | | | | Ory-Season Wa | | 2) |
| Water Marks (B1) | | | Sulfide Odor (C1) | ~ Doots (C2) | | Crayfish Burrow | | Imagen (CO) |
| Sediment Deposits | | | hizospheres on Living | g Roots (C3) | | Saturation Visib | | |
| Drift Deposits (B3) | | | of Reduced Iron (C4) | 0-:1- (00) | | Stunted or Stres | | (וט |
| Algal Mat or Crust | • | | n Reduction in Tilled | Solls (C6) | | Geomorphic Po | | |
| Iron Deposits (B5) | | | Surface (C7) | | | Shallow Aquitar | | ` |
| | on Aerial Imagery (B7) | | lain in Remarks) | | | /licrotopograph | • |) |
| Sparsely Vegetate | d Concave Surface (B8 | ·) | | | F | AC-Neutral Te | est (D5) | |
| | | | | | | | | |
| Field Observations | | | | 1 | | | | |
| Field Observations: | V N- | V D | ul- (: l \). | | | | | |
| Surface Water Present? | Yes No No | | th (inches): | _ | | | | |
| Water Table Present? | Yes No No | | th (inches): | — Wetland | l Uudralaau | Brocont? | /oo | No. V |
| Saturation Present? (includes capillary fringe) | Yes No _ | X Dept | th (inches): | vvetiand | l Hydrology | Present? | res | _ NO |
| . , , , , , | | | | | | | | |
| Describe Recorded Data (st | ream gauge, monitoring | g well, aerial photos, p | previous inspections) |), if available: | | | | |
| | | | | | | | | |
| | | | | | | | | |
| Remarks: | | | | | | | | |
| | | | | | | | | |
| | | | | | | | | |
| | | | | | | | | |
| | | | | | | | | |
| No primary or secondary | indicators were preser | it; therefore, the hydro | ology criterion has no | ot been met. | | | | |
| | | | | | | | | |
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US Army Corps of Engineers Northcentral and Northeast - Version 2.0

VEGETATION (Four Strata) - Use scientific names of plants.

| | Absolute | Dominant | Indicator | Dominance Test worksheet: | - | |
|--|----------------|---------------|--------------|--|----------------------|--|
| ree Stratum (Plot size: 30 ft.) | % cover | Species? | Status | Number of Dominant Species | | |
| 1. Ailanthus altissima | 70 COVE | <u> </u> | UPL | That Are OBL, FACW, or FAC | : 0 | (A) |
| | | | <u> </u> | matric obe, triow, of trio | | (//) |
| 2 | | | | Total Number of Dominant | | |
| 3 | | | | Species Across All Strata: | 2 | (B) |
| | | | | Species Across Air Strata. | | (B) |
| 5 | | | - | Develop of Deminent Charles | | |
| 6 | | | - | Percent of Dominant Species That Are OBL, FACW, or FAC | . 0 | (A/D) |
| 7 | | T-1-1-0 | | That Are OBL, FACW, or FAC | : 0 | (A/B) |
| | 0 | = Total Cover | | Prevalence Index Worksheet | | |
| Sapling/Shrub Stratum (Plot size: 15 ft. | 1 | | | Total % Cover of: | | , by: |
| | <i>)</i> 10 | Yes | NI | OBL species 0 | Multiply x 1 = | 0 |
| 1. Elaeagnus umbellata | 5 | Yes | FACU | · - | | 0 |
| 2. Robinia pseudoacacia | | res | FACU | | | |
| 3 | | | | | | 0 |
| 4 | | | - | FACU species 105 | | 20 |
| 5 | | | - | UPL species 0 | | 0(D) |
| 6 | | | | Column Totals: 105 | (A)4 | (B) |
| 7 | 45 | T-t-1 0 | | Describer of leden - D/ | A - 4.04 | |
| | 15 | = Total Cover | | Prevalence Index = B/ | A = <u>4.00</u> | <u>, </u> |
| Herb Stratum (Plot size: 5 ft.) | | | | Hydrophytic Vegetation India | | |
| Herb Stratum (Plot size: 5 ft.) 1. Poa pratensis | 80 | Yes | FACIL | | | |
| 2. Trifolium repens | 10 | No | FACU FACU | 1 - Rapid Test for Hyd 2 - Dominance Test is | · · · | |
| · | | | - | 3 - Prevalence Index is | | |
| 3. <u>Taraxacum officinale</u> | 10 | No | FACU | | | unnartina |
| 4 | | | - | 4 - Morphological Ada | | |
| 5 | | | - | | or on a separate she | , |
| 6 | | | - | Problematic Hydrophy | tic vegetation (Exp | iain) |
| 7 | | | | 1 | | |
| 8 | | | | ¹ Indicators of hydric soil and w | | ıst |
| 9 | | | | be present, unless disturbed o | • | |
| 10 | | | | Definitions of Five Vegetatio | | |
| 11 | | | | Tree - Woody plants 3 in. (7.6 | • | neter |
| 12 | | | | at breast height (DBH) regard | ess of height. | |
| | 100 : | = Total Cover | | Continue/Observe NV - a describe esta | - I # 0 : DDI | |
| | | | | Sapling/Shrub - Woody plants | | 1 |
| Woody Vine Stratum (Plot size: 30 ft.) | | | | and greater than or equal to 3.2 | 28 π (1 m) tall. | |
| 1. None observed | | | | | | |
| 2 | | | | Herb - All herbaceous (non-wo | | ess |
| 3 | | | | of size, and woody plants less | than 3.28 ft tall. | |
| 4 | | | | | | |
| | 0 : | = Total Cover | | Woody vine - All woody vines | greater than 3.28 ft | in height. |
| | | | | | | |
| | | | | Hydrophytic | | |
| | | | | Vegetation | | |
| | | | | Present? Yes | NoX | |
| | | | | | | |
| Remarks: | | | | | | |
| | | | | | | |
| | | | | | | |

The hydrophytic vegetation criterion has not been met.

Sampling Point: SP 2

SOIL Sampling Point: SP 2

| Depth | Matrix | | | Redox F | | the absence of | , | |
|-------------------------|---------------------------|------------------|------------------|----------------|---------------------------|---------------------------|-------------------------|--|
| (inches) | Color (moist) | % (| Color (moist) | % | Type ¹ | Loc ² | Texture | Remarks |
| 0-3 | 10YR 4/3 | 100 | 20.0. (| | | | Silt Loam | riomanie |
| 3-15 | 10YR 5/3 | 95 | | | - | | Silt Loam | |
| 0 10 | 10YR 5/6 | 5 | | | | | Oilt Louin | |
| | 10110 3/0 | | | | | | | |
| | | | | | | | | |
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| | | | | | | | | |
| | | | | | | | | |
| | | | | | <u> </u> | | | |
| ¹ Type: C=C | Concentration, D=Depl | etion, RM=Red | duced Matrix, MS | S=Masked Sa | nd Grains. | ² Location: Pl | L=Pore Lining, M=Matrix | ζ. |
| Hydric Soil | s Indicators: | | | | | | | roblematic Hydric Soils ³ : |
| Histoso | ol (A1) | | Polyval | ue Below Sur | face (S8) (LRR R | | 2 cm Muck (| (A10) (LRR K, L, MLRA 149B) |
| | Epipedon (A2) | | | LRA 149B) | . , , | | | e Redox (A16) (LRR K, L, R) |
| | Histic (A3) | | | • | 9) (LRR R, MLR | \ 149R\ | | Peat or Peat (S3) (LRR K, L, R) |
| | | | | | | 1 1 4 3 6) | | |
| | gen Sulfide (A4) | | | • | ll (F1) (LRR K, L) | | | e (S7) (LRR K, L) |
| | ed Layers (A5) | 44.4.11 | | Gleyed Matrix | (F2) | | | elow Surface (S8) (LRR K, L) |
| | ed Below Dark Surface | e (A11) | | ed Matrix (F3) | | | | urface (S9) (LRR K, L) |
| | Dark Surface (A12) | | | Dark Surface | | | | nese Masses (F12) (LRR K, L, R) |
| | Mucky Mineral (S1) | | | ed Dark Surfa | ` ' | | | oodplain Soils (F19) (MLRA 149 |
| Sandy | Gleyed Matrix (S4) | | Redox | Depressions (| (F8) | | Mesic Spod | ic (TA6) (MLRA 144A, 145, 149B |
| Sandy | Redox (S5) | | | | | | Red Parent | Material (F12) |
| Strippe | ed Matrix (S6) | | | | | | Very Shallov | v Dark Surface (F22) |
| Dark S | urface (S7) (LRR R, N | /ILRA 149B) | | | | | Other (Expla | ain in Remarks) |
| | | | | | | | <u> </u> | |
| ³ Indicators | of hydrophytic vegetati | on and wetlan | d hydrology mus | t be present, | unless disturbed | or problematic. | | |
| Restrictive | Layer (if observed): | | , ,, | • | | | | |
| Tymor | | | | | | | | |
| Type: | | | | | | Hudria (| Soil Present? Yes | No. V |
| Deptii (ii | nches): | | | | | nyuncs | Soli Present? Tes_ | NoX |
| | | | | | | | | |
| Damada | | | | | | | | |
| Remarks: | | | | | | | | |
| Remarks: | | | | | | | | |
| Remarks: | | | | | | | | |
| | sitive indication of hvdr | ric soils was ol | oserved. | | | | | |
| | sitive indication of hydr | ic soils was ol | oserved. | | | | | |
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| | sitive indication of hydr | ic soils was ol | oserved. | | | | | |
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| | sitive indication of hydr | ic soils was ol | oserved. | | | | | |
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| | sitive indication of hydr | ic soils was ol | oserved. | | | | | |

WETLAND DETERMINATION DATA FORM - Northcentral and Northeast Region

| Project/Site: | Soccer Stadium and Mixed- | Jse Ci | ity/County: Bridge | port, Fairfi | eld County | Sampling D |)ate: | 9/6/2023 |
|---------------------------------|------------------------------------|--------------------------|--------------------------|--------------|---------------|----------------------------------|--------------|-----------------|
| Applicant/Owner: | LaBella As | sociates, D.P.C. | | State: | CT | Sample Po | oint: | SP 3 |
| Investigator(s): | Sagan M. Simko, CPSS, | PWS | Section, Township, | Range: | | | | |
| Landform (hillslope, terrace, | etc.): Terra | ice | Local relief (concav | e, convex, | none): | None | Slope (%): | 0-1 |
| Subregion (LRR or MLRA): | LRR R, MI | _RA 144A | Lat:41.1 | 8127 | Long: | -73.18472 | Datum: | NAD83 |
| Soil Map Unit Name: | | Urban land (307) | | | NWIC | lassification: | | None |
| Are climatic / hydrologic cond | ditions on the site typical for th | is time of year? | (Yes / No) | Yes | (if no, e | xplain in Rem | arks.) | |
| Are Vegetation No | Soil No ,or Hydrolog | y No significant | tly disturbed? | Are "Norn | mal Circumst | ances" preser | nt? Yes | X No |
| Are Vegetation No | ,Soil No ,or Hydrolog | y No naturally p | oroblematic? | | (If needed, e | explain any ans | swers in Rem | arks.) |
| STIMMADY OF EIND | INGS - Attach site ma | n chowing car | nling point lo | ations | transact | e imports | nt foatur | os oto |
| SUMMART OF FIND | INGS - Allacii Sile ilia | ip snowing sam | ipinig ponit iot | alions, | lianseci | s, illipulta | iiit ieatui | 55, ElG. |
| | | | | | | | | |
| Hydrophytic Vegetation Pres | sent? Yes | No X | | | | | | |
| Hydric Soil Present? | Yes | No X | Is the Sample | d Area | | | | |
| Wetland Hydrology Present | ? Yes | No X | within a Wetla | nd? | Ye | es | No | X |
| | | | | If you | ontional Wot | tland Site ID: | | |
| Remarks: (Eynlain alternative | e procedures here or in a sepa | arate report) | | ıı yes, | optional wei | lianu Sile ID. | | |
| remarks. (Explain alternative | 5 procedures here or in a sept | nate report) | | | | | | |
| HYDROLOGY Wetland hydrology Ind | licators: | | | | Second | lary Indicators | (minimum of | f two required) |
| Primary Indicators (mini | mum of one is required; check | (all that annly) | | | | Surface Soil Cr | | two required) |
| Surface Water (A | | Water-Stained Lea | aves (B9) | | | rainage Patte | ` ' | |
| High Water Table | · — | Aquatic Fauna (B1 | ` , | | | loss Trim Line | | |
| Saturation (A3) | | Marl Deposits (B15 | • | | | ry-Season Wa | | 2) |
| Water Marks (B1) | | Hydrogen Sulfide C | · | | | Crayfish Burrov | - | -/ |
| Sediment Deposit | | | neres on Living Roots | (C3) | | saturation Visil | | Imagery (C9) |
| Drift Deposits (B3 | · · | Presence of Reduc | = | () | | Stunted or Stre | | |
| Algal Mat or Crust | · — | | ction in Tilled Soils (C | 6) | | Geomorphic Po | | 2., |
| Iron Deposits (B5) | · · | Thin Muck Surface | • | 0) | | Shallow Aquita | | |
| | on Aerial Imagery (B7) | Other (Explain in R | | | | nanow / iquita nicrotopograph | |) |
| | ed Concave Surface (B8) | _ Other (Explain III IV | (emarks) | | | AC-Neutral Te | • |) |
| Oparsery vegetate | d Colleave Sulface (Do) | | | | — ' | AO-Neutiai I | 63t (D0) | |
| | | | | | | | | |
| Field Observations: | | | | | | | | |
| Surface Water Present? | Yes No X | Depth (inche | es): | | | | | |
| Water Table Present? | Yes No X | Depth (inche | | | | | | |
| Saturation Present? | Yes No X | Depth (inche | · —— | Wetland | Hydrology | Present? | Yes | No X |
| (includes capillary fringe) | 100 110 <u>X</u> | | | Wothana | injurology . | . 10001111 | | |
| . , , , , | tream gauge, monitoring well, | agrial photos, provious | s inepostions) if avai | able: | | | | |
| Describe Recorded Data (Si | ream gauge, monitoring wen, | aeriai priotos, previous | s irispections), ii avai | able. | | | | |
| | | | | | | | | |
| Remarks: | | | | | | | | |
| Remarks. | | | | | | | | |
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| | | | | | | | | |
| No primary or accordan | vindicatora wara procent: that | oforo the budrology or | itarian has not been | mot | | | | |
| No primary or secondary | y indicators were present; ther | elore, the hydrology ch | iteriori nas not been | net. | | | | |
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US Army Corps of Engineers Northcentral and Northeast - Version 2.0

VEGETATION (Four Strata) - Use scientific names of plants.

| | Absolute | Dominant | Indicator | Dominance Test worksheet: |
|---|--------------|------------|-----------|---|
| Free Stratum (Plot size: 30 ft.) | % cover | Species? | Status | Number of Dominant Species |
| 1. Ailanthus altissima | · | 10 | UPL | That Are OBL, FACW, or FAC: 0 (A) |
| 2. | · | | | |
| 3. | | | | Total Number of Dominant |
| 4. | | | | Species Across All Strata: 0 (B) |
| 5 | | | | |
| 6. | | | | Percent of Dominant Species |
| 7. | | | | That Are OBL, FACW, or FAC: 0 (A/B) |
| | | otal Cover | | |
| | · | | | Prevalence Index Worksheet: |
| Sapling/Shrub Stratum (Plot size: 15 f | t) | | | Total % Cover of: Multiply by: |
| 1. None observed | | | | OBL species 0 x 1 = 0 |
| 2 | | | | FACW species 0 x 2 = 0 |
| 3 | | | | FAC species 0 x 3 = 0 |
| 4 | | | | FACU species 100 x 4 = 400 |
| 5 | | | | UPL species 0 x 5 = 0 |
| 6 | | | | Column Totals: (A) (B) |
| 7 | | | | |
| | = T | otal Cover | | Prevalence Index = B/A = 4.00 |
| Herb Stratum (Plot size: 5 ft.) | | | | Hydrophytic Vegetation Indicators: |
| 1. Poa pratensis | 80 | | FACU | 1 - Rapid Test for Hydrophytic Vegetation |
| Plantago lanceolata | 20 | - | FACU | 2 - Dominance Test is >50% |
| 3. | | | | 3 - Prevalence Index is ≤ 3.0 ¹ |
| 4. | | | | 4 - Morphological Adaptations ¹ (Provide supporting |
| 5. | | | | data in Remarks or on a separate sheet) |
| 6. | | | | Problematic Hydrophytic Vegetation ¹ (Explain) |
| 7 | | | | |
| 8 | | | | ¹ Indicators of hydric soil and wetland hydrology must |
| 9. | | | | be present, unless disturbed or problematic. |
| 10. | · | | | Definitions of Five Vegetation Strata: |
| 11 | | | | Tree - Woody plants 3 in. (7.6 cm) or more in diameter |
| 12. | | | | at breast height (DBH) regardless of height. |
| | 100 = T | otal Cover | | |
| | | | | Sapling/Shrub - Woody plants less than 3 in. DBH |
| Woody Vine Stratum (Plot size: 30 ft.) | | | | and greater than or equal to 3.28 ft (1 m) tall. |
| 1. None observed | | | | |
| 2 | | | | Herb - All herbaceous (non-woody) plants, regardless |
| 3 | | | | of size, and woody plants less than 3.28 ft tall. |
| 4 | | | | |
| | = T | otal Cover | | Woody vine - All woody vines greater than 3.28 ft in height. |
| | | | | Hydrophytic |
| | | | | Vegetation |
| | | | | |
| | | | | Present? |
| Remarks: | | | | |
| Nomano. | | | | |
| | | | | |
| | | | | |
| | | | | |
| The hydrophytic vegetation criterion has no | ot been met. | | | |
| | | | | |
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Sampling Point: SP 3

SOIL Sampling Point: SP 3

| Hydric Soils Indicators: Histosol (A1) Histic Epipedon (A2) Black Histic (A3) Hydrogen Sulfide (A4) Stratified Layers (A5) Depleted Below Dark Surface (A11) Thick Dark Surface (A12) Sandy Mucky Mineral (S1) Sandy Redox (S5) Stripped Matrix (S4) Sandy Redox (S5) Stripped Matrix (S6) Dark Surface (S7) (LRR R, MLRA 149B) *Indicators of hydrophytic vegetation and wetland hydrology must be present, unless disturbed or problematic. **Restrictive Layer (if observed): Type: **Polyvalue Below Surface (S8) (LRR R, Depleted Below Surface (S9) (LRR R, MLRA 149B) **Inin Dark Surface (S9) (LRR R, MLRA 149B) **Polyvalue Below Surface (S9) (LRR R, MLRA 149B) **Polyvalue | Texture Remarks Silt Loam Silt Loam PL=Pore Lining, M=Matrix. Indicators for Problematic Hydric Soils³: 2 cm Muck (A10) (LRR K, L, MLRA 149B) Coast Prairie Redox (A16) (LRR K, L, R) 5 cm Mucky Peat or Peat (S3) (LRR K, L, I) Dark Surface (S7) (LRR K, L) Polyvalue Below Surface (S8) (LRR K, L) Thin Dark Surface (S9) (LRR K, L) Iron-Manganese Masses (F12) (LRR K, L, Piedmont Floodplain Soils (F19) (MLRA 144A, 145, 145) Red Parent Material (F12) Very Shallow Dark Surface (F22) Other (Explain in Remarks) |
|--|---|
| 0-3 | Silt Loam Silt Loam Silt Loam PL=Pore Lining, M=Matrix. Indicators for Problematic Hydric Soils³: 2 cm Muck (A10) (LRR K, L, MLRA 1498) Coast Prairie Redox (A16) (LRR K, L, R) 5 cm Mucky Peat or Peat (S3) (LRR K, L, I) Polyvalue Below Surface (S8) (LRR K, L) Thin Dark Surface (S9) (LRR K, L) Iron-Manganese Masses (F12) (LRR K, L, Piedmont Floodplain Soils (F19) (MLRA 14 Mesic Spodic (TA6) (MLRA 144A, 145, 145, 145) Red Parent Material (F12) Very Shallow Dark Surface (F22) |
| 3-17 10YR 5/4 95 10YR 5/8 5 10YR 5/8 5/8 5 10YR 5/8 5/8 5/8 5/8 5/8 5/8 5/8 5/8 5/8 5/8 | PL=Pore Lining, M=Matrix. Indicators for Problematic Hydric Soils³: 2 cm Muck (A10) (LRR K, L, MLRA 149B) Coast Prairie Redox (A16) (LRR K, L, R) 5 cm Mucky Peat or Peat (S3) (LRR K, L, III) Polyvalue Below Surface (S8) (LRR K, L) Thin Dark Surface (S9) (LRR K, L) Iron-Manganese Masses (F12) (LRR K, L, III) Mesic Spodic (TA6) (MLRA 144A, 145, 145) Red Parent Material (F12) Very Shallow Dark Surface (F22) |
| Type: C=Concentration, D=Depletion, RM=Reduced Matrix, MS=Masked Sand Grains. Polyvalue Below Surface (S8) (LRR R, Histosol (A1) Polyvalue Below Surface (S9) (LRR R, Histosed (A1)) Polyvalue Below Surface (S9) (LRR R, MLRA 149B) Black Histic (A3) Thin Dark Surface (S9) (LRR R, MLRA 149B) Hydrogen Sulfide (A4) Loamy Mucky Mineral (F1) (LRR K, L) Stratified Layers (A5) Loamy Gleyed Matrix (F2) Depleted Below Dark Surface (A11) Depleted Matrix (F3) Thick Dark Surface (A12) Redox Dark Surface (F6) Sandy Mucky Mineral (S1) Depleted Dark Surface (F7) Sandy Gleyed Matrix (S4) Redox Depressions (F8) Sandy Redox (S5) Stripped Matrix (S6) Dark Surface (S7) (LRR R, MLRA 149B) Polyvalue Below Surface (S9) (LRR R, MLRA 149B) Redox Dark Surface (S9) (LRR R, MLRA 149B) Polyvalue Below Surface (S9) (LRR R, MLRA 149B) Thin Dark Surface (S9) (LRR R, MLRA 149B) Redox Dark Surface (F7) Redox Depressions (F8) Sandy Redox (S6) Dark Surface (S7) (LRR R, MLRA 149B) Polyvalue Below Surface (S9) (LRR R, MLRA | PL=Pore Lining, M=Matrix. Indicators for Problematic Hydric Soils³: 2 cm Muck (A10) (LRR K, L, MLRA 1498) Coast Prairie Redox (A16) (LRR K, L, R) 5 cm Mucky Peat or Peat (S3) (LRR K, L, I) Dark Surface (S7) (LRR K, L) Polyvalue Below Surface (S8) (LRR K, L) Thin Dark Surface (S9) (LRR K, L) Iron-Manganese Masses (F12) (LRR K, L, Piedmont Floodplain Soils (F19) (MLRA 14 Mesic Spodic (TA6) (MLRA 144A, 145, 145, 145) Red Parent Material (F12) Very Shallow Dark Surface (F22) |
| Type: C=Concentration, D=Depletion, RM=Reduced Matrix, MS=Masked Sand Grains. Polyvalue Below Surface (S8) (LRR R, Histosol (A1) Polyvalue Below Surface (S8) (LRR R, Histose) (A1) Polyvalue Below Surface (S9) (LRR R, MLRA 149B) Histic Epipedon (A2) MLRA 149B) Black Histic (A3) Thin Dark Surface (S9) (LRR R, MLRA 149B) Hydrogen Sulfide (A4) Loamy Mucky Mineral (F1) (LRR K, L) Stratified Layers (A5) Loamy Gleyed Matrix (F2) Depleted Below Dark Surface (A11) Depleted Matrix (F3) Thick Dark Surface (A12) Redox Dark Surface (F6) Sandy Mucky Mineral (S1) Depleted Dark Surface (F7) Sandy Gleyed Matrix (S4) Redox Depressions (F8) Sandy Redox (S5) Stripped Matrix (S6) Dark Surface (S7) (LRR R, MLRA 149B) Type: Hydri Remarks: | Indicators for Problematic Hydric Soils ³ : 2 cm Muck (A10) (LRR K, L, MLRA 149B) Coast Prairie Redox (A16) (LRR K, L, R) 5 cm Mucky Peat or Peat (S3) (LRR K, L, I Dark Surface (S7) (LRR K, L) Polyvalue Below Surface (S8) (LRR K, L) Thin Dark Surface (S9) (LRR K, L) Iron-Manganese Masses (F12) (LRR K, L, Piedmont Floodplain Soils (F19) (MLRA 14 Mesic Spodic (TA6) (MLRA 144A, 145, 145, 145) Red Parent Material (F12) Very Shallow Dark Surface (F22) |
| Histosol (A1) — Polyvalue Below Surface (S8) (LRR R, MLRA 149B) Black Histic Epipedon (A2) — Thin Dark Surface (S9) (LRR R, MLRA 149B) Hydrogen Sulfide (A4) — Loamy Mucky Mineral (F1) (LRR K, L) Stratified Layers (A5) — Loamy Gleyed Matrix (F2) Depleted Below Dark Surface (A11) — Depleted Matrix (F3) Thick Dark Surface (A12) — Redox Dark Surface (F6) Sandy Mucky Mineral (S1) — Depleted Dark Surface (F7) Sandy Gleyed Matrix (S4) — Redox Depressions (F8) Stripped Matrix (S6) Dark Surface (S7) (LRR R, MLRA 149B) Polyvalue Below Surface (S9) (LRR R, MLRA 149B) Loamy Mucky Mineral (F1) (LRR K, L) Loamy Mucky Mineral (F1) (LRR K, L) Depleted Matrix (F3) Redox Dark Surface (F6) Park Surface (S7) (LRR R, MLRA 149B) Polyvalue Below Surface (S9) (LRR R, MLRA 149B) Thin Dark Surface (S9) (LRR R, MLRA 149B) Polyvalue Below Surface (S9) (LRR R, MLRA 149B) Thin Dark Surface (S9) (LRR R, MLRA 149B) Polyvalue Below Surface (S9) (LRR R, MLRA 149B) Thin Dark Surface (S9) (LRR R, MLRA 149B) Polyvalue Below Surface (S9) (LRR R, MLRA 149B) Polyvalue Below Surface (S9) (LRR R, MLRA 149B) Thin Dark Surface (S9) (LRR R, MLRA 149B) Polyvalue Below Surface (S9) (LRR R, MLRA 149B) Polyvalue 1610 | Indicators for Problematic Hydric Soils ³ : 2 cm Muck (A10) (LRR K, L, MLRA 149B) Coast Prairie Redox (A16) (LRR K, L, R) 5 cm Mucky Peat or Peat (S3) (LRR K, L, I Dark Surface (S7) (LRR K, L) Polyvalue Below Surface (S8) (LRR K, L) Thin Dark Surface (S9) (LRR K, L) Iron-Manganese Masses (F12) (LRR K, L, Piedmont Floodplain Soils (F19) (MLRA 14 Mesic Spodic (TA6) (MLRA 144A, 145, 145, 145) Red Parent Material (F12) Very Shallow Dark Surface (F22) |
| Histosol (A1) — Polyvalue Below Surface (S8) (LRR R, MLRA 149B) Black Histic Epipedon (A2) — Thin Dark Surface (S9) (LRR R, MLRA 149B) Hydrogen Sulfide (A4) — Loamy Mucky Mineral (F1) (LRR K, L) Stratified Layers (A5) — Loamy Gleyed Matrix (F2) Depleted Below Dark Surface (A11) — Depleted Matrix (F3) Thick Dark Surface (A12) — Redox Dark Surface (F6) Sandy Mucky Mineral (S1) — Depleted Dark Surface (F7) Sandy Gleyed Matrix (S4) — Redox Depressions (F8) Stripped Matrix (S6) Dark Surface (S7) (LRR R, MLRA 149B) Polyvalue Below Surface (S9) (LRR R, MLRA 149B) Loamy Mucky Mineral (F1) (LRR K, L) Loamy Mucky Mineral (F1) (LRR K, L) Depleted Matrix (F3) Redox Dark Surface (F6) Park Surface (S7) (LRR R, MLRA 149B) Polyvalue Below Surface (S9) (LRR R, MLRA 149B) Thin Dark Surface (S9) (LRR R, MLRA 149B) Polyvalue Below Surface (S9) (LRR R, MLRA 149B) Thin Dark Surface (S9) (LRR R, MLRA 149B) Polyvalue Below Surface (S9) (LRR R, MLRA 149B) Thin Dark Surface (S9) (LRR R, MLRA 149B) Polyvalue Below Surface (S9) (LRR R, MLRA 149B) Polyvalue Below Surface (S9) (LRR R, MLRA 149B) Thin Dark Surface (S9) (LRR R, MLRA 149B) Polyvalue Below Surface (S9) (LRR R, MLRA 149B) Polyvalue 1610 | Indicators for Problematic Hydric Soils ³ : 2 cm Muck (A10) (LRR K, L, MLRA 149B) Coast Prairie Redox (A16) (LRR K, L, R) 5 cm Mucky Peat or Peat (S3) (LRR K, L, I Dark Surface (S7) (LRR K, L) Polyvalue Below Surface (S8) (LRR K, L) Thin Dark Surface (S9) (LRR K, L) Iron-Manganese Masses (F12) (LRR K, L, Piedmont Floodplain Soils (F19) (MLRA 14 Mesic Spodic (TA6) (MLRA 144A, 145, 145, 145) Red Parent Material (F12) Very Shallow Dark Surface (F22) |
| Hydric Soils Indicators: Histosol (A1) — Polyvalue Below Surface (S8) (LRR R, MLRA 149B) Black Histic (A3) — Thin Dark Surface (S9) (LRR R, MLRA 149B) Hydrogen Sulfide (A4) — Loamy Mucky Mineral (F1) (LRR K, L) Stratified Layers (A5) — Loamy Gleyed Matrix (F2) Depleted Below Dark Surface (A11) — Depleted Matrix (F3) Thick Dark Surface (A12) — Redox Dark Surface (F6) Sandy Mucky Mineral (S1) — Depleted Dark Surface (F7) Sandy Gleyed Matrix (S4) — Redox Depressions (F8) Stripped Matrix (S6) Dark Surface (S7) (LRR R, MLRA 149B) 3Indicators of hydrophytic vegetation and wetland hydrology must be present, unless disturbed or problematic. Restrictive Layer (if observed): Type: Depth (inches): Hydri | Indicators for Problematic Hydric Soils ³ : 2 cm Muck (A10) (LRR K, L, MLRA 149B) Coast Prairie Redox (A16) (LRR K, L, R) 5 cm Mucky Peat or Peat (S3) (LRR K, L, I Dark Surface (S7) (LRR K, L) Polyvalue Below Surface (S8) (LRR K, L) Thin Dark Surface (S9) (LRR K, L) Iron-Manganese Masses (F12) (LRR K, L, Piedmont Floodplain Soils (F19) (MLRA 14 Mesic Spodic (TA6) (MLRA 144A, 145, 145, 145) Red Parent Material (F12) Very Shallow Dark Surface (F22) |
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APPENDIX D

Professional Qualifications



PROJECT ROLESenior Project Scientist II

EDUCATION

Bachelor of Science in Environmental Resource Management, The Pennsylvania State University, 2005

Master of Science in Biology, Bloomsburg University of Pennsylvania, 2015

REGISTRATION

Certified Professional Soil Scientist (CPSS), 2012, #36359 Professional Wetland Scientist (PWS), 2012, #2284

PROFESSIONAL MEMBERSHIPS

Soil Science Society of America, Society of Wetland Scientists, The Wildlife Society

SUMMARY OF QUALIFICATIONS

Mr. Simko has approximately 17 years of experience in performing an array of wetland delineations and site assessments. His experience encompasses soil morphological evaluations, infiltration and percolation testing, wetland mitigation design and monitoring, bog turtle habitat identification, as well as threatened and endangered species surveys. In addition, he has completed carbonate geology site evaluations, identification of asbestos-containing material, and underground storage tank removals and investigations. Mr. Simko's computer skills include ArcGIS 10 and GPS Pathfinder Office. As a Senior Project Scientist II at BL Companies, Mr. Simko's responsibilities include wetland investigations, soil investigations, ground water investigations, Phase I site assessments, remediation related activities, remediation system monitoring and maintenance, and engineering compliance inspection for natural gas pipeline projects.

RELEVANT EXPERIENCE

Peer Review, 4-Lot Subdivision Inland Wetland Commission, Stratford, Connecticut

Served as lead Soil and Wetland Scientist in the performance of a peer review of a proposed 4-lot subdivision application submission to the Inland Wetland Commission of Stratford, CT. The peer review required a site visit to verify previous wetland delineations and assistance with the technical review of the submission. Upon completion of review, findings were presented inperson to the Stratford Inland Wetland Commission.

Carter Road Culvert Improvements, Thomaston, Connecticut

Served as Environmental Scientist (Soil/Wetland Scientist) for the delineation of wetlands and preparation of function/value report for the repair and improvements to this deteriorated stone masonry abutment culvert that was impacted by flood events and long-term deterioration.

Bridge Replacement Group 13E-W, West River Bridge, Rhode Island Department of Transportation, Providence, Rhode Island

Conducted stream and wetland delineations in the vicinity of the West River Bridge in Providence as part of the Rhode Island Department of Transportation Bridge Replacement project. Additional assessment of the functions and values of the water resources was completed and a habitat survey of the substrate and surrounding vegetative communities was conducted within the vicinity of the bridge abutments and potential work area. Also served as Senior Project Scientist to investigate the presence or absence of inland wetlands and watercourses in the area of the West River Bridge in Providence, RI. Additionally, conducted substrate observations and analyses of the West River within the area of proposed bridge work to ascertain the likelihood of threatened & endangered species presence and/or their habitat.

Route 37 Bridge Rehabilitations and Replacements, Rhode Island Department of Transportation, Warwick and Cranston, Rhode Island

Served as Senior Project Scientist, with responsibilities including wetlands delineation, function and values assessment, and close coordination with the bridge designer in order to submit environmental permit documentation on a fast-track basis.

East Bay Bike Path, Barrington River & Warren River Bridges Replacement, Rhode Island Department of Transportation, Barrington and Warren, Rhode Island

Served as Wetland and Soil Scientist, with responsibilities including wetlands delineation, function and values assessment, determination of coastal and freshwater wetland jurisdiction, and close coordination with the bridges designer to submit environmental permit documentation with the greatest efficiency. Also served as Senior Project Scientist to investigate the presence or absence of inland and coastal wetlands, and watercourses in the area of the Barrington Bike Path Bridge



#837, over the Barrington River, and the Warren Bike Path Bridge #838, over the Palmer River. Additionally, conducted substrate observations and analyses of the Barrington River and Palmer River within the area of proposed bridge piers / supports to ascertain likelihood of shellfish or threatened & endangered species presence and/or their habitat.

Bridge Group 17A, Rhode Island Department of Transportation, Cumberland, Rhode Island

Served as Senior Project Scientist to investigate the presence or absence of inland wetlands and watercourses for the proposed rehabilitation of bridge number 075401 carrying Rt. 114 (Diamond Hill Road) over I-295 in Cumberland, RI, bridge number 075101 carrying Rt. 122 (Mendon Road) over I-295 in Cumberland, RI, and bridge numbers 074601; and 074621 carrying Rt. 7 over I-295 in Smithfield, RI. Additionally, wetland and stream biophysical elements such as landscape position, size, geology, hydrology, substrate, and vegetation were observed to determine the wetland and stream functions and to what capacity they are performed.

Consultant Liaison Engineering Services for the State and Federal Local Bridge Program, Connecticut Department of Transportation, Statewide, Connecticut

Served as Senior Project Scientist for several bridge rehabilitation and replacement projects for the Connecticut Department of Transportation across the state. Responsibilities included performing wetland delineations, function and values assessments, and bat habitat assessments at each bridge location where natural resources were identified as being within the proximity of proposed work. Additional responsibilities included attaining environmental permitting for the Connecticut Department of Energy and Environmental Protection and U.S. Army Corps of Engineers, identifying invasive species, and coordination for listed species.

Connecticut Department of Transportation State Project No. 108-189 – Moosup Valley State Park Trail, Plainfield to Sterling, Connecticut

Served as Senior Project Scientist to investigate the presence or absence of vernal pools along the Moosup Valley State Park Trial. Vernal pools were identified utilizing available mapping, aerial photography and field investigation. Evidence of obligate amphibian species presence and breeding was noted in the field via inspection beyond visual and audial, including trapping and dip-netting.

Metro North Milvon Substation – West River Substation Vernal Pool Assessment, Milford to New Haven, Connecticut Served as Senior Project Scientist to investigate the presence or absence of vernal pools along a portion of the commuter train route. Any vernal pool areas were noted and recorded with GPS coordinates to submeter accuracy. Vernal pools were identified utilizing available mapping, aerial photography, and field investigation. Evidence of obligate amphibian species

Bog Turtle Surveys – Mid-Atlantic Center for Herpetology & Conservation – Various locations within Eastern Pennsylvania
Served as Survey Volunteer over the course of several surveying seasons with the Mid-Atlantic Center for Herpetology &
Conservation. Bog turtle habitat was identified, and species-specific surveying techniques were utilized. Experience assisting with implantation of Passive Integrated Transponders (PIT tags) was also gained. Mr. Simko has located 23 bog turtles, a critically endangered species, throughout his surveying career.

American Tower Sites-Various States throughout the Northeast

Conducted NEPA reviews and clearances for cellular communication tower installation sites that include wetland delineations, migratory bird and bat habitat, GIS mapping, and National Historic Preservation Act Section 106 clearances as needed.

PSEG Long Island, Western Nassau Transmission Project, Valley Stream to Garden City, New York

Serves as Construction Field Inspector for a 7.5 mile underground electric transmission line in Nassau County, NY. As Construction Field Inspector Mr. Simko is tasked with day-to-day inspection of the project site with respect to contractor activities constructing, installing, testing, and placing in service an underground 138kV circuit.

Amazon.com Services LLC, DEB3 – Delivery Station Buildout, Waterbury, Connecticut

presence and breeding was noted in the field via visual and audial inspection.

Served as lead Soil Scientist and Wetlands Investigator for a proposed site redevelopment project. Responsibilities included reverification of wetland delineations and coordination with the City Planner for Waterbury, CT in order to move the project through the Inland Wetland Commission application process.



Bog Turtle Survey, PNDI Review, Wetland Delineation, Amazon.com Services LLC – Quakertown, Pennsylvania

Served as Senior Project Scientist to perform habitat survey for bog turtles, as well as performing other Pennsylvania Natural Diversity Inventory (PNDI) tasks. Also performed a wetland delineation for the site in accordance with the Army Corps of Engineers Wetland Delineation Manual and the appropriate Regional Supplement.

Hope Street Culvert Replacement, City of Stamford, Connecticut

Served as lead Wetland Investigator for an emergency culvert replacement project in the vicinity of Hope Street & Mead Street, Stamford Connecticut.

4-Lot Subdivision Inland Wetland Commission Peer Review, Strafford, Connecticut

Served as lead Soil and Wetland Scientist in the performance of a peer review of a proposed 4-lot subdivision application submission to the Inland Wetland Commission of Stratford, CT.

Avangrid – Wetland Delineations and Vernal Pool Investigation Within Metro North Railroad Corridor, Westport to New Haven, CTServed as lead Soil and Wetland Scientist and Biologist in the performance of survey work for wetlands and vernal pool areas along the railroad corridor between Westport and New Haven, CT.

Simmonsville Bridge Replacement, Rhode Island Department of Transportation, Johnston, Rhode Island

Served as Senior Project Scientist, with responsibilities including wetlands delineation, function and values assessment, bat habitat assessments, and close coordination with the bridge designer in order to submit environmental permit documentation on a fast-track basis.

Route 37 Bridge Rehabilitations and Replacements, Rhode Island Department of Transportation, Warwick and Cranston, Rhode Island

Served as Senior Project Scientist, with responsibilities including wetlands delineation, function and values assessment, and close coordination with the bridge designer in order to submit environmental permit documentation on a fast-track basis.

Williams, Transco Pipeline, Atlantic Sunrise Pipeline Project, Various Counties, Pennsylvania

Serves as Senior Engineering Compliance Inspector within Columbia County, PA. Served as Senior Project Scientist for the completion of soil test pit evaluations and stormwater detention basin infiltration testing for compressor station sites throughout the state.

Kinder Morgan, Utopia Pipeline, Various Counties, Ohio

Serves as Senior Project Scientist for an approximately 225-miles ethane/propane pipeline through northern Ohio. Responsibilities include conducting wetland, soils, and natural resource studies.

Dominion Energy, Atlantic Coast Pipeline, Various Counties, West Virginia & Virginia

Served as an Environmental Scientist and conducted wetland screenings, delineations, permitting, and mitigation design and monitoring for 130 miles of natural gas pipeline projects for the Krause and Wellsboro pipelines.

SWEPI (Shell), Various Counties, Pennsylvania

As an Environmental Scientist, Mr. Simko conducted wetland screenings, delineations, permitting, and mitigation design and monitoring for 130 miles of natural gas pipeline projects for the Krause and Wellsboro pipelines. Services were completed in 2015.

Hilcorp & Cabot Natural Gas, Various Natural Gas Well Pads & Pipeline Projects, Various Counties, Pennsylvania

As Erosion and Sedimentation (E&S) inspector, Mr. Simko conducted E&S inspections at various natural gas well pads and gathering pipeline projects located in the northern tier and southwestern portions of Pennsylvania. His duties involved preparing inspection reports and photo documentation. Services were completed in 2014.

PVR Natural Gas Gathering, Various Natural Gas Well Pads & Pipeline Projects, Susquehanna & Wyoming Counties, Pennsylvania Served as the Environmental Scientist responsible for wetland screenings and delineations for another company to install a gas pipeline at their facility, as well as various other natural gas pipeline and well pad projects throughout northern Wyoming County and Susquehanna County in Pennsylvania. Services were completed in 2013.



Williams (Access) Midstream Company, Various Natural Gas Well Pad Sites, Columbia County, Pennsylvania

Served as the Environmental Scientist responsible for wetland screenings and delineations, as well as threatened and endangered species habitat assessments, for various natural gas well pad sites within Columbia County, Pennsylvania. Services were completed in 2013.

PP&L Susquehanna to Roseland 500 KV Electric Transmission Line, Pennsylvania

Served as the Environmental Scientist responsible for wetland delineations, as well as threatened and endangered species habitat assessments, for a large segment of electric transmission line within Pennsylvania of the PPL Electric Utilities project known as the Susquehanna-Roseland Line. Firm of Record: Woodland Design Associates, Inc., Honesdale, Pennsylvania

Southeast Bristol Business Park - Lot 3, Lot 9, Lot 10, Bristol, Connecticut

Serving as Senior Project Scientist, conducted a wetland delineation survey for Lot 3, Lot 9, and Lot 10 of the Southeast Bristol Business Park in August of 2021. Following field delineation efforts, a wetland delineation report was created to give details regarding the field work findings. Additionally, a field site visit meeting with the City of Bristol's Inland Wetlands and Watercourses Commission (IWWC) was performed to present wetland delineation findings to the Commission for their review and subsequent approval. Following the IWWC site meeting and agreement with the wetlands and watercourses delineation work, the City of Bristol's official IWWC wetland mapping was updated from previous delineation work to reflect BL Companies' more inclusive and comprehensive field findings and geographical positioning system (GPS) data collection.

894 Middle Street - Lot 17, Lot 17-3 & Lot 17-4-1, Bristol, Connecticut

Serving as Senior Project Scientist, conducted a wetland delineation survey in October of 2021 on the property located at 894 Middle Street in the City of Bristol, comprised of Lot 17, Lot 17-3 & Lot 17-4-1. Following field delineation efforts, a wetland delineation report was created to give details regarding the field work findings. The field survey revealed several areas of erosional features in and around the wetlands and watercourses on the site, as well as areas of dumping of household refuse and other assorted trash and debris. These findings were brought to the attention of the City of Bristol and a site meeting with the City's Inland Wetlands and Watercourses Commission (IWWC), Wetland Scientist, and City Engineer was performed to present findings.

Wetland/Waterbody Identification and Delineation, Ludlow, Massachusetts

Serving as Senior Project Scientist, conducted a wetland delineation survey, including functions and values assessment for a property in Ludlow, MA in June of 2022. Following field delineation efforts, a wetland delineation memo was created to give details regarding the field work findings.

Utility Pipeline Crossing, Brockton, Massachusetts

BL Companies provided the integration of GIS-based, GPS-based, and CAD-based data utilizing ArcMap software to develop an Environmental Plot Plan for the design and permitting of a natural gas utility line over the Salisbury River in Brockton, MA. The scope of services that BL is providing consisted of the following:

- Received and integrated non-BL GIS data, BL survey data, and design-related CAD data into an overall ENV plot
 plan. This included a multitude of geoprocessing techniques within the ArcMap software.
- Provided E&S design for project on the plan.
- Incorporated local environmental buffer ordinances utilizing geoprocessing techniques.
- Prepared and plotted the data in a visually aesthetic manner for use in the local permitting process.

Utility Line Crossing Evaluation Proposed River Crossing Project-Norwell, Massachusetts

BL's engineering and environmental team conducted an in-depth evaluation of the different river crossing methods for a proposed utility line crossing over a regulated river in Norwell, MA. The methodologies considered impacts regulated features including wetlands, rivers, Riverfront and potential impacts to migratory fish and avian species. Horizontal directional drill, mounting the utility line and impacts to the existing bridge and construction of a stand-alone aerial crossing independent of an existing bridge structure where evaluated. The crossing method has not been finalized and further cost evaluations are being considered by the client.





PROJECT ROLE
Senior Project Manager

EDUCATION

Bachelor of Science in Biology, West Chester University, 1992

CERTIFICATIONS / TRAINING

Professional Wetlands Scientist (PWS), Society of Wetlands Scientists PA Fish & Boat Commission Scientific Collector's Permit PA DCNR Wild Plant Management Permit OSHA 40-Hour Hazardous Waste Site Training CFR29 1910.120, 1986 OSHA 8-Hour Refresher Training for Hazardous Waste Sites, 1987-2021 PA DEP Certified Drinking Water Laboratory Director 1996-2007 Pollution Biology, Penn State University, 2002 Environmental Law, Penn State University, 2001

SUMMARY OF QUALIFICATIONS

Mr. Wolf specializes in building client trust and enduring relationships within the environmental studies and permitting sections across multiple disciplines of the engineering field. His overall experience is focused on natural resources evaluations to include wetlands and aquatic resources, operating, and overseeing drinking water and water quality testing laboratories, and overseeing groups conducting wetland delineations, permitting, mitigation, and plant and animal surveys. Additional responsibilities include managing large scale projects with multi-disciplined teams to accomplish client permitting and site evaluation goals. Technical background includes experience with studies in terrestrial ecology and botany, environmental compliance monitoring, and construction oversight during and after completion of construction projects.

Mr. Wolf has extensive experience leading teams that interface with multiple state, local, and federal regulatory agencies, including the U.S. Army Corps of Engineers (USACE), state environmental protection departments, and the US Environmental Protection Agency (USEPA) Inland Wetland Commissions (IWC) as part of ongoing project coordination for multi-faceted development, energy generation and transmission projects. Mr. Wolf is team lead and project manager for linear energy siting and routing projects over thousands of acres throughout the northeast down through Florida and into the Midwestern states.

RELEVANT EXPERIENCE

Large Scale Warehouse Development Oldmans Township, New Jersey

Conduct field and permitting oversite for team of wetland and stream delineators. Assess ditch wetlands, various isolated wetlands and abutting wetlands associated with riverine systems. Complete LOI coordination with the NJDEP and complete the Section 404 permitting process for the conversion of former federal army barracks and training compound to office and warehouse development.

Spark Carwash Site – Ocean Township, New Jersey

Project Manager overseeing field teams conducting wetland presence/absence surveys and P/A LOI for approval to the NJDEP. Utilize NJ Freshwater wetlands mapper along with hydric soils layers prior to visiting sites to determine potential problem areas and field verify wetland parameters, or lack of, using the Unified Federal Methodology of the 1989 Manual along with appropriate field determination data sheets for the specific region in which wetlands are identified.

Industrial Development - New Greenwich, New Jersey

Project manager overseeing field teams completing wetland delineations and completing LOIs for inland wetlands delineations for within the project area.

Telecom Provider, 28 Sites Throughout New Jersey

Project Manager overseeing teams conducting NEPA assessments, Phase I Environmental Site Assessments, wetland delineations, and GIS analysis for multiple new and expansion projects for telecommunication compounds/towers. Project management included managing various phases of individual projects, including preparation of proposals, budgets, change orders, and client care activities. Additional project-specific responsibilities include identifying cultural and historic concerns in and around the project sites, wetland delineations within an identified study corridor, 404 wetlands permitting, asbestos and





lead-based paint surveys, and collection of GPS data utilizing a Trimble GPS system and client care. Utilizes ArcGIS to create visual aid maps and exhibits for permits and construction plans.

14601 Sweitzer Lane, Prince George's County, Maryland

Provided Project Senior technical environmental oversight and guidance for field team conducting forest stand delineation, tree conservation plans, and completing invasive species management plan for a warehouse refit project. Our team utilized grid assessments of 1/10th-acre sample plot analysis, completed documentation of primary canopy layer, subcanopy species, and understory species to provide a qualitative and quantitative analysis to determine the health of the on-site forest habitat. The data was then compiled and presented as site plans, forest management plans, and an overall forest stand delineation report. Upon completion of the forest stand delineation, a tree conservation plan that included conservation easements for both existing forest and forest natural regeneration areas was developed. As part of the management of the conservation areas, an invasive species management plan was developed and approved by the MD National Parks and Planning Commission on behalf of Prince George's County. The invasives species management plan identified the predominate invasive species and developed a four-year plan to eradicate the invasive species by manual, mechanical, and herbicide application methods. The plan preparation and certification of the forest stand delineation and tree conservation plan was completed during 2021. The forest natural species regeneration and invasive species management is on-going through September of 2024.

Walker Farms, New Castle County, Delaware

Served as the Project Manager and technical environmental lead in conducting a natural resource assessment utilizing the New Castle County (NCC) updates to the Unified Development Code under the New Castle County Delaware, Code of Ordinances, Chapter 40, Article 10, Environmental Standards, "Green NCC" protocol enacted by the County Commissioners in December 2021. On-site forest habitat assessments utilizing grid assessments of 1/10th-acre sample plot analysis. Data was collected documenting the dominate canopy species, subcanopy species, and understory species to provide a qualitative and quantitative analysis to determine the health of the on-site forest habitat. Other on-site evaluations consisted of wetland and watercourse delineations, and desktop assessments of floodplains/floodways, riparian zones, steep slopes, and problematic geological formations. The data was compiled and presented as site plans and technical reports. BL Companies completed plan and report preparation in early 2022 with the information submitted to New Castle County for regulatory clearance.

Baseline Ecological Evaluations and Baseline Ecological Assessment and Evaluations

Conduced Baseline Ecological Evaluations (BEEs) and BERAs within NJ Industrial Reclamation program. Also conducted these BEEs for coal fired power plants in NJ and DE. Observed Peregrine falcon nesting behavior at two facilities. Conducted ecological risk assessments for Brownfields and Industrial Reuse sites in PA and NJ. The risk assessments included pathway reduction and observations of local birds of prey and the nesting behaviors associated within the project area.

Natural Gas Transmission Installation, PGCDCRRP, Maryland

Oversaw and conducted stream and wetlands field surveys, forest stand delineations, cultural resources surveys, mitigation, site investigation, and permitting assistance through a high-density residential area of Laurel through Waldorf MD of a proposed natural gas transmission line. Interfaced with Maryland Department of the Environment and the Baltimore Districts of the USACE to complete the field review of a jurisdictional determination for the pipeline route.

Natural Gas Transmission Line Replacement, Virginia and Maryland

Oversaw and conducted stream and wetlands field surveys along the VA and MD transmission line segments. Conducted threatened and endangered (T&E) species clearances and interfaced with Norfolk and Baltimore Districts of the USACE to document Nationwide Permit (NWP) and State Programmatic General Permit (SPGP) 5 Permit applicability for the projects. Obtained in-place state Memorandums of Agreements (MOAs) for ongoing maintenance activities within the transmission line right of way.

Gas Fired Power Generation Plant, Southern Virginia

Lead permitting for natural resources assessments, including streams and wetlands, permitting for impact to streams and wetlands, mitigation bank identification, and credit secure for wetlands and stream impacts. Oversaw field crews that





conducted habitat surveys to provide documentation for clearance of U.S. Fish and Wildlife Service (USFWS), identified T&E species at the location, and successfully permitted roadway impacts to the site.

Coal Combustion Residuals Remediation, Eastern Virginia

Lead natural resources team for identification of T&E species reviews and field survey verification, guided and oversaw surveys for small whorled pogonia and northern long-eared bat, USFWS eagle take and monitoring permitting, stream and wetlands surveys utilizing the 1987 USACE Wetlands Delineation Manual and regional supplement for the Atlantic and Gulf Coastal Plain and the Unified Stream Methodology (USM) for the entire 489+ acre parcel. Procured the Jurisdictional Determination (JD) and successful Section 404/401 Virginia Department of Environmental Quality permitting for impacts to streams and wetlands, including mitigation for impacts. Oversaw cultural resources surveys and interactions with the Virginia Department of Historic Resources, which included archeological assessments of historic structures and Phase 1a for locations on-site identified from desktop surveys. Completed and successfully fulfilled requirements for impacts to Resource Protection Areas (RPAs) under the County's Chesapeake Bay Preservation Act, including the Preservation Area Site Assessment (PASA) using the Fairfax method to conduct Perennial Flow Determinations (PFD) and the associated Water Quality Impact Assessment (WQIA) for encroachments into RPAs and mitigation for RPA impacts.

Battery Storage Facility, Holyoke, Massachusetts

Conducted wetland field delineation and completed the wetlands report for inland freshwater wetland located at a potential Energy Storage Site in Holyoke, MA. The freshwater wetland buffer was proposed for impacts from the project footprint. After consultation with the Holyoke Conservation Commission, the client revised the project layout to eliminate buffer impacts. The project included coordination with both the Mass. Department of Environmental Protection (MADEP) and the Holyoke Conservation Commission, due to the uncertainty of the jurisdictional limits at the time of application. Review of the MASSMapper revealed that there were no threatened or endangered species or Areas of Special Environmental Concern located in the project area.

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- Received and integrated non-BL GIS data, BL survey data, and design-related CAD data into an overall Environmental plot plan. This included a multitude of geoprocessing techniques within the ArcMap software.
- Provided Erosion and Sediment (E&S) design for project on the plan.
- Incorporated local environmental buffer ordinances utilizing geoprocessing techniques.
- Prepared and plotted the data in a visually aesthetic manner for use in the local permitting process.

Utility Line Crossing Evaluation Proposed River Crossing Project, Norwell, Massachusetts

BL's engineering and environmental team conducted an in-depth evaluation of the different river crossing methods for a proposed utility line crossing over a regulated river in Norwell, MA. The methodologies considered impacts to regulated features including wetlands, rivers, riverfront, and potential impacts to migratory fish and avian species. Horizontal directional drill, mounting the utility line, and impacts to the existing bridge and construction of a stand-alone aerial crossing independent of an existing bridge structure were evaluated. The crossing method has not been finalized and further cost evaluations are being considered by the client.

Peer Review, 4-Lot Subdivision Inland Wetland Commission, Stratford, Connecticut

Conducted third party review of a proposed residential development near a Tier 1 vernal pool and associated inland freshwater wetland. The Town of Stratford's Inland Wetland Commission (IWC) had requested a third-party review of a development proposed near a sensitive resource and surrounding neighborhood. Reviewed and critiqued proposed impacts from stormwater, on-site septic, and proximity to bedrock. Evaluated possible impacts to the wetlands at the site from these components. Identified approximately 25 different negative components and presented findings to the IWC. These findings helped the IWC determine that the development needed significant improvement before it could be approved.



Pameacha Pond Dam Removal Project, Middletown, Connecticut

Conducted dam and natural resources assessment and developed a containment plan to ensure that the invasive northern snakehead fish was contained within the impoundment area of the Pameacha Pond. Worked with stream restoration team to develop a post dam removal restoration strategy, including evaluating an upstream reference reach using horizontal surveys and channel evaluation.

Metro North Railroad Catenary Bonnet Replacement Project, Fairfield to Bridgeport, Connecticut

Oversaw and lead natural resources (NR) investigations along the Metro North Railroad as part of electric transmission line support upgrades. NR investigations included vernal pool surveys and identification of obligate species or eggs present in pools as indicator species, and inland and tidal wetlands delineations using high tide lines, coupled with vegetative transition demarcations as identified in the field.

Multiple Solar Sites, Connecticut

Oversee and direct natural resources team to conduct wetland delineations, functions and values assessments, and habitat surveys for multiple sites located throughout Connecticut. Field delineations are conducted utilizing the US Army Corps of Engineers 1987 Wetland Delineation Manual (Environmental Laboratory, 1987) along with the appropriate Regional Supplements. The CT hydric or poorly drained soils delineation line is included in the final report mapping to align with both state and federal guidance in mapping wetland areas. Interface with various Inland Wetland Commissions within different local jurisdictions.

Thin Layer Placement Marsh Restoration, Old Lyme, Connecticut

Lead mitigation options discussion, researched methodologies, and presented white paper to the USACE - New England District, the Connecticut Department of Energy and Environmental Protection (CTDEEP), and Office of Environmental Protection within the Connecticut Department of Transportation (CTDOT). Prepare research teams to conduct on-site testing, locate potential dredge material sources, and interfaced with multiple state, federal, and private entities to corroborate feasibility of restoration design. Coordinated with multiple outside agencies, consultants, and stakeholders to identify the appropriate mitigation strategy for coastal and tidal wetlands systems. Presented white paper to the USACE and CTDEEP for review and approval to use Thin Layer Placement as an appropriate marsh restoration strategy within a State Park in CT.

Pipeline Replacement and Relocation Projects, Northwest Pennsylvania

Served as project manager for multiple pipeline replacement projects within several Exceptional Value (EV) and wild trout streams located adjacent to wetlands. Oversaw and assisted field teams in delineating water resources, collecting Level Two Rapid Assessment (L2RA) data and compiling the environmental assessment. Managed surveyors conducting rare, threatened, or endangered species surveys for endangered plants and reptiles known to occur within the project boundaries. Facilitated and oversaw preparation and final review for submittal of Joint Permit Application (JPA) and associated restoration plan in lieu of mitigation for impacts to water resources on the project. Interfaced with PA Department of Environmental Protection (PADEP) and USACE representatives to conduct a jurisdictional determination (JD) for routes and permit successful JPA or general permit submittal. The projects' scope also included stream restoration, cultural resources clearances, NPDES permitting, construction monitoring, environmental inspections, and post construction monitoring of restored resources and impacted wetlands and streams.

Laboratory Director, East Berlin, Pennsylvania

Envisioned, designed, constructed, and developed all protocol, procedures, Quality Assurance/Quality Control Plan and instrumentation for a Pennsylvania Department of Environmental Protection certified drinking water and wastewater analytical laboratory. Presented business plan to lenders and secured funding for operations, developed employees, employee benefits program and oversaw day to day operations as laboratory director of the start-up venture from inception to over \$2MM in revenue within 5 years.

Laboratory Director, East Stroudsburg, Pennsylvania

Oversaw and updated all sample collection, testing and quality assurance/quality control procedures for a failing Pennsylvania Department of Environmental Protection (PADEP) certified drinking water and water quality testing laboratory. Assumed day to





day control of sample procedures and updated all testing methodologies to retain certification by the PADEP within a two-month time frame. Rewrote all QA/QC manuals and updated testing procedures to assure adherence to recognized testing procedures.

12 Mitigation Sites, Northeast Pennsylvania

Served as project manager on inception of monitoring for 12 mitigation sites located in northeast Pennsylvania. Wetlands mitigation and stream restoration were required for 12 different pipeline projects located in Wyoming and Susquehanna County, PA. Oversaw and conducted site identification, met with landowners, and secured approvals from the PADEP and USACE to construct the sites. Installed groundwater monitoring wells, performed initial assessments of the water resources, and designed the mitigation sites for construction. Selected the construction contractor and conducted oversight during construction. Performed post construction monitoring for each of the 12 successful mitigation and stream restoration locations.

Rhode Island Department of Transportation, Bridge Replacement Group 13E-W West River Bridge, Providence, Rhode Island Served as Environmental Project Manager for the natural resources group that conducted stream and wetland delineations in the vicinity of the West River bridge in Providence as part of the RIDOT Bridge Replacement project. Additional assessment of the functions and values of the water resources was completed, and a habitat survey of the substrate and surrounding vegetative communities was conducted within the vicinity of the bridge abutments and potential work area.

Rhode Island Department of Transportation, Route 37 Bridge Rehabilitations and Replacements, Warwick and Cranston, Rhode Island

Served as Environmental Project Manager of the multi-disciplined team conducting wetlands delineation and function and values assessment. Worked in close coordination with the bridge designer in order to submit environmental permit documentation on a fast-track basis.

Barrington & Warren Bike Path Bridges, Barrington and Warren, Rhode Island

Served as Environmental Project Manager of the natural resources team that conducted wetland and stream delineation of the East Bay Bike Path bridges over the Barrington and Palmer Rivers in Barrington and Warren, RI. A regulated watercourse and four (4) coastal wetlands were identified within the project area. An initial assessment of the coastal habitat and substrate was conducted to facilitate information to the NOAA's National Marine Fisheries Service. In addition, the functions and values of the wetlands were assessed, and avoidance and minimization measures were considered to reduce impacts to the wetland areas.

Consultant Liaison Engineering Services for the State and Federal Local Bridge Program, Connecticut Department of Transportation, Statewide, Connecticut

Served as Senior Project Scientist for several bridge rehabilitation and replacement projects for CTDOT across the state. Responsibilities included performing wetland delineations, function and values assessments, and bat habitat assessments at each bridge location where natural resources were identified as being within the proximity of proposed work. Additional responsibilities included attaining environmental permitting for the CTDEEP and U.S. ACOE, identifying invasive species, and coordination for listed species.

City of Bristol, Bristol, Connecticut

Coordinate assessment of stream and wetland delineation and develop a site restoration plan for impacted watercourses and wetland features located on a city owned property. The City's IWC had identified several areas of concern on a City owned property that included a soil stock pile of PCB contaminated soils that was being eroded by uncontrolled stormwater discharge from the site. Lead team to conduct an evaluation of remedial alternatives to stabilize the sandy soils on the site, remove sediment from wetlands, and propose a restoration plan for review and approval by the IWC. Restoration is ongoing and expected to be completed in October 2022.

Southeast Bristol Business Park, Bristol, Connecticut

Served as Project Manager for a wetland delineation survey for Lot 3, Lot 9, and Lot 10 of the Southeast Bristol Business Park in August of 2021. The Lots are approximately 12.67 acres in combined size and approximately 16 hours of surveying efforts were performed at the Lots. Following field delineation efforts, a wetland delineation report was created to give details regarding the





field work findings. Additionally, a field site visit meeting with the City of Bristol's Inland Wetlands and Watercourses Commission (IWWC) was performed to present BL Companies' wetland delineation findings to the Commission for their review and subsequent approval. Following the IWWC site meeting and agreement with BL Companies' wetlands and watercourses delineation work, the City of Bristol's official IWWC wetland mapping was updated from previous delineation work to reflect BL Companies' more inclusive and comprehensive field findings and geographical positioning system (GPS) data collection. BL Companies' extensive geographical information system (GIS) knowledge and experience was utilized to present the City of Bristol with mapping and digital data to quickly and easily update their official mapping.

Additional Relevant Projects

Initiate and develop Post Construction Monitoring program suitable for USACE permit compliance on natural gas pipelines in PA as part of ongoing pipeline construction.

Lead field teams delineating streams and wetlands along a 20-mile pipeline through the Washington DC/MD suburbs. Secured JD from the USACE. Oversaw and assisted with Forest Stand Delineations (FSD) and Tree Conservation Plans (TCP's) for hundreds of acres of woodland along the proposed route, including multiple alternative routes.

Pipelines in and Susquehanna Wyoming Counties PA. T&E plant survey along proposed pipelines. Multiple plant species identified during the initial PNDI clearance phase. Presence/absence surveys conducted within the pipeline ROW and buffer to 300' away.

Conducted multiple Rare, Threatened, and Endangered (RTE) surveys for habitat capable of supporting snow trillium (*Trillium nivale*). Sites were cleared based upon completion of extensive ground surveys.

Completed multiple site field surveys for RTE species to include *Ellisia nyctelea*, *Aplectrum hyemale* along with assessments for macroinvertebrates, terrestrial amphibians, and fish inventories. Studies were conducted as part of ongoing investigations or monitoring events for sites under restoration and occurred in the multi state region from CT to VA.

Design and develop stormwater treatment system utilizing common reed (*Phragmites australis*) to treat stormwater runoff from a lead battery recycling facility prior to discharge to surface water.

Served as biologist overseeing an award-winning team of geologists, engineers, and biologists coordinating with state and federal regulatory groups that designed a storm and surface water runoff treatment system for a commercial development within Karst terrain. The system utilized stormwater treatment with physical (Stormceptor) primary treatment to a release into a wetlands treatment system to provide tertiary treatment prior to release to wetlands adjacent to an exceptional value wild trout stream.

Conducted preliminary remediation alternatives analysis for a tidally influenced marsh system in New York. This Superfund site was contaminated with heavy metals and is currently under remediation. The analysis included the location, identification, and observation of bald eagles in the vicinity of the site.

Conducted RTE plant surveys in Susquehanna, Wyoming, Lackawanna, Chester, Delaware, Dauphin and Juniata, Susquehanna and Wyoming Counties, Pennsylvania and assisted with RTE studies of plant populations at various locations in MD and VA.

Conducted water quality surveys, sediment sampling, and quantification of contaminants of coal fired electrical generation plants in response to TMDL documentation.

Provided project scope and budget for teams conducting environmental, cultural and land development permitting acquisition for solar, wind and fossil fuel projects.





Lead team of specialists in habitat assessment and potential impacts assessment of plant and animal species for a proposed pipeline that would impact a portion of the US Forestry Service property. The project was under review by FERC and the timelines were very abbreviated for the review and findings submittal for the Biological Assessment.

Affiliations

Director, PA Certified Drinking Water Laboratory, 1996-2002, 2008-2011 Professional Wetlands Scientist, Society of Wetlands Scientists





July 8, 2024

Bridgeport Stadium 255 Kosuth Street Bridgeport, CT 06608

RE: Floodplain Assessment for Proposed Bridgeport Stadium

BACKGROUND

LaBella is designing a modular soccer stadium and related improvements at 255 Kossuth Road and 141 Stratford Avenue totaling 20.45 acres. The site is currently occupied by an unused dog track and associated 2-story, 47,000 square-foot (sq-ft) building, 1-story, 16,000 sq-ft and a 5-acre parking lot (see Figure 1). The project site is in the floodplain fringe of Zone AE (100-year) Special Flood Hazard Area. It is outside of the 100-year regulatory floodway.

LaBella performed a hydraulic analysis to assess potential impacts resulting from the construction and grading associated with the proposed soccer stadium. The 2013 Fairfield County Flood Insurance Study (FIS) and applicable Flood Insurance Rate Map (FIRM) 09001C0441G illustrate that the existing dog track and 16,000 sq-ft building are within the floodplain fringe. However, the large parking lot and a majority of the 47,000 sq-ft building are outside of the floodplain fringe. The entire site is inundated by the base (100-year) flood, except for the parking lot and a portion of the 47,000 sq-ft building (see Figures 2 and 3).

Per State regulations, any proposed development constructed in a regulated floodplain must result in 1.0 foot or less of rise for the base (100-year) elevation.

PROCEDURE

LaBella utilized the standard FEMA process for assessing floodplain impacts. This typically includes preparing four separate models, which are described as follows.

- 1. Duplicate Effective (DE) Model Reconstruction of an approx. 2,300-foot-long portion of the hydraulic model in a recent version of HEC-RAS. In this instance, the original model was limited to HEC-2 pdf documentation. The tabular HEC-2 data was decoded into excel to provide factors including cross-section points, manning's n-values, downstream distances and bridge opening data. This data was then entered into HEC-RAS to generate the DE model. Cross-sections from upstream to downstream included:
 - a. Section A (0.116);
 - b. Intermediate section just downstream of the Route 130 bridge (0.131);
 - c. Section B (0.257);
 - d. Intermediate section (0.390) between B and C; and
 - e. Section C (0.437).

The Route 130 bridge (near Section 0.131) was modeled as a special bridge and used a pressure and weir submerged inlet and outlet coefficient of discharge of 1.56. The bounding cross-sections for the Route 130 bridge were 0.257 and 0.131. Cross-section 0.131 contained a variety of high



points, which were interpreted to be piers or piles for the bridge. The high points were left in place for the DE model.

Cross-section 0.390 appeared to fall in line with the Conrail bridge. The HEC-2 model did not use a bridge code at this location and therefore the Conrail bridge was left as a cross-section. The cross-section had a variety of high points, which were interpreted to be piers or piles for the bridge.

Cross-sections A, B and C are shown on the FEMA insurance rate map (FIRM), however the intermediate cross-section locations are not known.

2. **Corrected Effective (CE) Model** – This model is a copy of the DE model, which was updated to reflect existing survey topography.

Changes to the model were made to improve modeling of the Route 130 bridge, including:

- Changing coefficient of discharge to 0.8 (from 1.56);
- Removing high points from cross-section 0.131;
- Adding 7 piers to the bridge section;
- Creating bounding cross-section 0.150 by duplicating the edited cross-section 0.131; and
- Changing Deck/Roadway distance to 1 foot (from 600 feet) due to the addition of crosssection 0.131.

Per FEMA standards, downstream reach lengths and manning's n-values were not changed from the DE to CE model.

3. **Existing Conditions Model** – This model is a copy of the CE model. Model updates were limited to adding two blocked obstructions to cross-section 0.257, which represent the dog track buildings that were constructed after publication of the original FEMA HEC-2 model data.

Per FEMA standards, downstream reach lengths and manning's n-values were not changed from the CE to Existing Conditions model.

4. Proposed Conditions Model – This model is a copy of the Existing Conditions model, which was updated to reflect proposed grading changes associated with the proposed soccer stadium at FEMA cross-section B (0.257). Note that cross-section B is roughly in line with the northern end of the stadium. The remaining cross-sections were not changed since they are outside of the project area.

Per FEMA standards, downstream reach lengths and manning's n-values were not changed from the Existing Conditions model to Proposed Conditions model.

The models each utilized subcritical flow. Downstream boundary conditions for the 100-year flow for the three scenarios included:

- 100-year flow with no tide (3.6 feet);
- 100-year flow with tide (9.8 feet); and
- 100-year flow with tidal plus surge (12.0 feet).



RESULTS AND CONCLUSIONS

A comparison of the DE and CE model results indicate no change in the water surface profile for the first two scenarios. However, there was a 0.01-foot increase in the '100-year flow plus tidal surge' scenario at cross-sections 0.437, 0.390 and 0.257. This change appears to be due to the change in orifice coefficient at the Route 130 bridge. Downstream of the bridge, the DE and CE profiles match for all three scenarios. Per FEMA standards, all profiles match, respectively, the specified water surface elevations of 3.6, 9.8 or 12.0 feet at Section A (downstream end of model).

A comparison of the CE, Existing Conditions and Proposed Conditions models indicates no change in water surface profiles for the entire 2,300-foot-long model reach. Per FEMA standards, all profiles match, respectively, the specified water surface elevations of 3.6, 9.8 or 12.0 feet at Section A (downstream end of model) for each scenario.

Therefore, it is concluded that the project does not cause a rise in the 100-year flood level and meets FEMA standards. The models also demonstrate that the study reach of the Pequonnock River is generally controlled by backwater starting at Section A and continuing upstream. A Letter of Map Change is not required at this time.

Respectfully submitted,

Sett Erles

LaBella Associates

Seth Erlich, PE, CFM Senior Civil Engineer

Cc: Stuart Mesinger

FIGURE 1 - PROJECT SITE LOCATION MAP

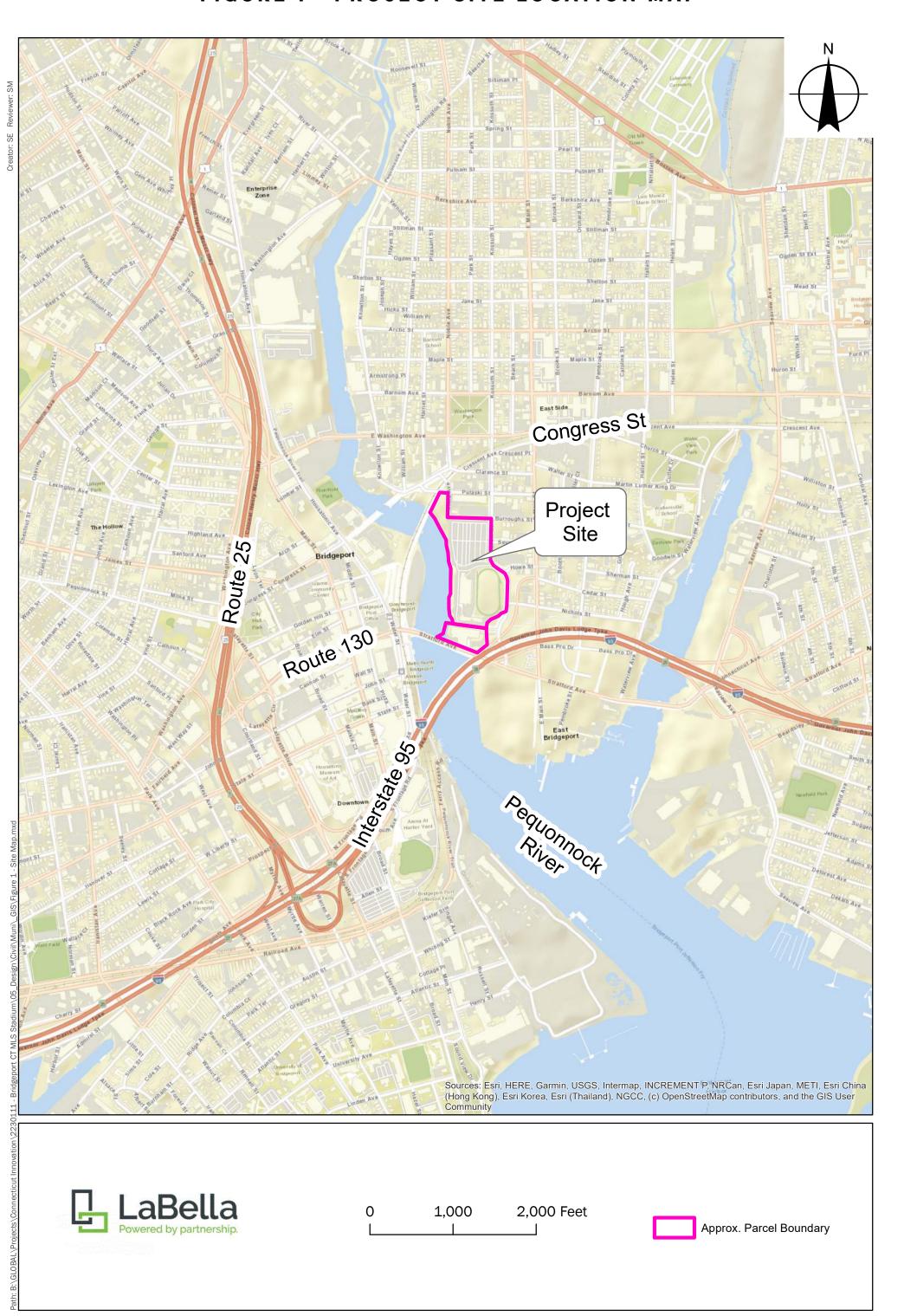


FIGURE 2 - EXISTING CONDITIONS

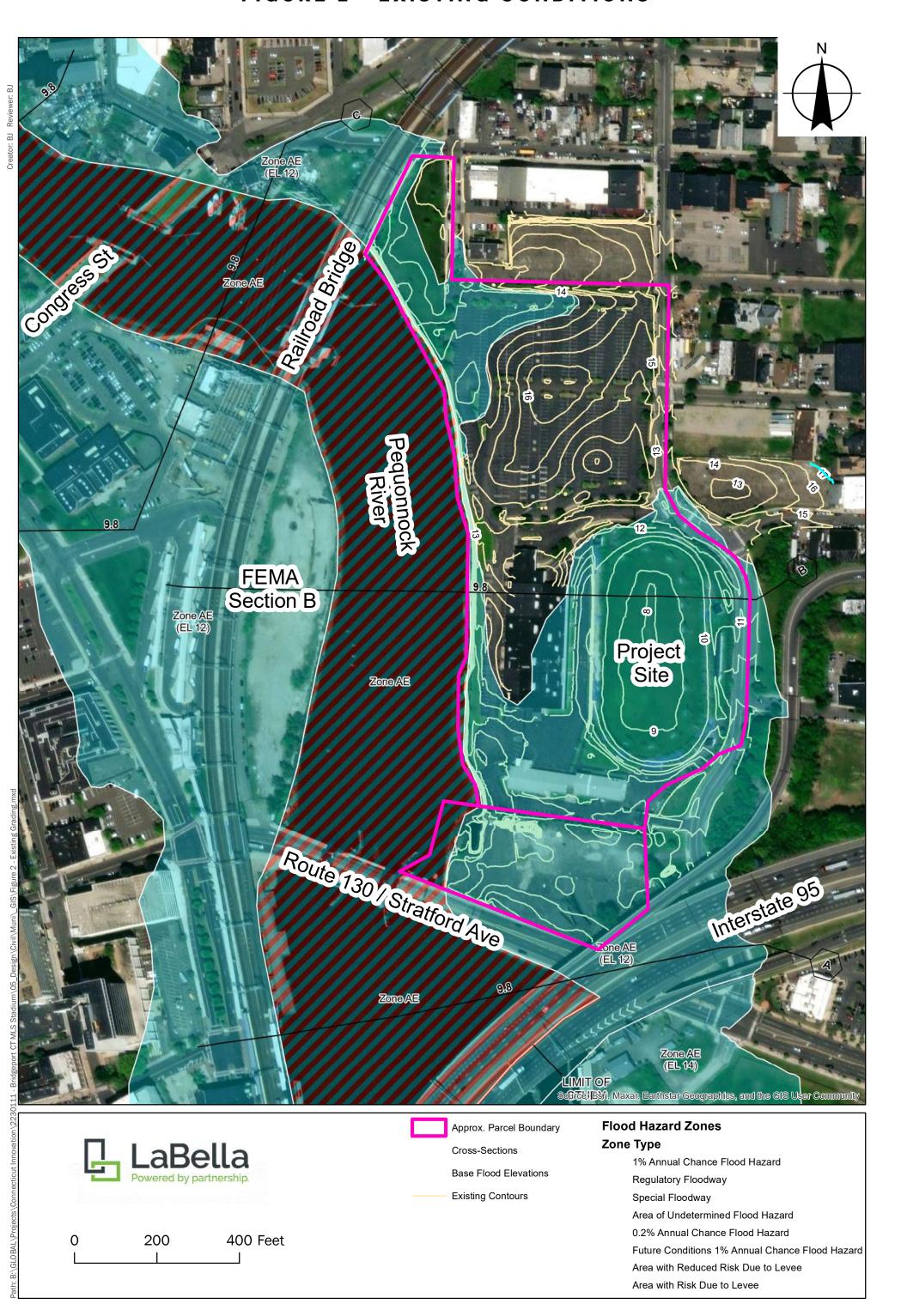
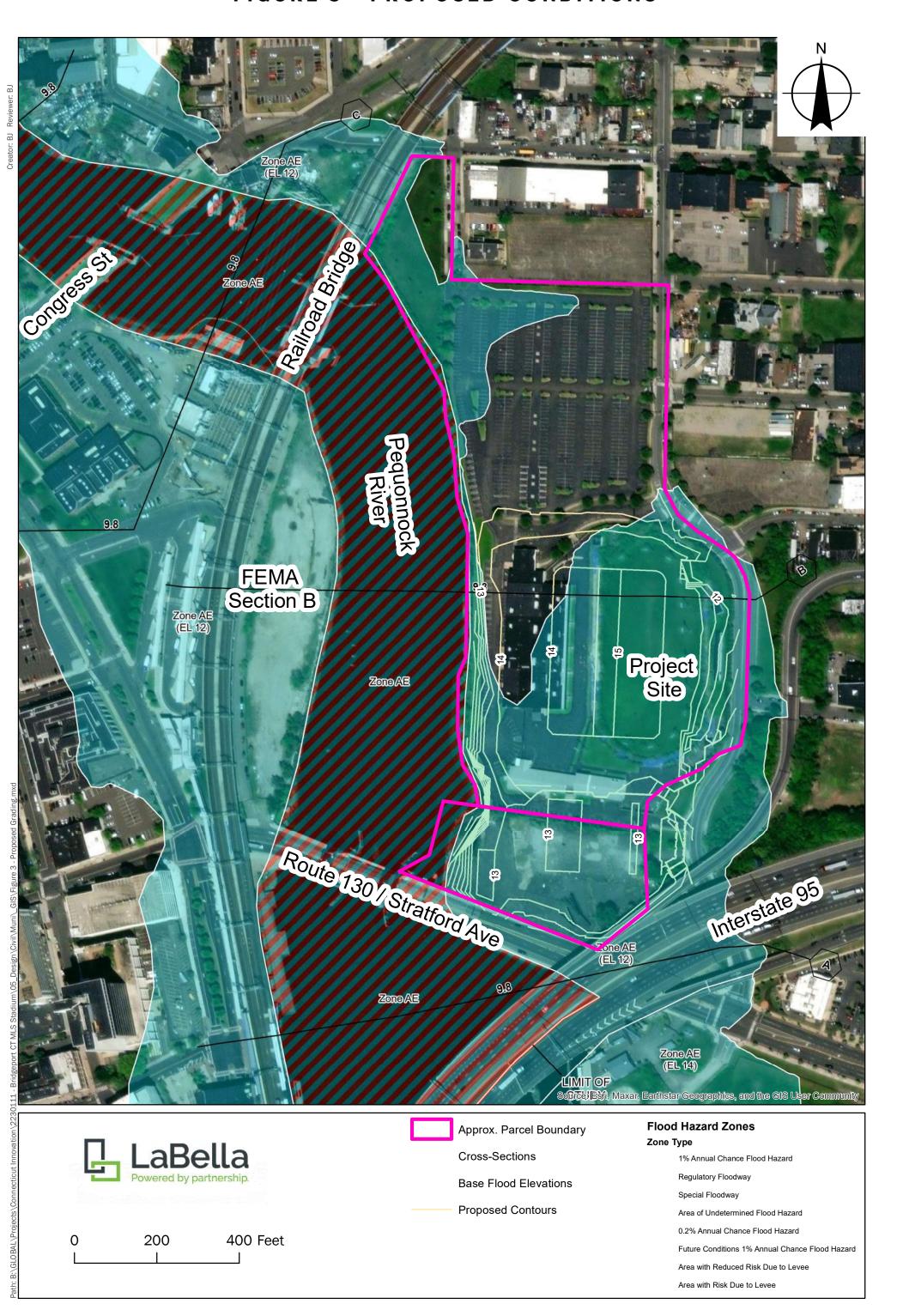
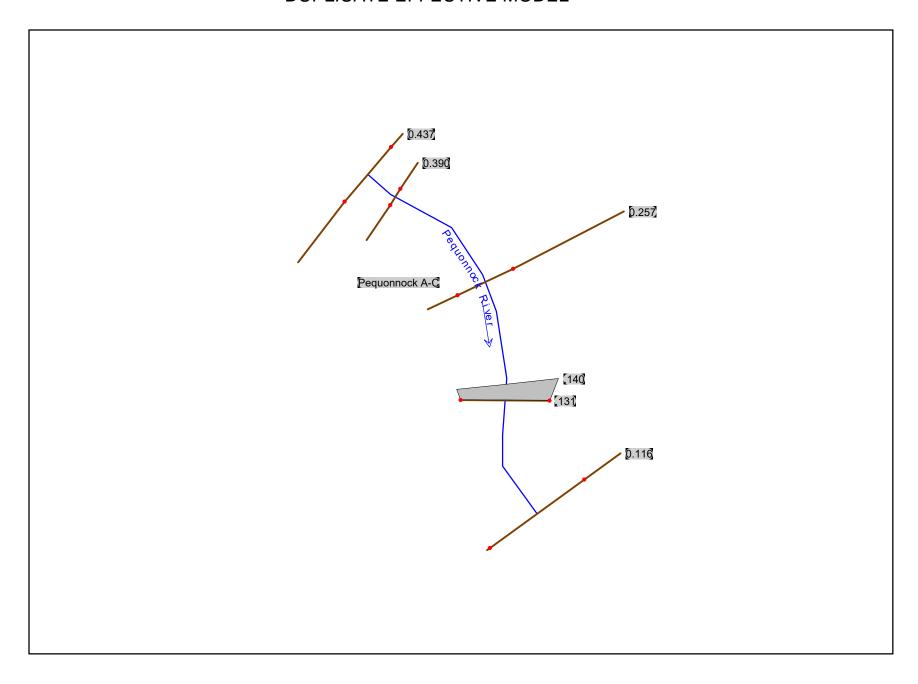
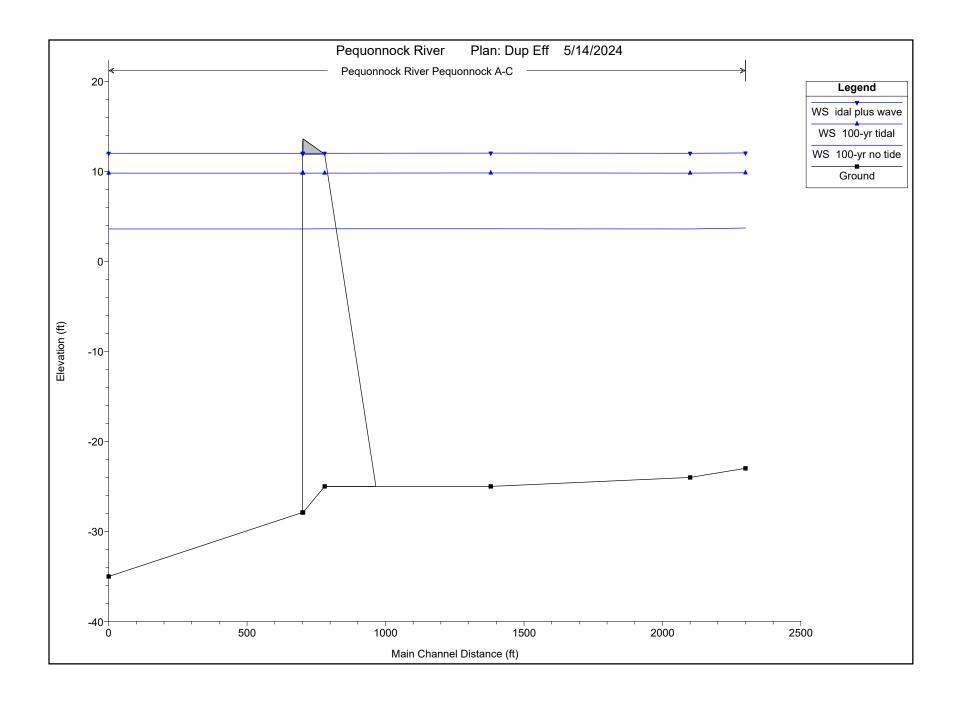


FIGURE 3 - PROPOSED CONDITIONS



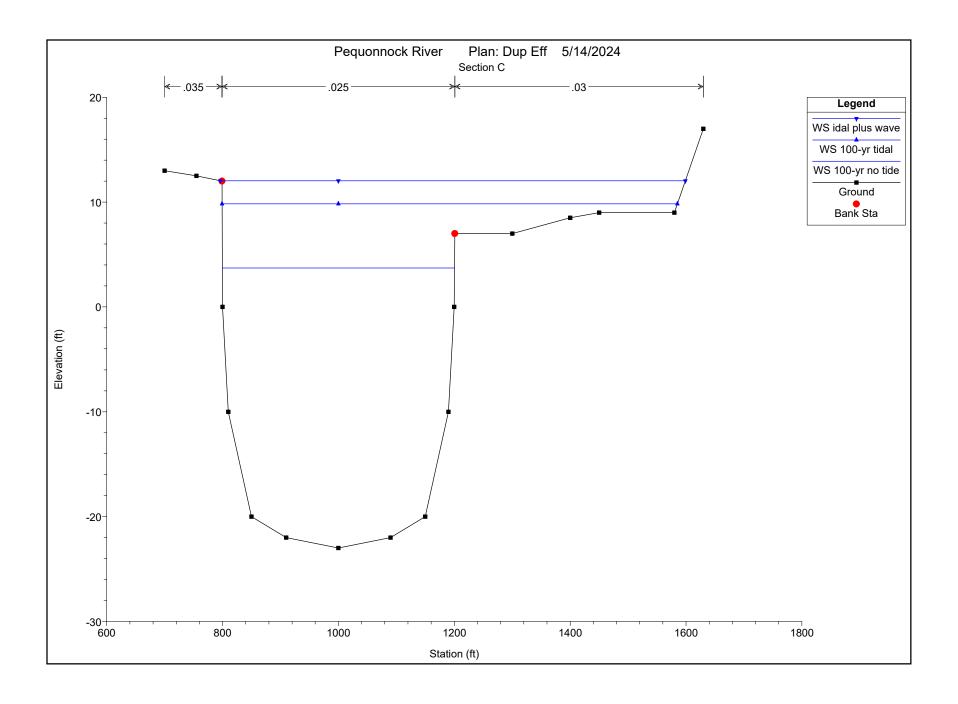
DUPLICATE EFFECTIVE MODEL

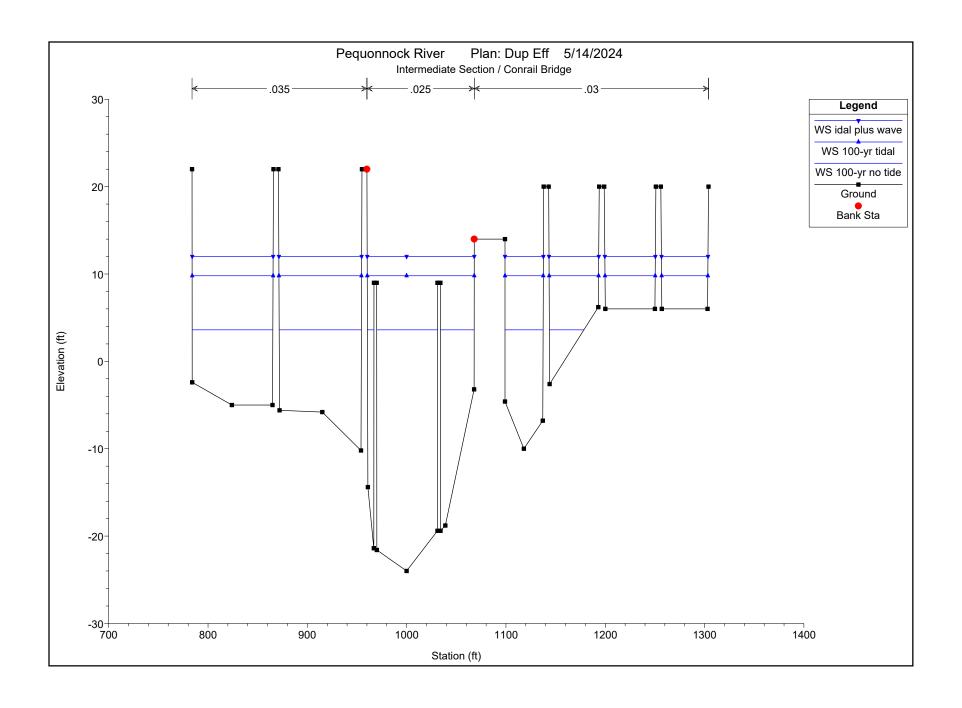


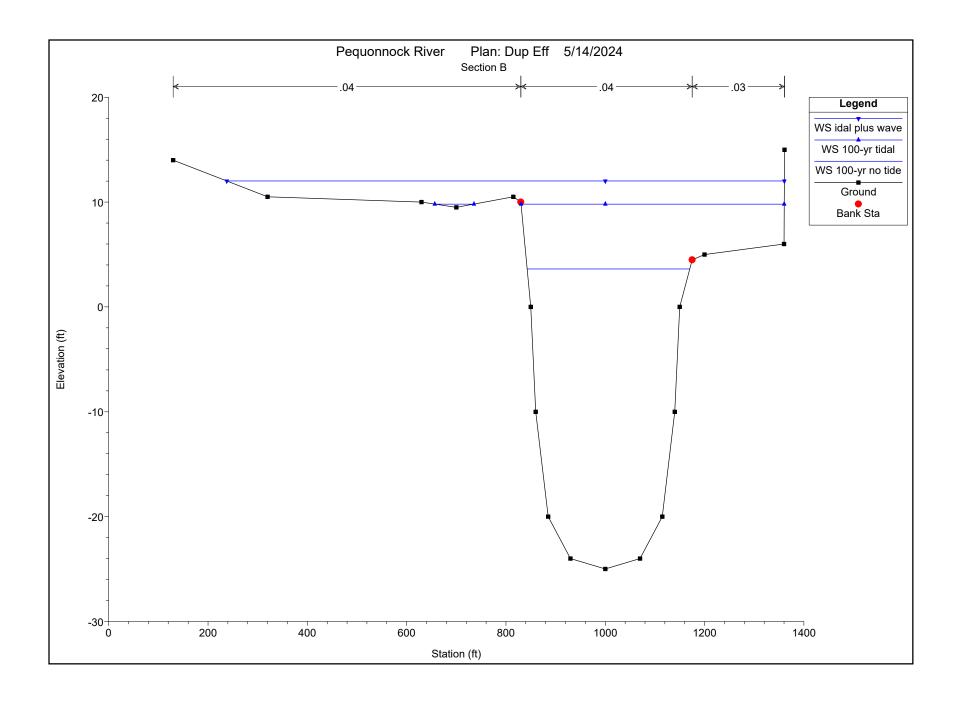


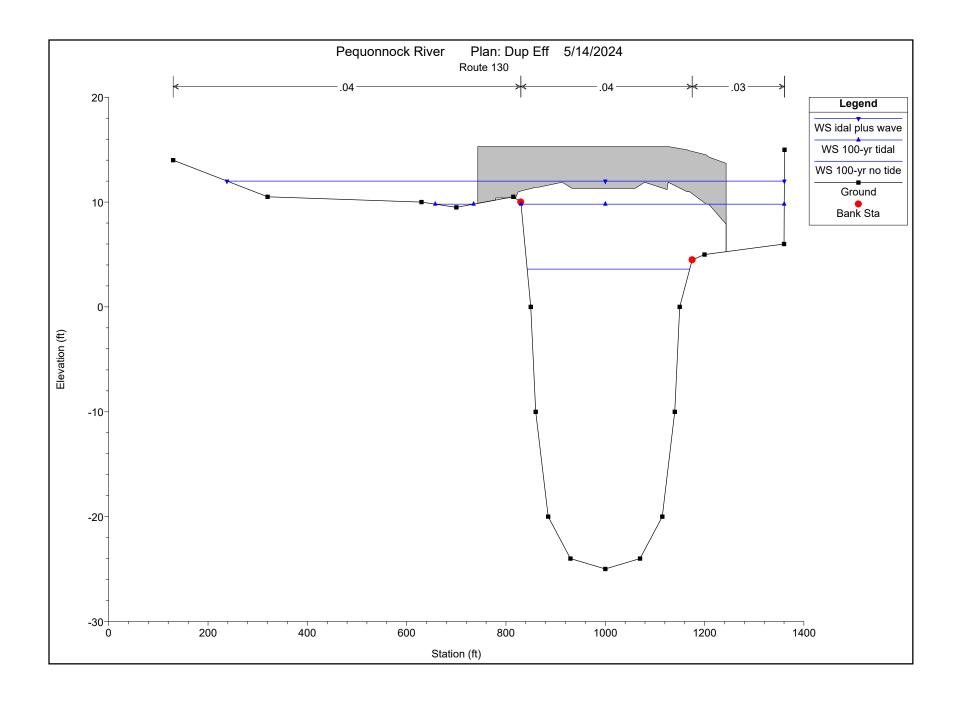
HEC-RAS Plan: DE River: Pequonnock River Reach: Pequonnock A-C

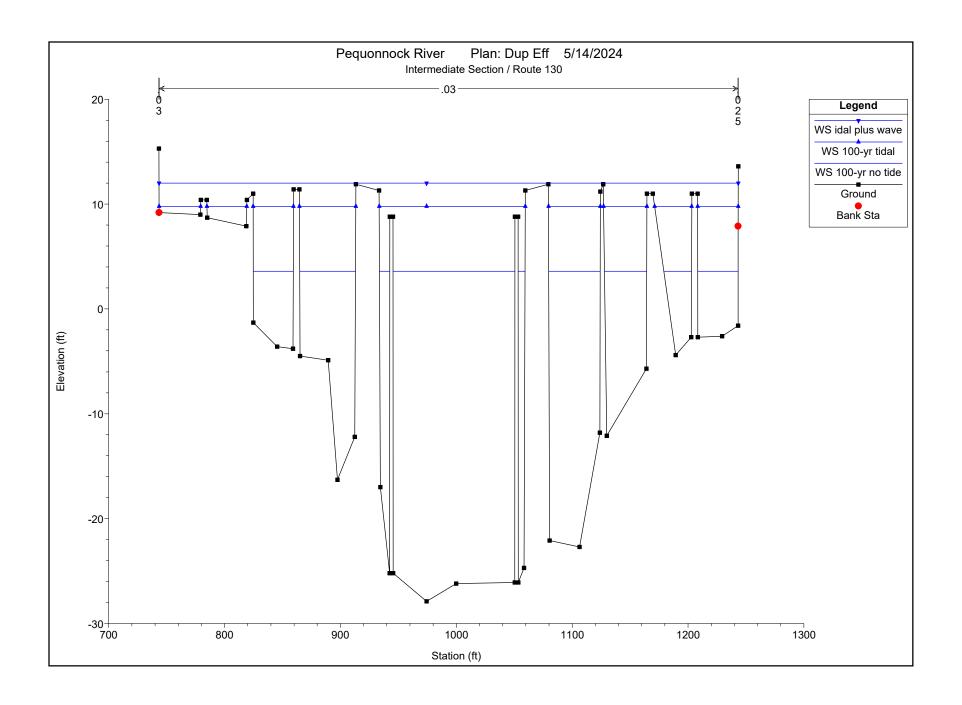
| Reach | River Sta | Profile | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chnl | Flow Area | Top Width | Froude # Chl |
|----------------|-----------|----------------|---------|-----------|-----------|-----------|-----------|------------|----------|-----------|-----------|--------------|
| | | | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft/ft) | (ft/s) | (sq ft) | (ft) | |
| Pequonnock A-C | 0.437 | 100-yr no tide | 9560.00 | -23.00 | 3.71 | | 3.72 | 0.000005 | 1.02 | 9354.74 | 400.84 | 0.04 |
| Pequonnock A-C | 0.437 | 100-yr tidal | 9560.00 | -23.00 | 9.84 | | 9.85 | 0.000002 | 0.80 | 12473.04 | 786.07 | 0.03 |
| Pequonnock A-C | 0.437 | idal plus wave | 9560.00 | -23.00 | 12.03 | | 12.04 | 0.000002 | 0.73 | 14212.71 | 802.99 | 0.02 |
| Pequonnock A-C | 0.390 | 100-yr no tide | 9560.00 | -24.00 | 3.60 | | 3.69 | 0.000101 | 2.74 | 4295.22 | 338.91 | 0.10 |
| Pequonnock A-C | 0.390 | 100-yr tidal | 9560.00 | -24.00 | 9.81 | | 9.84 | 0.000101 | 1.70 | 6846.21 | 457.91 | 0.06 |
| Pequonnock A-C | 0.390 | idal plus wave | 9560.00 | -24.00 | 12.01 | | 12.03 | 0.000024 | 1.48 | 7856.47 | 459.21 | 0.05 |
| | | | | | | | | | | | | |
| Pequonnock A-C | 0.257 | 100-yr no tide | 9560.00 | -25.00 | 3.62 | -19.76 | 3.64 | 0.000020 | 1.29 | 7395.02 | 327.34 | 0.05 |
| Pequonnock A-C | 0.257 | 100-yr tidal | 9560.00 | -25.00 | 9.81 | -19.76 | 9.82 | 0.000009 | 0.97 | 10316.54 | 608.73 | 0.03 |
| Pequonnock A-C | 0.257 | idal plus wave | 9560.00 | -25.00 | 12.01 | -19.76 | 12.02 | 0.000006 | 0.87 | 12497.22 | 1122.72 | 0.03 |
| Pequonnock A-C | .140 | | Bridge | | | | | | | | | |
| Pequonnock A-C | .131 | 100-yr no tide | 9560.00 | -27.90 | 3.59 | | 3.63 | 0.000047 | 1.55 | 6178.19 | 342.44 | 0.06 |
| Pequonnock A-C | .131 | 100-yr tidal | 9560.00 | -27.90 | 9.79 | | 9.81 | 0.000024 | 1.14 | 8418.11 | 429.21 | 0.05 |
| Pequonnock A-C | .131 | idal plus wave | 9560.00 | -27.90 | 12.00 | | 12.01 | 0.000019 | 1.02 | 9412.24 | 499.92 | 0.04 |
| | | | | | | | | | | | | |
| Pequonnock A-C | 0.116 | 100-yr no tide | 9560.00 | -35.00 | 3.60 | -29.80 | 3.60 | 0.000001 | 0.52 | 18504.34 | 651.65 | 0.02 |
| Pequonnock A-C | 0.116 | 100-yr tidal | 9560.00 | -35.00 | 9.80 | -29.80 | 9.80 | 0.000001 | 0.42 | 22597.95 | 698.57 | 0.01 |
| Pequonnock A-C | 0.116 | idal plus wave | 9560.00 | -35.00 | 12.00 | -29.80 | 12.00 | 0.000001 | 0.40 | 24512.47 | 891.00 | 0.01 |

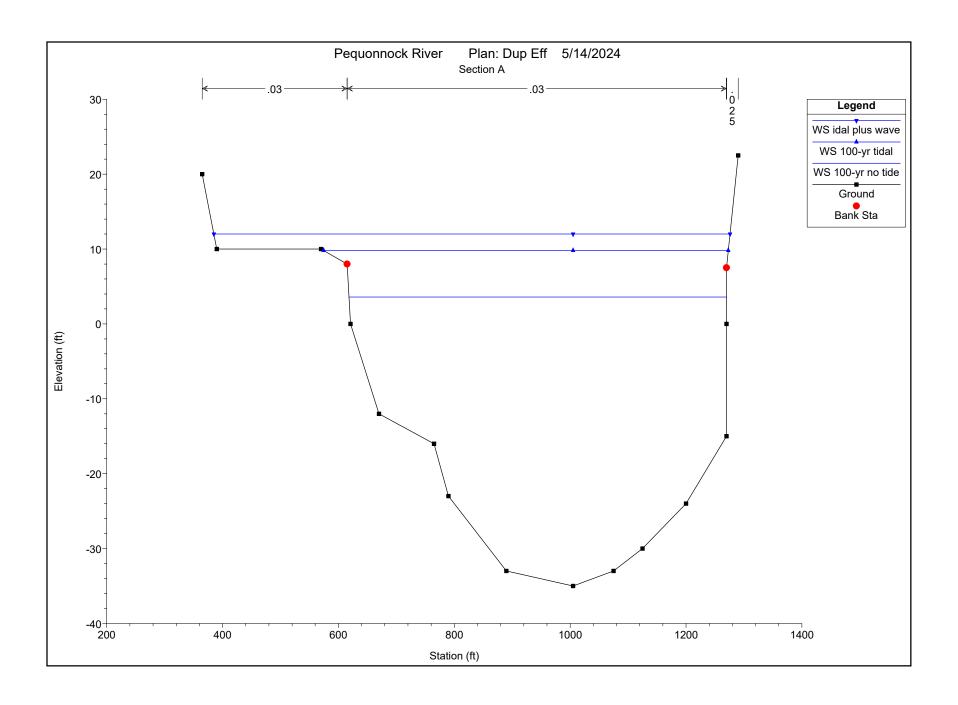




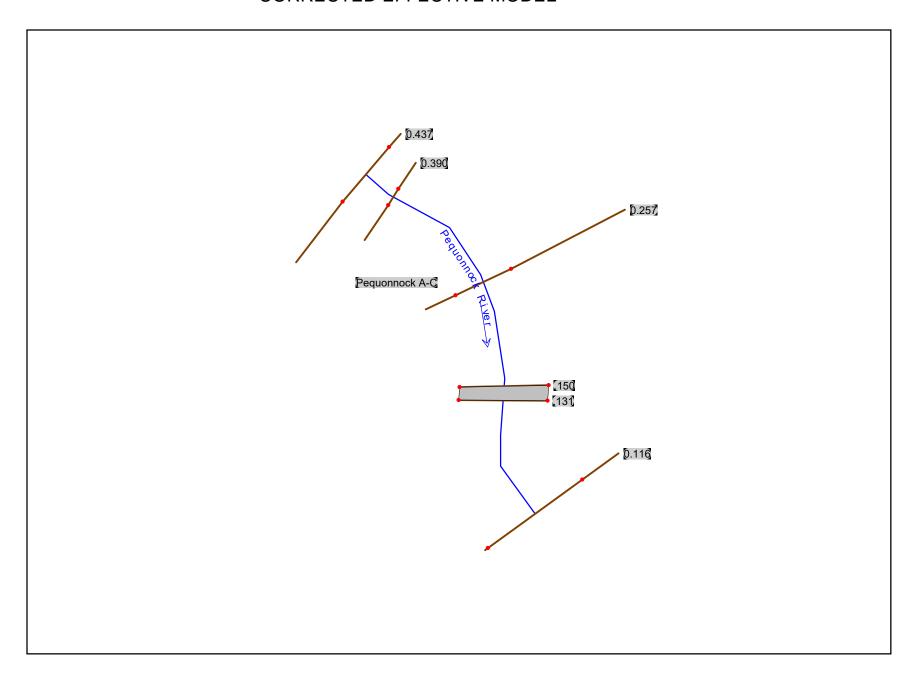


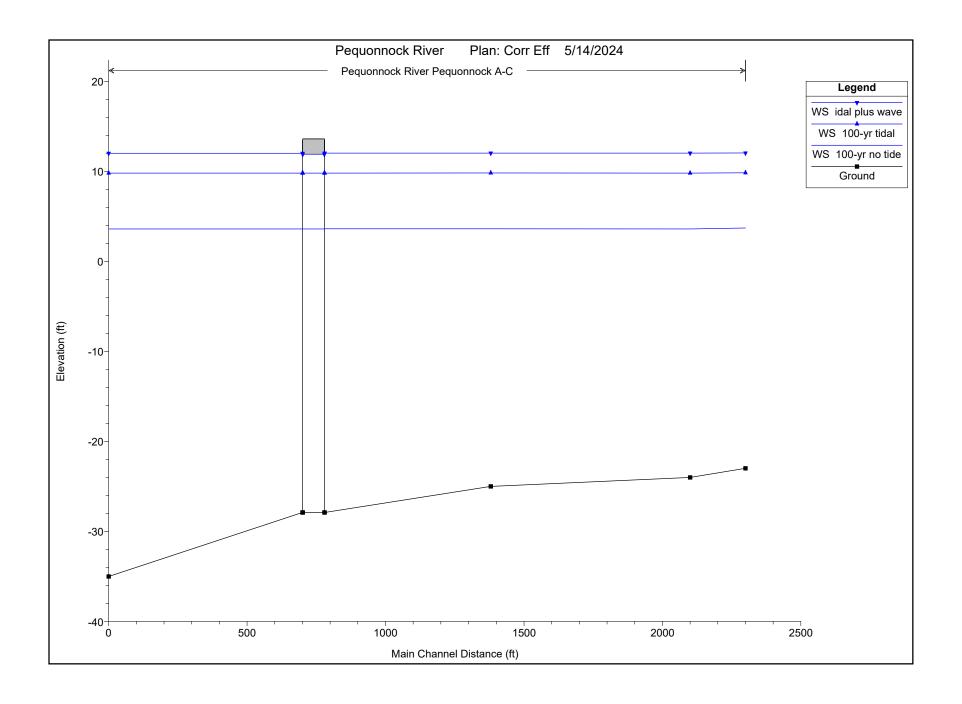






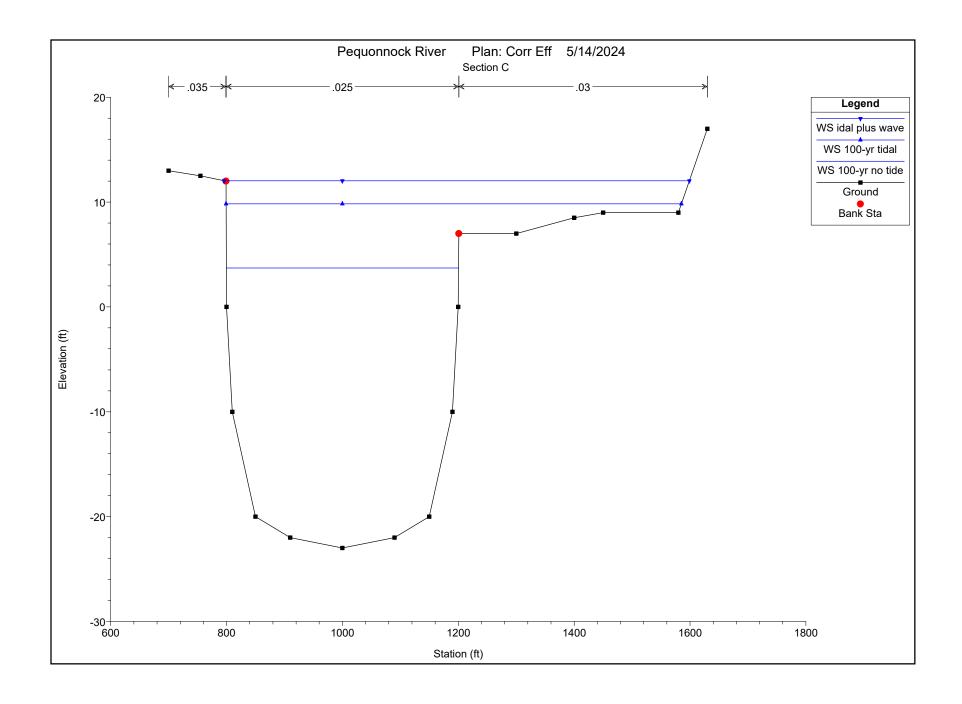
CORRECTED EFFECTIVE MODEL

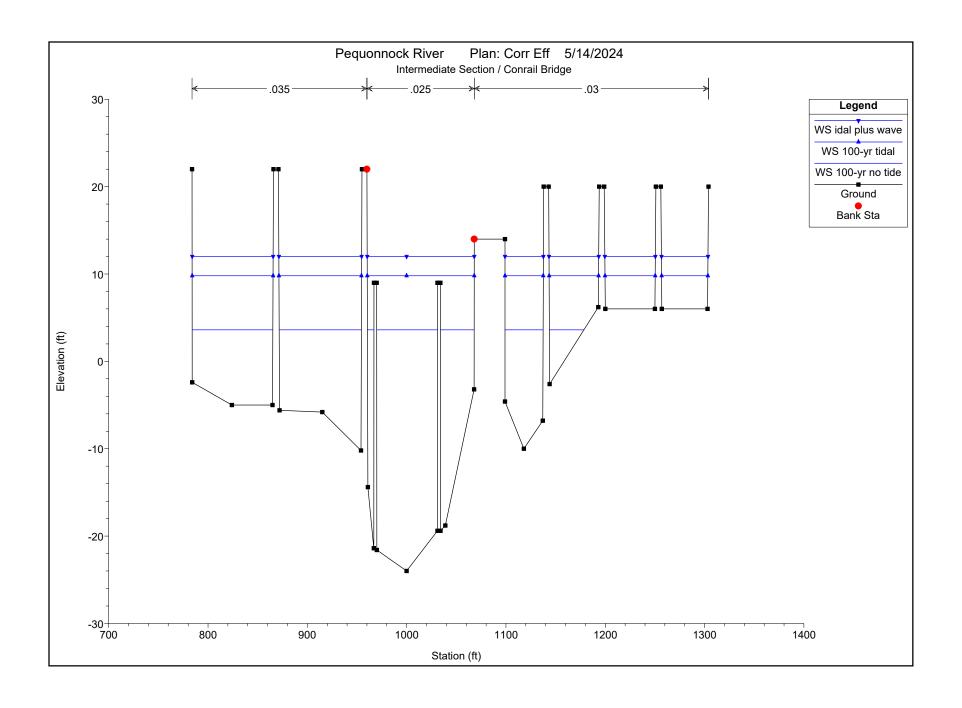


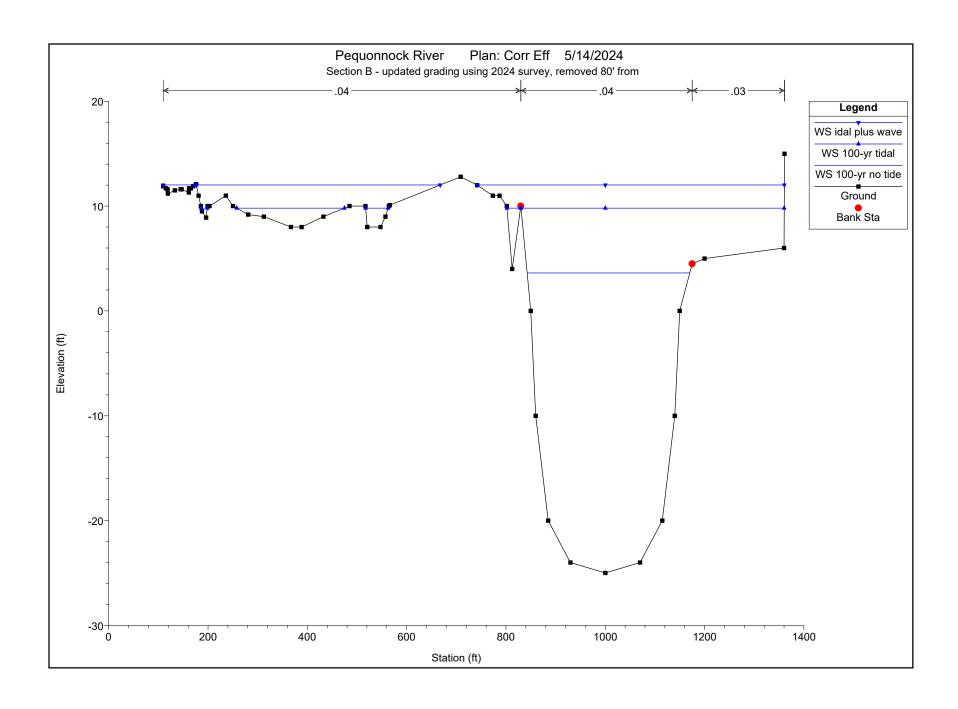


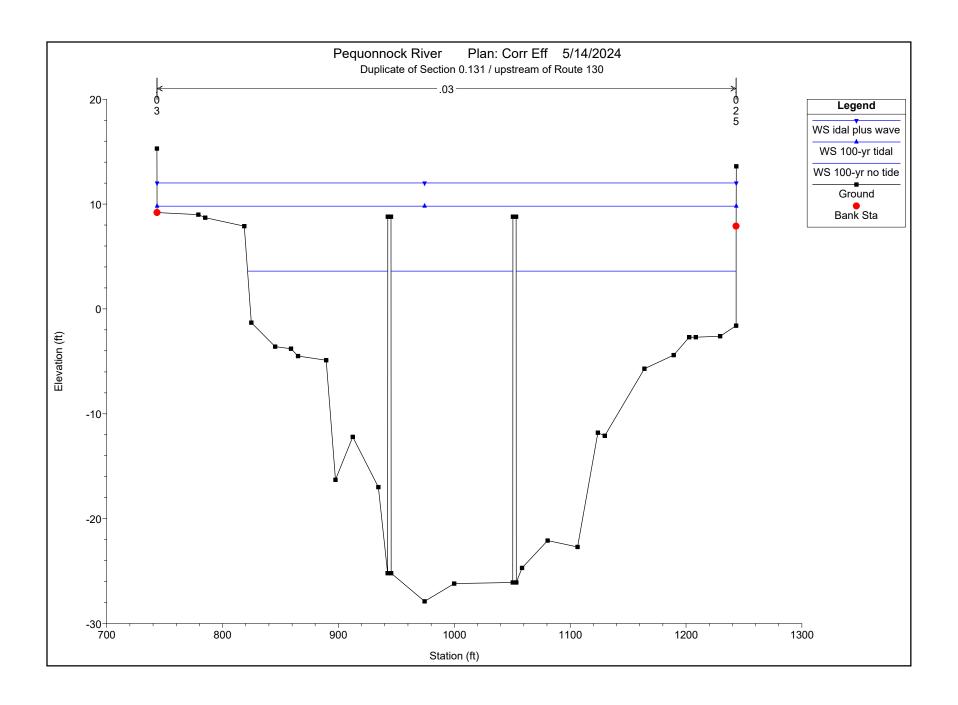
HEC-RAS Plan: CE River: Pequonnock River Reach: Pequonnock A-C

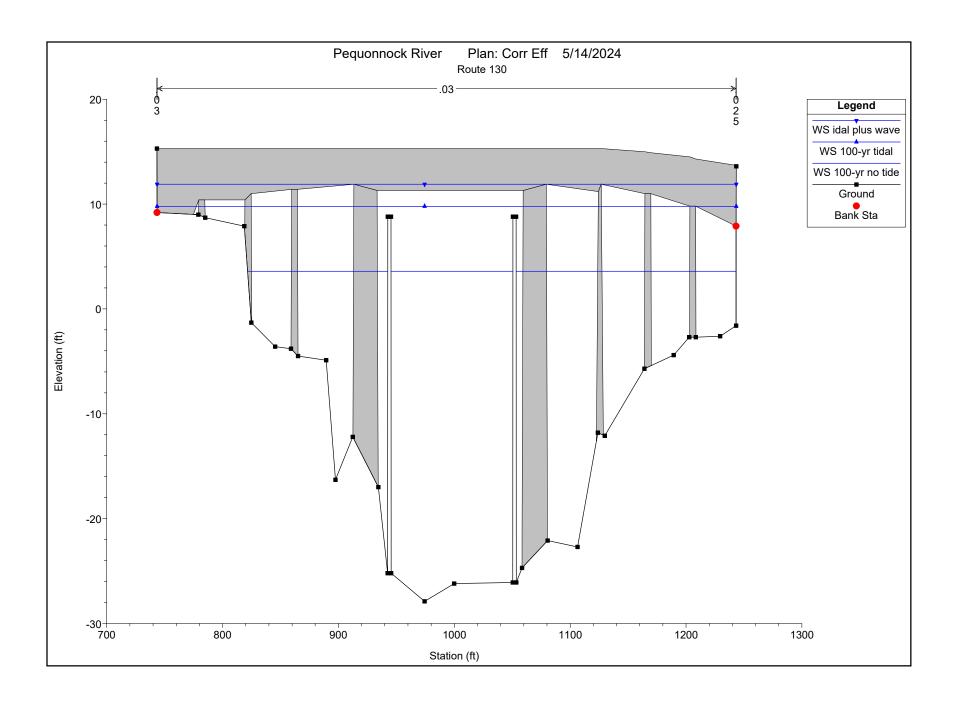
| Reach | River Sta | Profile | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chnl | Flow Area | Top Width | Froude # Chl |
|----------------------|-----------|----------------|---------|-----------|-----------|-----------|-----------|------------|----------|-----------|-----------|--------------|
| | | | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft/ft) | (ft/s) | (sq ft) | (ft) | |
| Pequonnock A-C | 0.437 | 100-yr no tide | 9560.00 | -23.00 | 3.71 | | 3.72 | 0.000005 | 1.02 | 9354.86 | 400.84 | 0.04 |
| Pequonnock A-C | 0.437 | 100-yr tidal | 9560.00 | -23.00 | 9.84 | | 9.85 | 0.000002 | 0.80 | 12473.34 | 786.08 | 0.03 |
| Pequonnock A-C | 0.437 | idal plus wave | 9560.00 | -23.00 | 12.04 | | 12.05 | 0.000002 | 0.73 | 14217.58 | 803.57 | 0.02 |
| | | | | | | | | | | | | |
| Pequonnock A-C | 0.390 | 100-yr no tide | 9560.00 | -24.00 | 3.60 | | 3.69 | 0.000101 | 2.74 | 4295.32 | 338.91 | 0.10 |
| Pequonnock A-C | 0.390 | 100-yr tidal | 9560.00 | -24.00 | 9.81 | | 9.84 | 0.000035 | 1.70 | 6846.39 | 457.91 | 0.06 |
| Pequonnock A-C | 0.390 | idal plus wave | 9560.00 | -24.00 | 12.02 | | 12.04 | 0.000024 | 1.48 | 7859.26 | 459.21 | 0.05 |
| Peguonnock A-C | 0.257 | 100-yr no tide | 9560.00 | -25.00 | 3.62 | | 3.64 | 0.000020 | 1.29 | 7395.12 | 327.34 | 0.05 |
| Pequonnock A-C | 0.257 | 100-yr tidal | 9560.00 | -25.00 | 9.81 | | 9.82 | 0.000020 | 0.97 | 10672.64 | 832.93 | 0.03 |
| Pequonnock A-C | 0.257 | idal plus wave | 9560.00 | -25.00 | 12.02 | | 12.03 | 0.000009 | 0.86 | 12893.53 | 1174.14 | 0.03 |
| r oquoriniosit / t o | 0.207 | luai pias wave | 0000.00 | 20.00 | 12.02 | | 12.00 | 0.00000 | 0.00 | 12000.00 | 117 1.11 | 0.00 |
| Pequonnock A-C | .150 | 100-yr no tide | 9560.00 | -27.90 | 3.61 | -20.52 | 3.63 | 0.000021 | 1.28 | 7485.69 | 415.95 | 0.05 |
| Pequonnock A-C | .150 | 100-yr tidal | 9560.00 | -27.90 | 9.80 | -20.52 | 9.82 | 0.000010 | 0.94 | 10162.39 | 499.84 | 0.04 |
| Pequonnock A-C | .150 | idal plus wave | 9560.00 | -27.90 | 12.01 | -20.52 | 12.02 | 0.000007 | 0.85 | 11266.89 | 499.92 | 0.03 |
| Pequonnock A-C | .140 | | Bridge | | | | | | | | | |
| | | | 3 | | | | | | | | | |
| Pequonnock A-C | .131 | 100-yr no tide | 9560.00 | -27.90 | 3.59 | | 3.62 | 0.000021 | 1.28 | 7480.28 | 415.94 | 0.05 |
| Pequonnock A-C | .131 | 100-yr tidal | 9560.00 | -27.90 | 9.80 | | 9.81 | 0.000010 | 0.94 | 10158.84 | 499.84 | 0.04 |
| Pequonnock A-C | .131 | idal plus wave | 9560.00 | -27.90 | 12.00 | | 12.01 | 0.000007 | 0.85 | 11258.89 | 499.92 | 0.03 |
| | | | | | | | | | | | | |
| Pequonnock A-C | 0.116 | 100-yr no tide | 9560.00 | -35.00 | 3.60 | -29.80 | 3.60 | 0.000001 | 0.52 | 18504.34 | 651.65 | 0.02 |
| Pequonnock A-C | 0.116 | 100-yr tidal | 9560.00 | -35.00 | 9.80 | -29.80 | 9.80 | 0.000001 | 0.42 | 22597.95 | 698.57 | 0.01 |
| Pequonnock A-C | 0.116 | idal plus wave | 9560.00 | -35.00 | 12.00 | -29.80 | 12.00 | 0.000001 | 0.40 | 24512.47 | 891.00 | 0.01 |

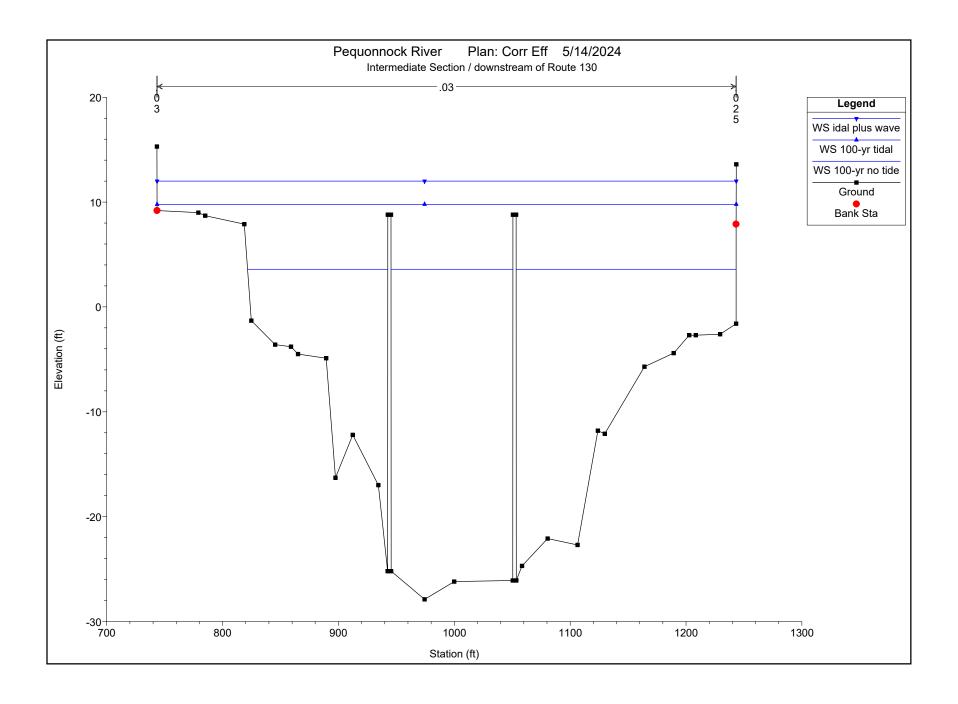


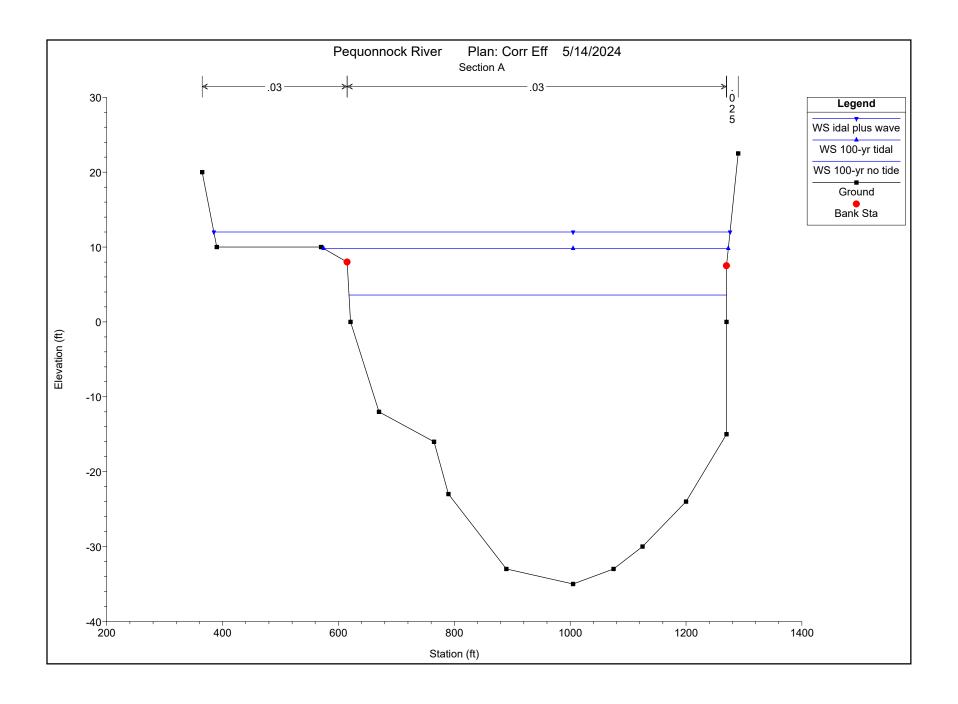




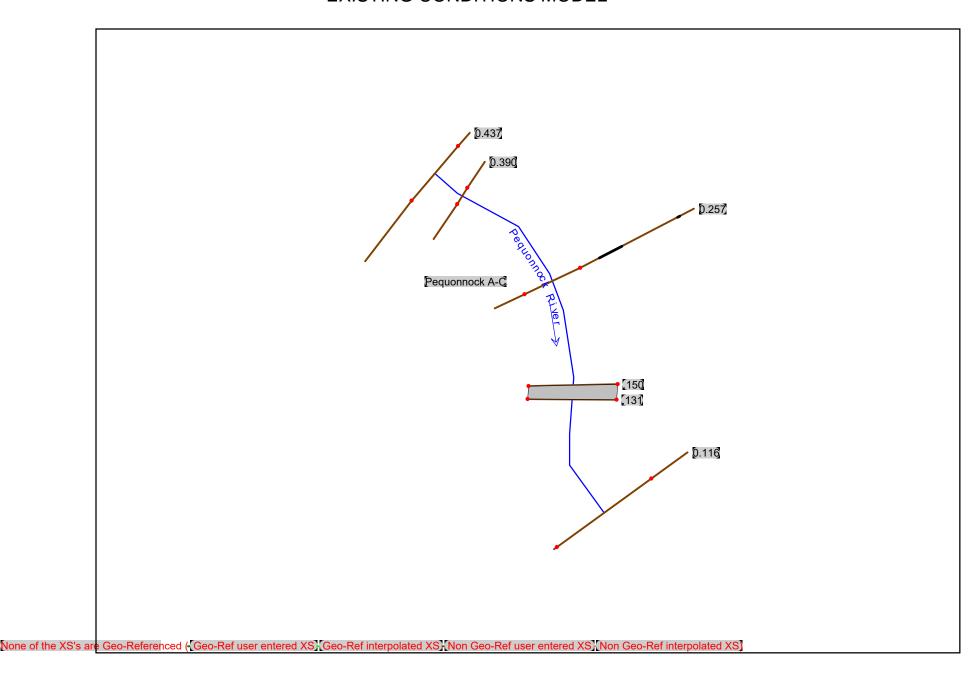


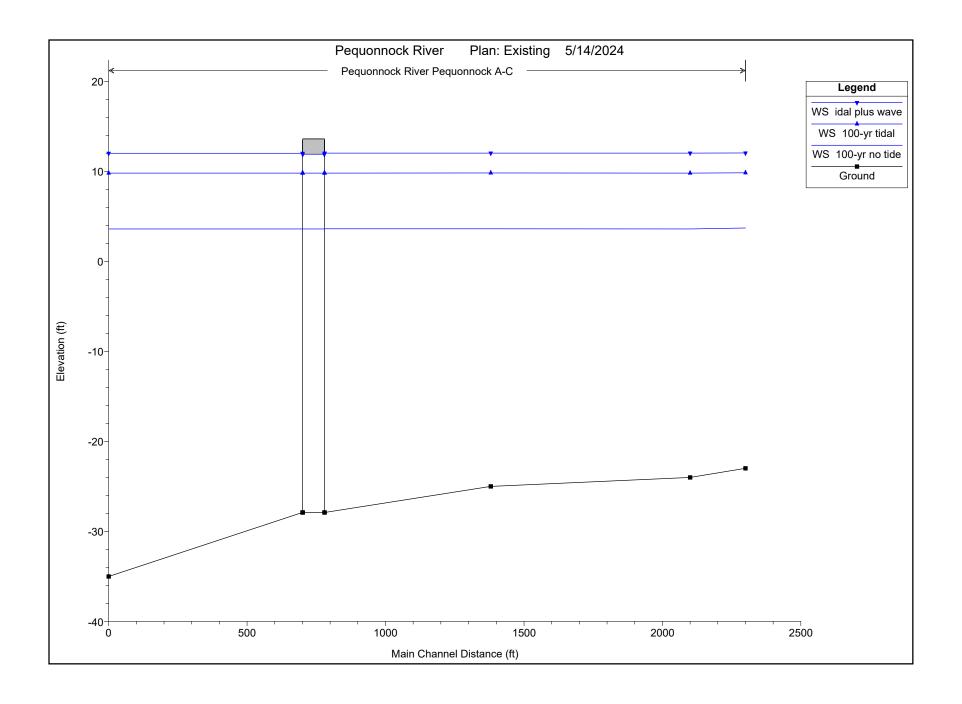






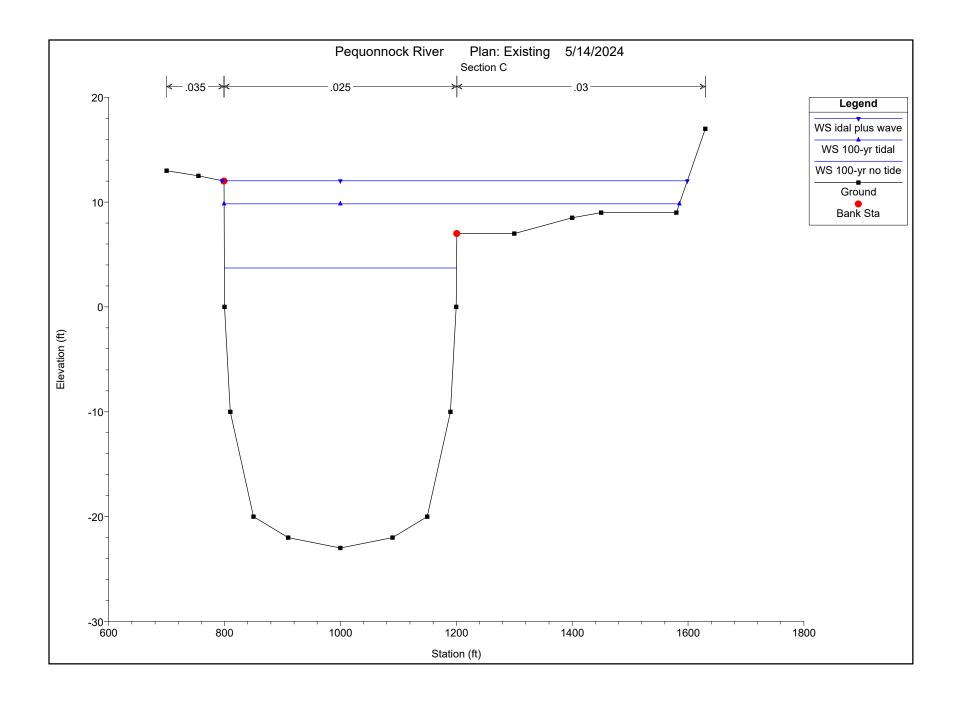
EXISTING CONDITIONS MODEL

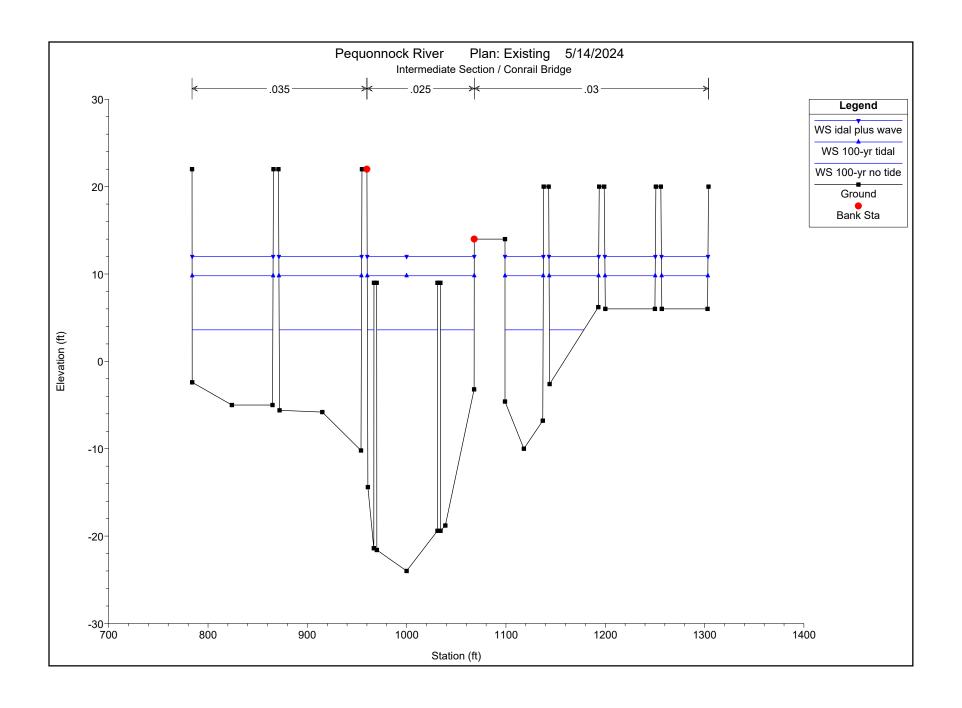


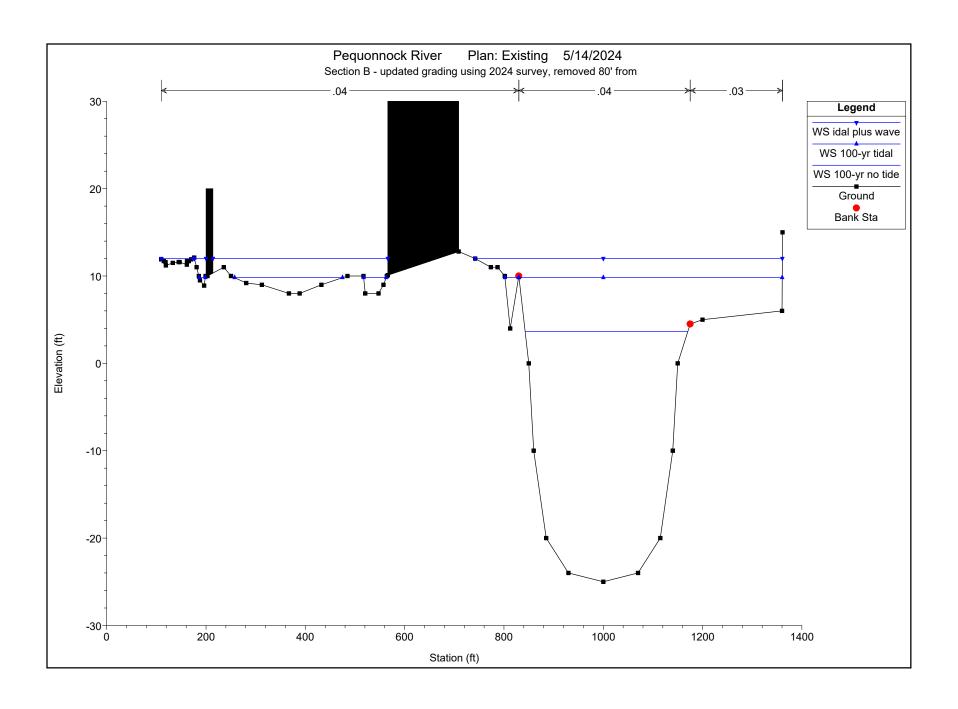


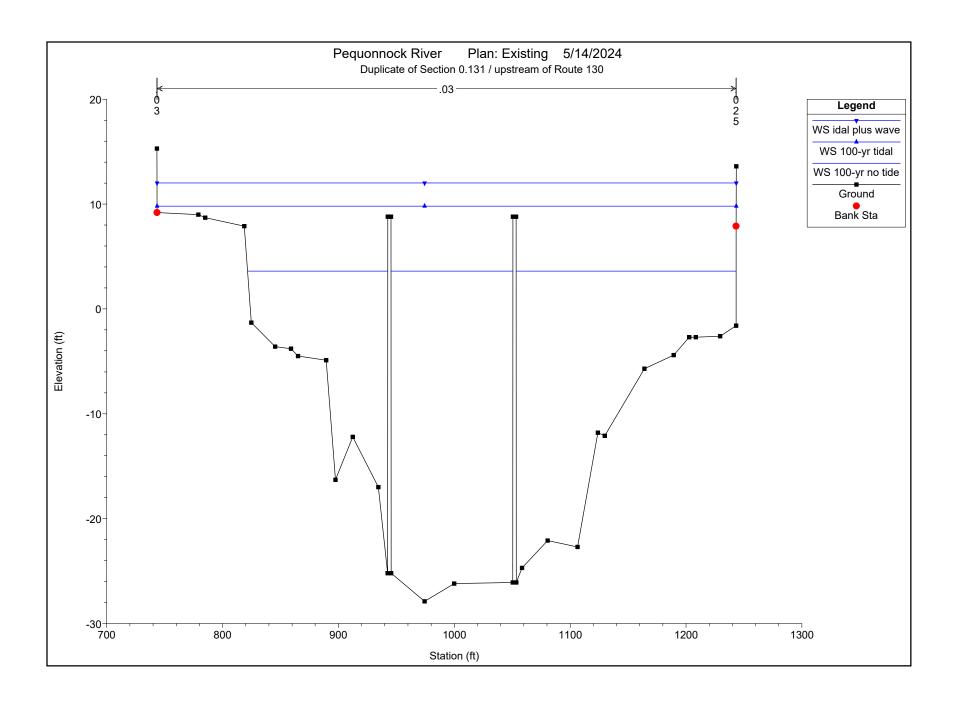
HEC-RAS Plan: Exist River: Pequonnock River Reach: Pequonnock A-C

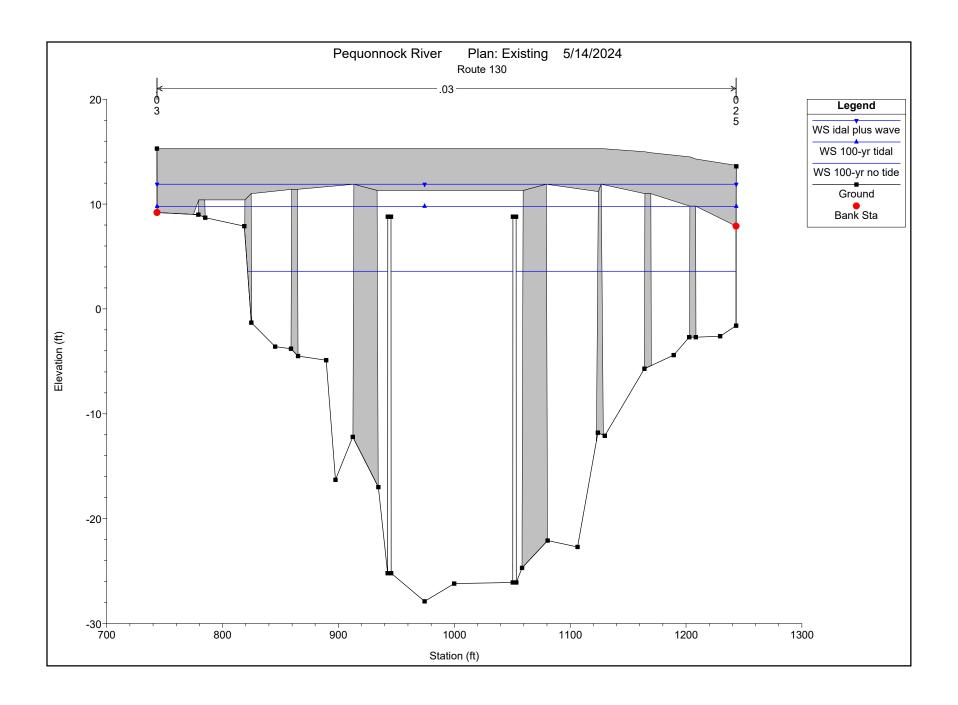
| Reach | River Sta | Profile | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chnl | Flow Area | Top Width | Froude # Chl |
|----------------|-----------|----------------|---------|-----------|-----------|-----------|-----------|------------|----------|-----------|-----------|--------------|
| | | | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft/ft) | (ft/s) | (sq ft) | (ft) | |
| Pequonnock A-C | 0.437 | 100-yr no tide | 9560.00 | -23.00 | 3.71 | | 3.72 | 0.000005 | 1.02 | 9354.86 | 400.84 | 0.04 |
| Pequonnock A-C | 0.437 | 100-yr tidal | 9560.00 | -23.00 | 9.84 | | 9.85 | 0.000002 | 0.80 | 12473.34 | 786.08 | 0.03 |
| Pequonnock A-C | 0.437 | idal plus wave | 9560.00 | -23.00 | 12.04 | | 12.05 | 0.000002 | 0.73 | 14217.58 | 803.57 | 0.02 |
| Pequonnock A-C | 0.390 | 100-yr no tide | 9560.00 | -24.00 | 3.60 | | 3.69 | 0.000101 | 2.74 | 4295.32 | 338.91 | 0.10 |
| Pequonnock A-C | 0.390 | 100-yr tidal | 9560.00 | -24.00 | 9.81 | | 9.84 | 0.000035 | 1.70 | 6846.39 | 457.91 | 0.06 |
| Pequonnock A-C | 0.390 | idal plus wave | 9560.00 | -24.00 | 12.02 | | 12.04 | 0.000024 | 1.48 | 7859.26 | 459.21 | 0.05 |
| Pequonnock A-C | 0.257 | 100-yr no tide | 9560.00 | -25.00 | 3.62 | | 3.64 | 0.000020 | 1.29 | 7395.12 | 327.34 | 0.05 |
| Pequonnock A-C | 0.257 | 100-yr tidal | 9560.00 | -25.00 | 9.81 | | 9.82 | 0.000009 | 0.97 | 10672.64 | 832.93 | 0.03 |
| Pequonnock A-C | 0.257 | idal plus wave | 9560.00 | -25.00 | 12.02 | | 12.03 | 0.000006 | 0.86 | 12769.91 | 1058.77 | 0.03 |
| Pequonnock A-C | .150 | 100-yr no tide | 9560.00 | -27.90 | 3.61 | -20.52 | 3.63 | 0.000021 | 1.28 | 7485.69 | 415.95 | 0.05 |
| Pequonnock A-C | .150 | 100-yr tidal | 9560.00 | -27.90 | 9.80 | -20.52 | 9.82 | 0.000010 | 0.94 | 10162.39 | 499.84 | 0.04 |
| Pequonnock A-C | .150 | idal plus wave | 9560.00 | -27.90 | 12.01 | -20.52 | 12.02 | 0.000007 | 0.85 | 11266.89 | 499.92 | 0.03 |
| Pequonnock A-C | .140 | | Bridge | | | | | | | | | |
| Pequonnock A-C | .131 | 100-yr no tide | 9560.00 | -27.90 | 3.59 | | 3.62 | 0.000021 | 1.28 | 7480.28 | 415.94 | 0.05 |
| Pequonnock A-C | .131 | 100-yr tidal | 9560.00 | -27.90 | 9.80 | | 9.81 | 0.000010 | 0.94 | 10158.84 | 499.84 | 0.04 |
| Pequonnock A-C | .131 | idal plus wave | 9560.00 | -27.90 | 12.00 | | 12.01 | 0.000007 | 0.85 | 11258.89 | 499.92 | 0.03 |
| Pequonnock A-C | 0.116 | 100-yr no tide | 9560.00 | -35.00 | 3.60 | -29.80 | 3.60 | 0.000001 | 0.52 | 18504.34 | 651.65 | 0.02 |
| Pequonnock A-C | 0.116 | 100-yr tidal | 9560.00 | -35.00 | 9.80 | -29.80 | 9.80 | 0.000001 | 0.42 | 22597.95 | 698.57 | 0.01 |
| Pequonnock A-C | 0.116 | idal plus wave | 9560.00 | -35.00 | 12.00 | -29.80 | 12.00 | 0.000001 | 0.40 | 24512.47 | 891.00 | 0.01 |

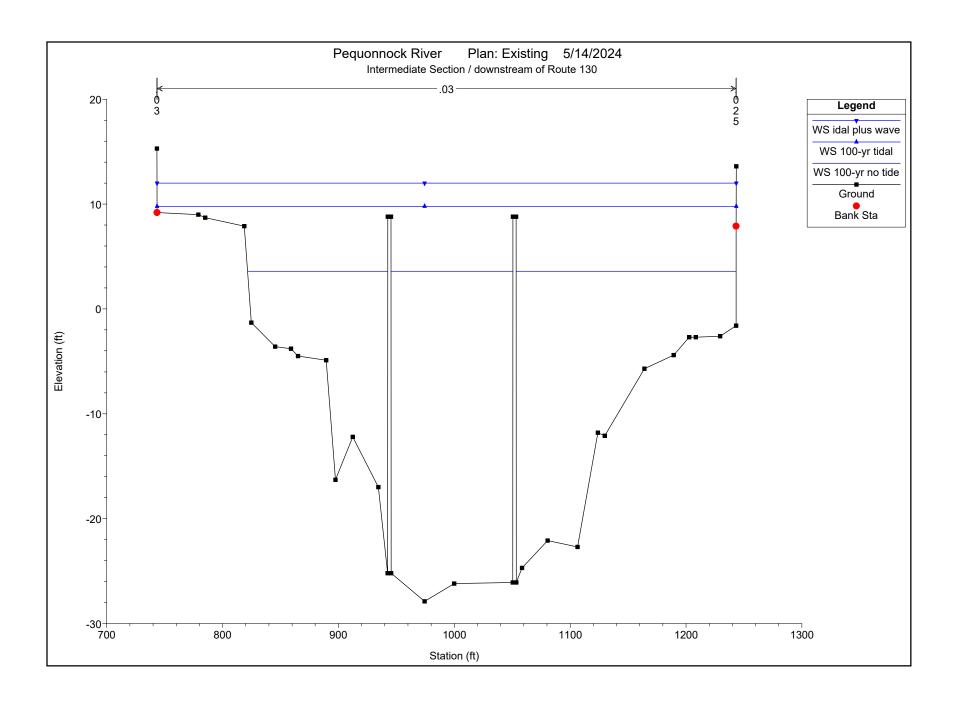


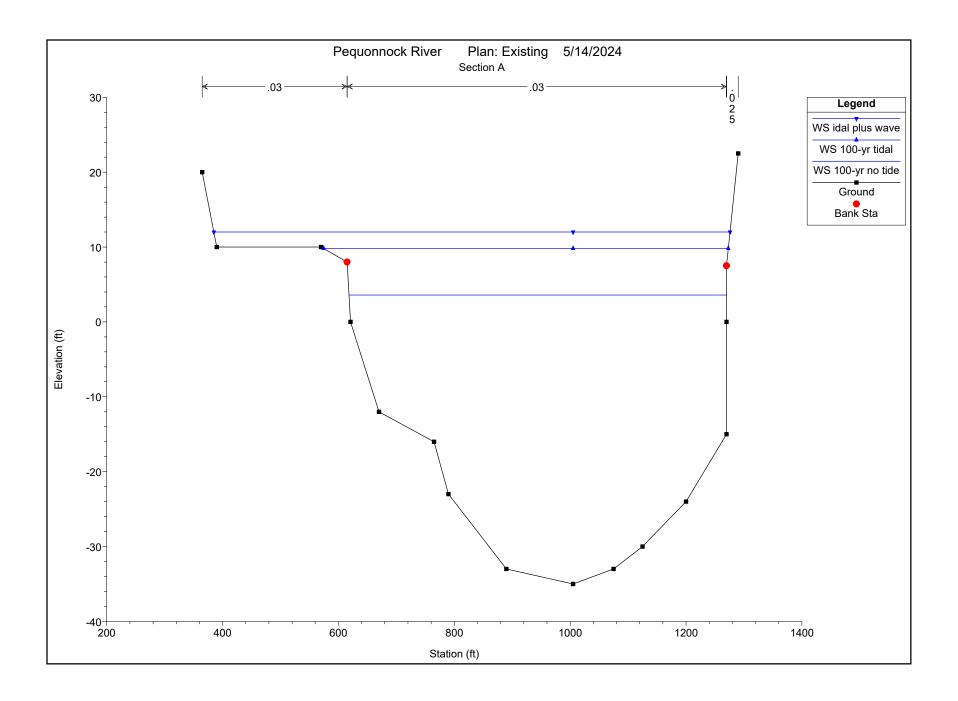




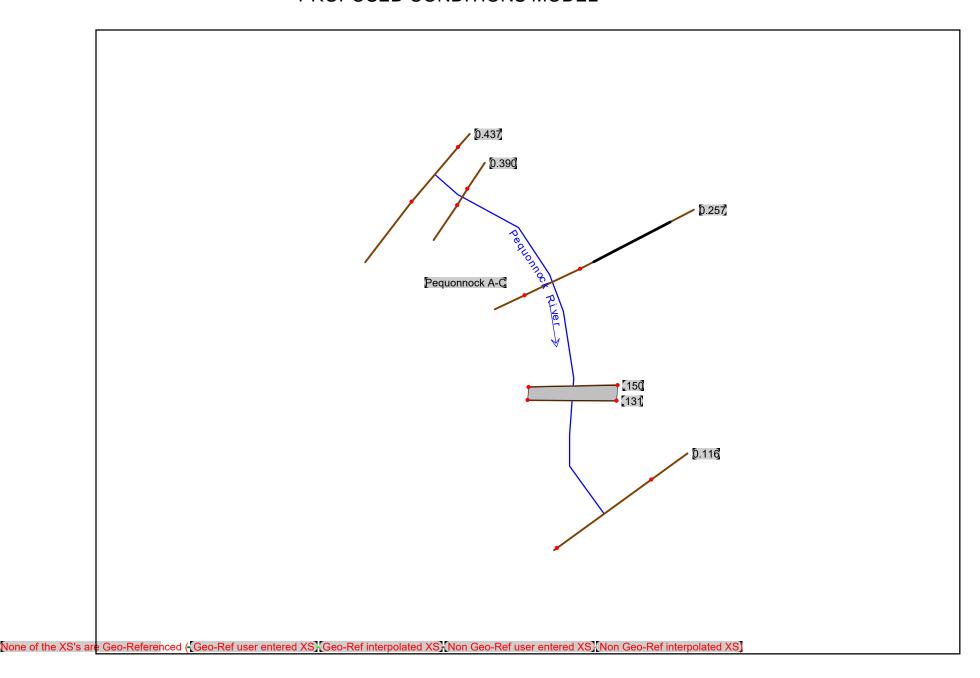


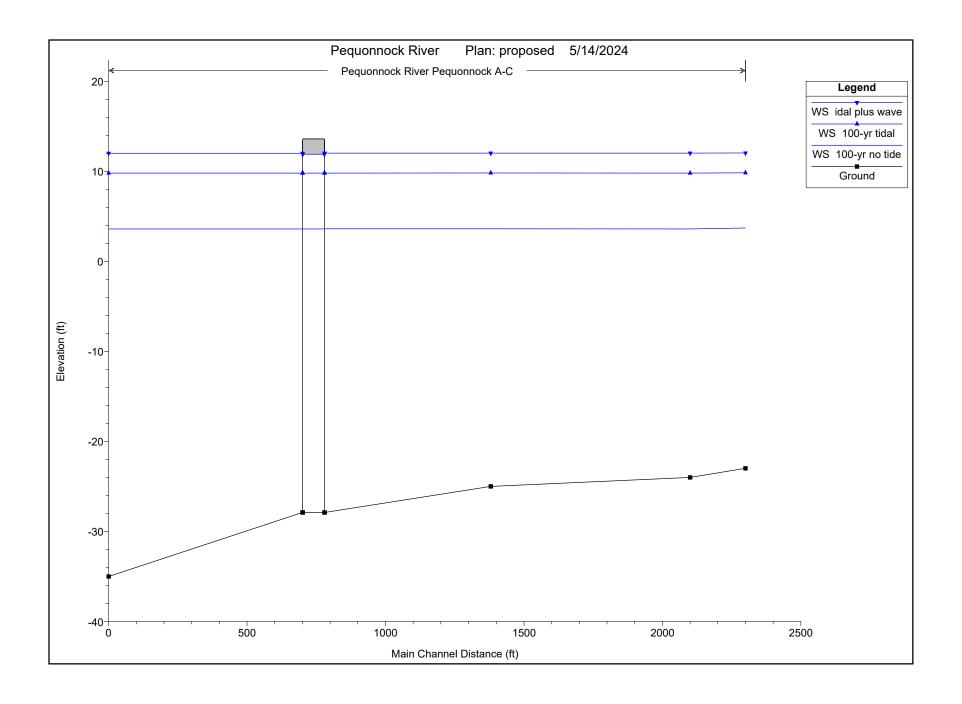






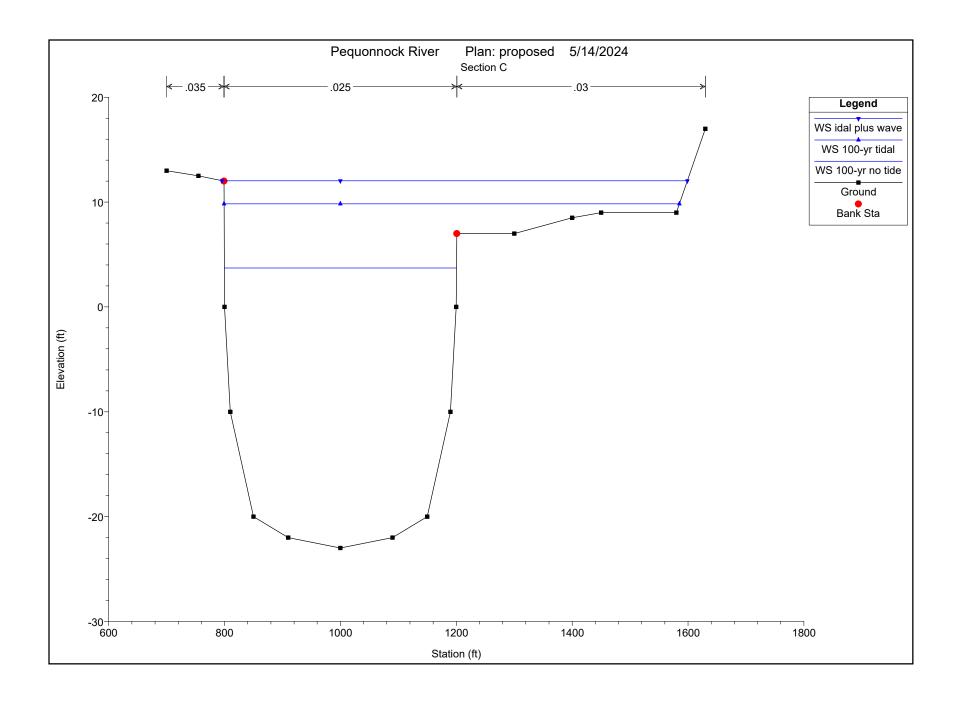
PROPOSED CONDITIONS MODEL

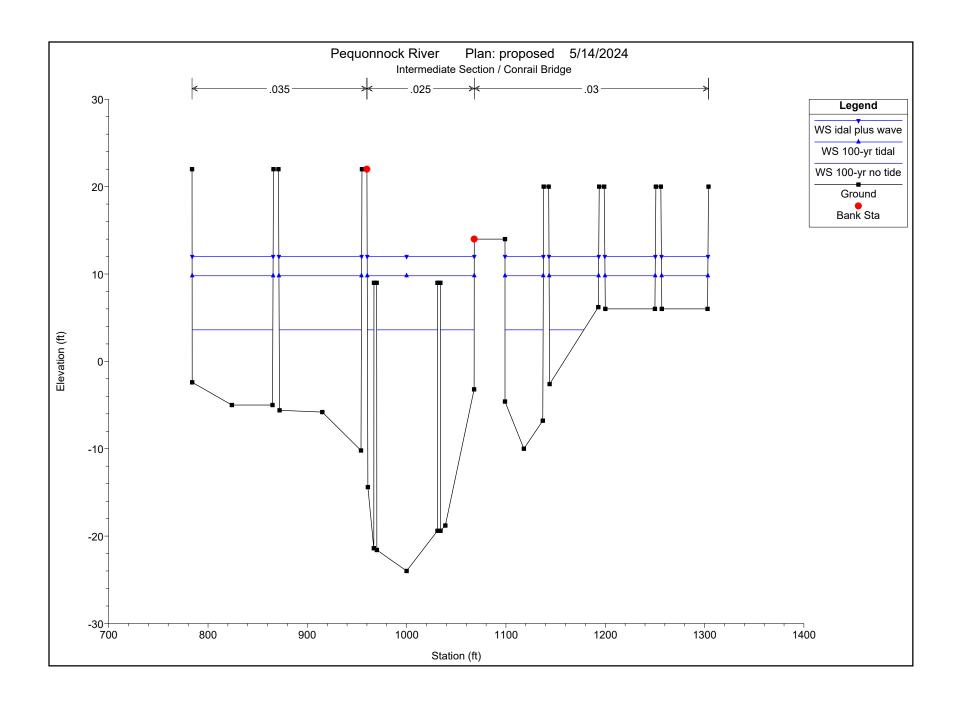


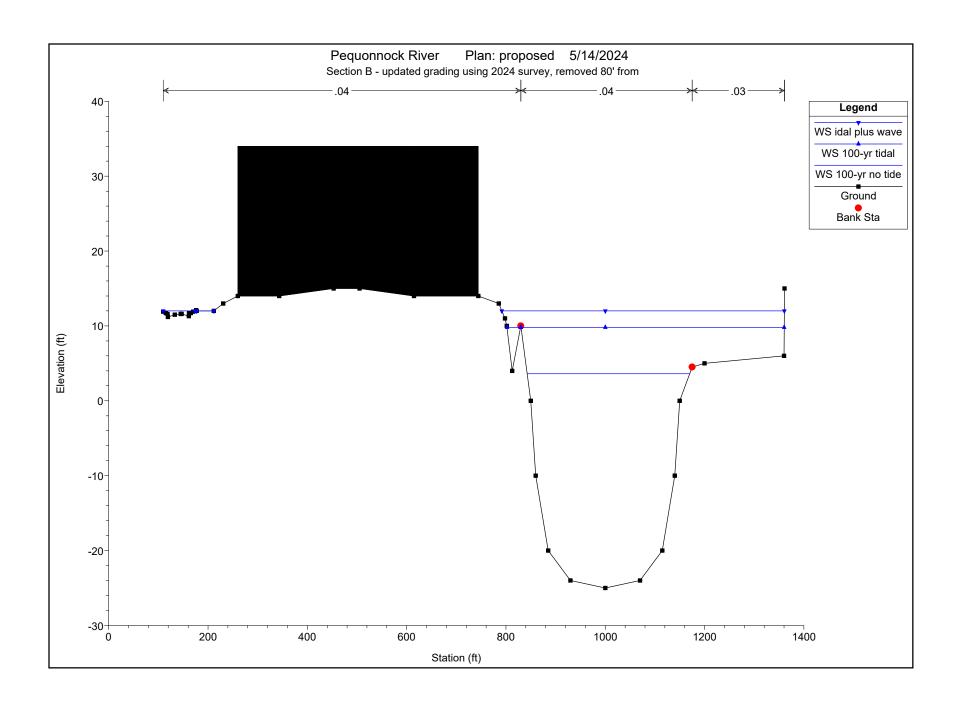


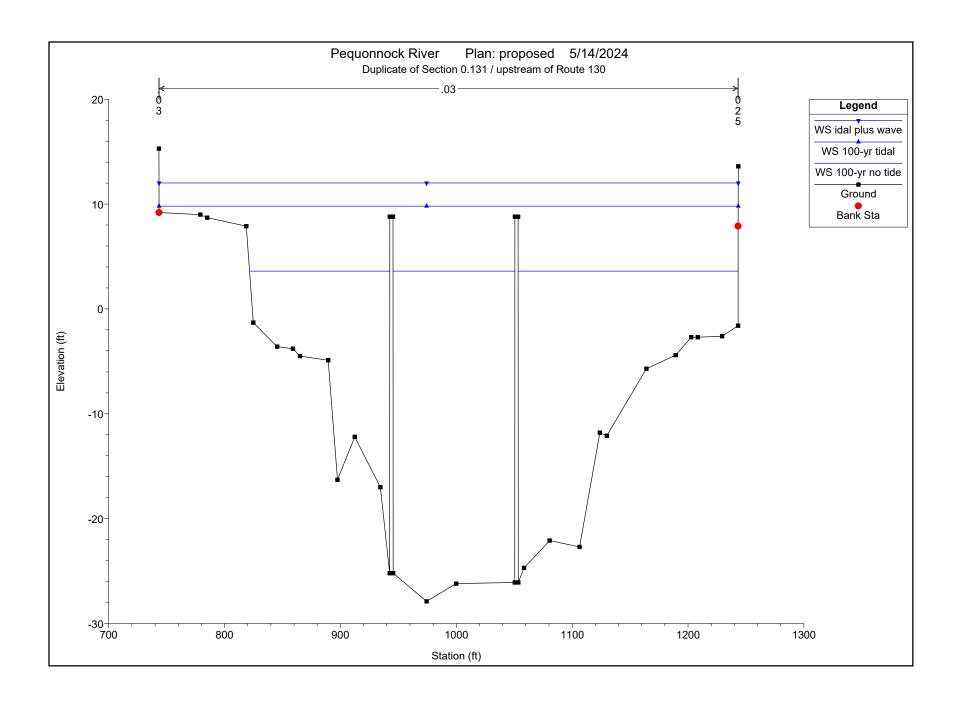
HEC-RAS Plan: PR River: Pequonnock River Reach: Pequonnock A-C

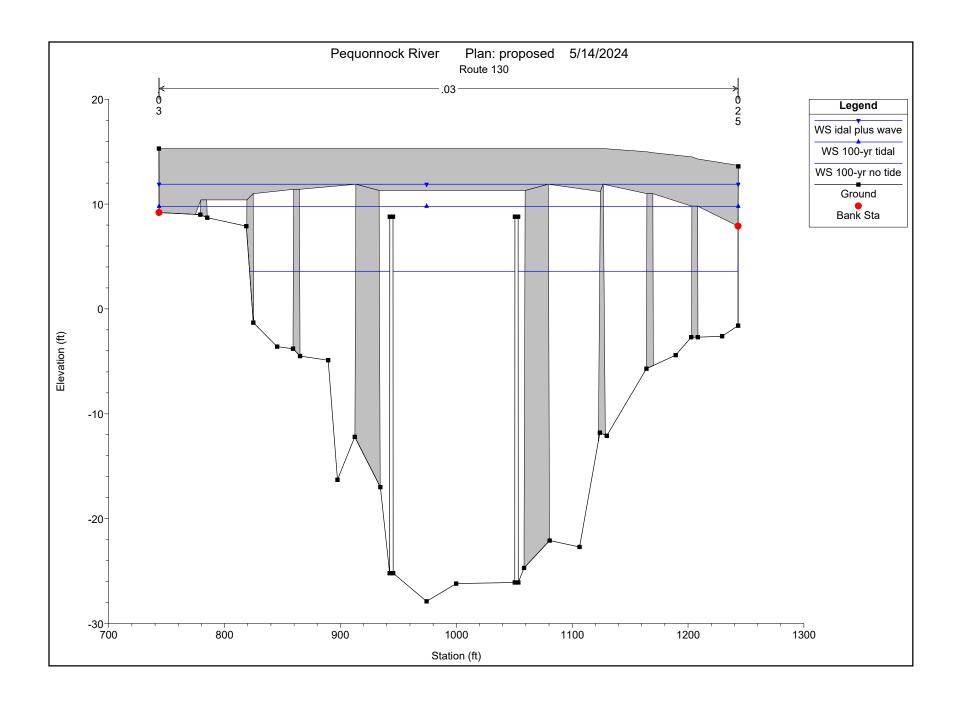
| Reach | River Sta | Profile | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chnl | Flow Area | Top Width | Froude # Chl |
|----------------|-----------|----------------|---------|-----------|-----------|-----------|-----------|------------|----------|-----------|-----------|--------------|
| | | | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft/ft) | (ft/s) | (sq ft) | (ft) | |
| Pequonnock A-C | 0.437 | 100-yr no tide | 9560.00 | -23.00 | 3.71 | | 3.72 | 0.000005 | 1.02 | 9354.86 | 400.84 | 0.04 |
| Pequonnock A-C | 0.437 | 100-yr tidal | 9560.00 | -23.00 | 9.84 | | 9.85 | 0.000002 | 0.80 | 12473.43 | 786.08 | 0.03 |
| Pequonnock A-C | 0.437 | idal plus wave | 9560.00 | -23.00 | 12.04 | | 12.05 | 0.000002 | 0.73 | 14217.64 | 803.57 | 0.02 |
| Pequonnock A-C | 0.390 | 100-yr no tide | 9560.00 | -24.00 | 3.60 | | 3.69 | 0.000101 | 2.74 | 4295.32 | 338.91 | 0.10 |
| Pequonnock A-C | 0.390 | 100-yr tidal | 9560.00 | -24.00 | 9.81 | | 9.84 | 0.000035 | 1.70 | 6846.44 | 457.91 | 0.06 |
| Pequonnock A-C | 0.390 | idal plus wave | 9560.00 | -24.00 | 12.02 | | 12.04 | 0.000024 | 1.48 | 7859.30 | 459.21 | 0.05 |
| Pequonnock A-C | 0.257 | 100-yr no tide | 9560.00 | -25.00 | 3.62 | | 3.64 | 0.000020 | 1.29 | 7395.12 | 327.34 | 0.05 |
| Pequonnock A-C | 0.257 | 100-yr tidal | 9560.00 | -25.00 | 9.81 | | 9.82 | 0.000009 | 0.97 | 10384.01 | 557.34 | 0.03 |
| Pequonnock A-C | 0.257 | idal plus wave | 9560.00 | -25.00 | 12.02 | | 12.03 | 0.000006 | 0.88 | 11656.40 | 667.75 | 0.03 |
| Pequonnock A-C | .150 | 100-yr no tide | 9560.00 | -27.90 | 3.61 | -20.52 | 3.63 | 0.000021 | 1.28 | 7485.69 | 415.95 | 0.05 |
| Pequonnock A-C | .150 | 100-yr tidal | 9560.00 | -27.90 | 9.80 | -20.52 | 9.82 | 0.000010 | 0.94 | 10162.39 | 499.84 | 0.04 |
| Pequonnock A-C | .150 | idal plus wave | 9560.00 | -27.90 | 12.01 | -20.52 | 12.02 | 0.000007 | 0.85 | 11266.89 | 499.92 | 0.03 |
| Pequonnock A-C | .140 | | Bridge | | | | | | | | | |
| Pequonnock A-C | .131 | 100-yr no tide | 9560.00 | -27.90 | 3.59 | | 3.62 | 0.000021 | 1.28 | 7480.28 | 415.94 | 0.05 |
| Pequonnock A-C | .131 | 100-yr tidal | 9560.00 | -27.90 | 9.80 | | 9.81 | 0.000010 | 0.94 | 10158.84 | 499.84 | 0.04 |
| Pequonnock A-C | .131 | idal plus wave | 9560.00 | -27.90 | 12.00 | | 12.01 | 0.000007 | 0.85 | 11258.89 | 499.92 | 0.03 |
| Pequonnock A-C | 0.116 | 100-yr no tide | 9560.00 | -35.00 | 3.60 | -29.80 | 3.60 | 0.000001 | 0.52 | 18504.34 | 651.65 | 0.02 |
| Pequonnock A-C | 0.116 | 100-yr tidal | 9560.00 | -35.00 | 9.80 | -29.80 | 9.80 | 0.000001 | 0.42 | 22597.95 | 698.57 | 0.01 |
| Pequonnock A-C | 0.116 | idal plus wave | 9560.00 | -35.00 | 12.00 | -29.80 | 12.00 | 0.000001 | 0.40 | 24512.47 | 891.00 | 0.01 |

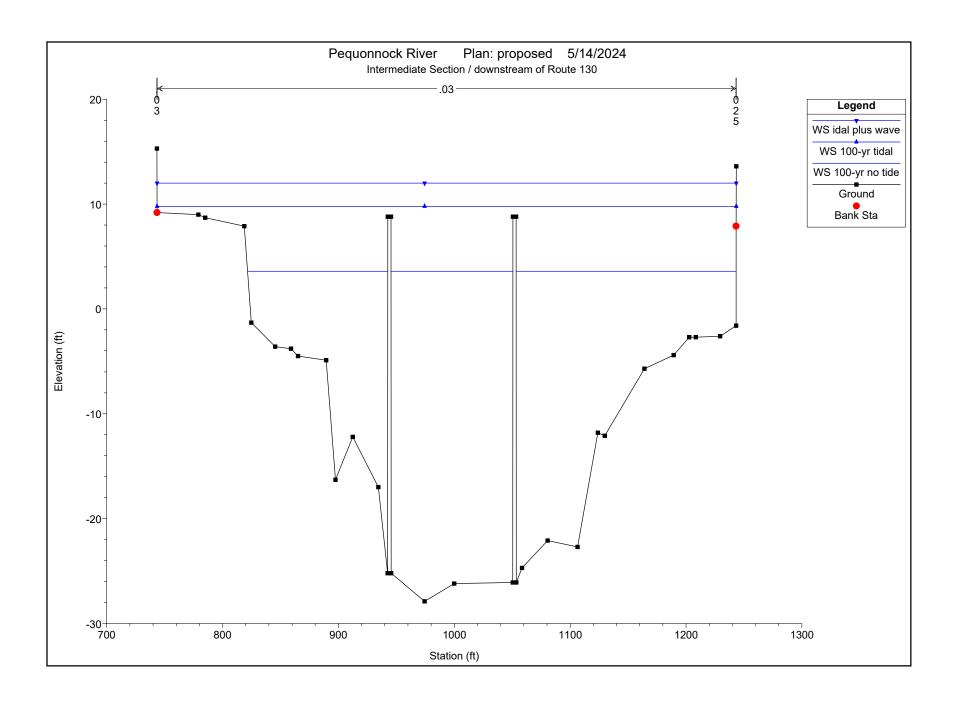


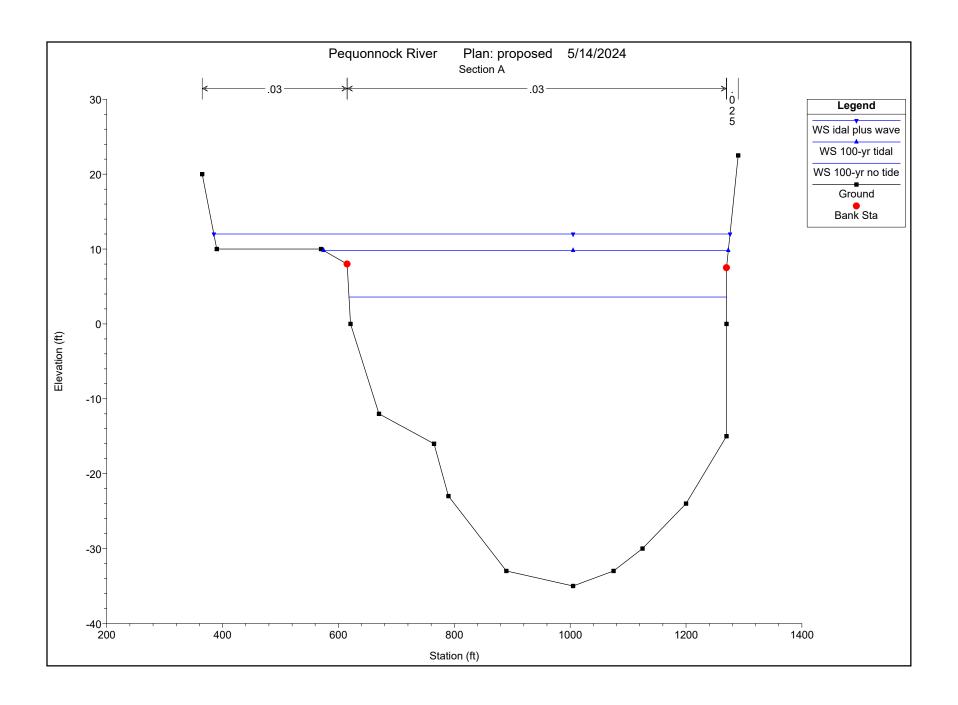












************************* HECZ RELEASE DATED NOV 76 UPDATED AUG1977 -ERROR-CORR--01,02MODIFICATION - 50,51,52,53 CONNECTICUT FLOOD INSURANCE STUDY HUD CONTRACT #H-4560 T1 CITY OF BRIDGEPORT CEM #3027.921 SEPTEMBER 20,1978 12 **T**3 PEQUONNOCK RIVER STA.0.057 TO STA. 3.500 100 YEAR NATURAL J1 ICHECK INO NINV IDIR STRT METRIC HVINS Q WSEL FQ -()6. ∞ () • -0. -0.000000 ~0.00 -0.0 -0. 3.600 -0.000 J2 NPROF TPLOT PREVS XSECV XSECH FN ALLDC IBW CHNIM ITRACE 1.000 -0.000 -1.000 -0.000-0.000 -0.000-0.000 -0.000 ~(°.000 -0.000 J3 VARIABLE CODES FOR SUMMARY PRINTOUT 38.000 1.000 43,000 26.000 3.000 50.000 61.000 53.000 27.000 21.000 22.000 -28 :000 54.000 0.000 200.000 -0.000 -0.000 -0.000 LEFT • 030 -NC-RIGHT 0 0 2 5 · CHANNEL: • () 3 () ·300 **~600** -0.000 -0.000 -0.000 ~0.000 **-0.**€000 QT 9,000 2630.000 6700.000 9560,000 21240.000 9560,000 9560.000 9560,000 9560.000 9560.000 FT -0.000-0.000 ~0.000 -0.000 -0.000-0.000 10.400 9.100 615,000 1270,000ID.... sections X1 17.000 .057 615.000 1270,000 0.000 0.000 0.000 -0.000 -0.000 -0.000 -GR 20,000 365.000 -10.000 390,000 10,000 570.000 8.000 615.000 0.000 621.000 -12,000 670.000 -16.000765,000 -23.000 790.000 -33,000 890.000 -35,000 1005.000 GR / -33,000 1075.000 -30.000 1125.000 -24.000 1200.000 ~15.000 1269,800 0.000 1269,900 GR 7,500 1270.000 22,500 1290,000 -0.000 -0.000 ~0.000 -0.000 -0.000 -0.000 ΕŢ -0.000 -0.000 -0.000 -0.000 -0.00010.600 -0.000 -0.000 -0.000NCORACHMENTS RIGHT LEFT BANK STATION RIGHT BANK STATION 52,000 •116 743.500 1243.300 250,000 400.000 310.000 -(4000 -0 db () () ~~ () . () (i) -X3-10.000 -0.000 ~() a () () -0.000 -0.000 ~0**.**000 -0.000 11.900 11.900 -0.000 GR 15,300 743,400 9.200 743.500 9,000 779.100 10.400 779,600 10.400 784.600 GR 8,700 785,100 7.900 818,800 10,400 819.300 11.000 824.700 -1.300824,900 СĐ -3,600 845.400 -3.800 859.100 11.400 859.600 11.400 864.600 -4.500 865.100 GR -4-900 889,400 -16.300 897.400 -12.200 912,400 11.900 913.400 11.300 933,400 GR -17,000 934,500 -25.200 942.500 8.800 942.600 8.800 945,400 -25.200 945.500 GR -27.900974.400 -26.200 1000.000 ~26.100 1050.500 8.800 1050.600 1053.400 8.800 GR -26.1001053,500 -24.7001058,500 11.300 1059,600 11.900 1079.500 -22.100 1080.600 GR -22.700 1106.400 -11.800 1123.900 11,200 1124.400 11,900 1126,900 -12.100 1129.900 GR -5.700 1164.100 11.000 1164.600 11.000 1169.600 -4.400 1189,400 -2.700 1202.800 GR 11.000 1203,300 11.000 1208,300 -2.700 1208,400 -2.600 1229.400 -1.600 1243.200 GR 7.900 1243,300 13,600 1243,400 -0.000 -0.000 -0.000 -0.000 ~0 e 0 0 0 -0.000 - S R **~0.000** 1.560 2,600 ~()_e()()() 100.000 NET AREA OF BRIDGE OPENING <u>⊳8900, nan</u> 020 ه ځ -27,900 -27,900 EFF AREA USED UNTIL BANKS US AND DS CH NVERT AT BRIDGE DOWNSTREAM DISTANCE EXCEEDED IGNORE FOR SB X 1 .131 0.000070.000 70.000 70.000 -O (INEFF STA -0.000 =0.00001.000 -X-2 -0.000-- () e V1.1~900 13,600 -0.000 -0 ^^^ -() (-0.000 -0.000 Х3 10.000 -0.000 -0.000 -0.000 -- () a () () () -6.000 -- () **▶**15.300 1.3.600 -0.000 BT -20,000 743,400 15.300 0.000 743.500 15.300 9.200 779:600 15.300 10.400 P T 784.600 15.300 10.400 819,300 15.300 10,400 824.700 15,300 11.000 359.600 ВT 15,300 11:400 864.600 15,300 11.400 913.400 15.300 11.900 933,400 15,300

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1124.400

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1059,600

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1079.500

| | BT | 1126.900 | 15.300 | 11.900 | 1164.600 | 15.000 | 11.000 | 1169.600 | 14.900 | 11.000 | 1203.300 | | 7 |
|----|---|------------------|--|---------------------------------|------------------------|-------------------|--|------------------|---------------------------------------|-------------------|--------------------|---|-------|
| | B.T. | 14.500 | 9.800 | 1208-300 | 14.300 | 9 6800 | 1243.300 | 13.700 | 7.900 | 1243.400 | 13.600 | ······································ | { |
| | BΥ | -() () () () | ~O.000 | -0.000 | . ~ <mark>0.000</mark> | -0.000 | -0.000 | -(),()() | -0.000 | -0.000 | -0.000 | | |
| | NC | 1 LEFT 1 0 0 1 5 | RIGHT • 020 | CHANNEL 025 | •100 | •300 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | | i |
| | ET | -0.000 | MANNING'S N VALUE | -0.000 | ~ <mark>0.000</mark> | ~0.000 | -0.000 | 10.600 | 9.100 | 830.000 | 1175.000 | | ţ |
| | \$10.00mm | ENCORACHMENTS | | | | LEFT | · · · DOWNSTREAM DISTANCE · · RIGHT | CHANNEL | · · · · · · · · · · · · · · · · · · · | | | ns-santa (1111) (1111) (1111) (111) (111) (111) (111) (111) (111) (111) (111) (111) (111) (111) (111) (111) (111) | |
| Ť. | x1 | 257 | 19.000 | 1 LEFT BANK STATION 8 3 0 0 0 0 | RIGHT BANK STATION | 760.000 | 600.000 | 680.000 | -0.000 | -0.000 | 0.000 | | (|
| | GR | 14.000 | 130,000 | 10.500 | 320.000 | 10,000 | 630.000 | 9.500 | 700.000 | 10.500 | 815.000 | | |
| | GR [| | 830.000 | 0.000 | 850.000 | -10.000 | 860.000 | -20.000 | 885.000 | -24.000 | 930.000 | | |
| | GR | -25.000 | 1000.000 | -24.000 | 1070.000 | -20.000 | 1115.000 | -10.000 | 1140.000 | 0.000 | 1150.000 | | 1 |
| | GR | 4.500 | 1175.000 | 5.000 | 1200.000 | 6.000 | 1360.000 | 15.000 | 1361.000 | -0.000 | -0.000 | | |
| | NC | LEFT • 040 | RIGHT 🔞 () 👍 () | CHANNEL • 030 | • 300 | • 600 | -0.000 | -0.000 | -0.000 | ~0.000 | ~0.000 | | , |
| | | | MANNING'S N VALUE | • | | | DOWNSTREAM DISTANCE | | | | | | (|
| | | | | LEFT BANK STATION | RIGHT BANK STATION | LEFT | RIGHT · | CHANNEL | | | | | |
| | X1 | •390 | 41,000 | 960.000 | 1068.100 | 920.000 | 520,000 | 720.000 | -0.000 | ~0.000 | -0.000 | | 1 |
| | GR | 22.000 | 784.000 | -2.400 | 784.100 | -5.000 | 824.000 | -5.000 | 865.000 | 22.000 | 866.000 | | • |
| | GR | 22.000 | 871.000 | -5.600 | 872.000 | -5.800 | 912.000 | -10.200 | 954.000 | 22.000 | 955.000 | | |
| | GR | 22.000 | 960.000 | -14.400 | 961.000 | -21.400 | 967.000 | 9.000 | 967.100 | 9.000 | 969.900 | | { |
| | GR | -21.600 | 970,000 | -24.000 | 1000.000 | -19,400 | 1031.000 | 9.000 | 1031.100 | 9.000 | 1034.000 | | |
| | GR | -19.400 | 1034,100 | -18.800 | 1039.000 | ~3 . 200 | 1068,000 | 14.000 | 1068.100 | 14.000 | 1099.000 | | |
| | GR | -4.600 | 1099,100 | -10.000 | 1118.000 | ≈6.800 | 1137,000 | 20,000 | 1138.000 | 20.000 | 1143.000 | | (|
| - | GR GR | -2.600 6.000 | 1144.000 | 6.200 | 1193.000 | 20.000 | 1194.000 | 20.000 | 1199.000 | 6.000 | 1200.000 | | |
| - | GR | 20.000 | 1250,000 1304,000 | 20.000 | 1251.000 | 20.000 | 1256.000 | 6,000 | 1257.000 | 6.000 | 1303.000 | · · | |
| - | NC. | | RIGHT . 030 | -0.000 CHANNEL 0025 | -0.000 .100 | -0.000 | -0.000 | -0.000 -0.000 | -0.000 | -0.000 -0.000 | -0.000 | | (. |
| | ET. | =0.000 | MANNING'S N VALUE | () e () () () | -0.000 | .300 -0.000 | ~0.000 | -0.000 | -0.000 9.100 | -0.000 800.000 | ≈0.000 1205.000 | | |
| | | -08000 | MANNING'S N VALUE | -0.000 | -0.000 | ~0.000 | DOWNSTREAM DISTANCE | -0.000 | 9.100 | 000.000 | 1205.000 | | |
| | | ENCORACHMENTS | | LEFT BANK STATION | RIGHT BANK STATION | LEFT | RIGHT | CHANNEL | | | | , | (|
| | -X1 | .437 | 18.000 | 799,000 | 1201.000 | 200:000 | 200.000 | 200.000 | -0.000 | -0.000 | -U.OUU | nan O'ramanan man man man dan man dan man dan man dan man dan man man man man man man man man dan man dan man | |
| | GR | 13.000 | 700.000 | 12.500 | 755.000 | 12,000 | 799.000 | 0.000 | 800.000 | -10.000 | 810.000 | | , |
| | GR | -20.000- | 850.000 | -22.000 | 910.000 | -23,000 | 1000.000 | ~22,000 | 1090.000 | ~20.000 | 1150.000 | . <mark> </mark> | (|
| | GR 📞 | <u>~ ~10.000</u> | 1190,000 | 0.000 | 1200.000 | 7.000 | 1201.000 | 7.000 | 1300.000 | 8.500 | 1400.000 | | |
| | ~-GR | 6.000 | 1450.000 | 9,000 | 1580,000 | 17.000 | 1630.000 | -0.000 | -0.000 | -0.000 | -0.000 | | í |
| | NC | -0.000 | ~0.000 | -0.000 | .400 | . 700 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | | (|
| | \$1000011000110001100000000000000000000 | | | | | | | | | | | · · · · · · · · · · · · · · · · · · · | |
| | X-1 | ····· | 36,000 | 794.000 | 1202.200 | 150.000 | 320.000 | 240.000 | -0.000 | -0.000 | ~Û•Û00 | | (|
| | ХЗ | 10.000 | -0.000 | -0.000 | -0.000 | ~0.000 | -0.000 | ~0.000 | 12.200 | 12.800 | ~0°000 | | |
| | GP | 19.000 | 786.000 | 8.500 | 787.000 | 8,500 | 794.000 | 5.500 | 796.000 | -1.800 | 796.100 | | |
| | GR | -8.200 | 821.100 | -9.200 | 856.100 | 3.000 | 856.200 | 3,500 | 866.100 | -10.400 | 856.200 | | (|
| | GR | -11.200 | 888-100 | -9.600 | 930.000 | 4.200 | 930.100 | 9,400 | 960.100 | -12.800 | 960.200 | | |
| | GR | -20.800 | 963.100 | 9.600 | 963.200 | 9.600 | 967.000 | -20.800 | 967.100 | -18.800 | 1010.000 | | |
| | GR | -12.800 | 1038.000 | 9.400 | 1038.100 | 9.400 | 1042.000 | 3.800 | 1068.000 | -12.200 | 1068.100 | | (|
| | GR | -9.200 | 1102.000 | -7.000 | 1133.100 | 3.000 | 1133.200 | 3.200 | 1143.100 | -4.800 | 1143.200 | | |
| | GP | -2.400 | 1202.100 | 6.400 | 1202.200 | 14.400 | 1266.000 | 14.000 | 1330.000 | 9,000 | 1550.000 | | , |
| | GR | 25.000 | 1560.000 | -0.000 | -0.000 | ~ () • () () () | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | | (|
| | SB | -0.000 | 1.560 | 5.600 | -0.000 | 136.000 | -0.000 | 7030-000 | 3.800 | -20.800 | -20.800 | | |
| | | | | | | | | | | | | | (. |
| | V 1 | 4.00 | _ Pr - 12 Pr 19 | _ /\$ /\$ & /\$ & /\$ | . Α δόδ | 00 000 | 0.0 000 | 00.000 | - A BAA | . M. Assa | A BAA | | |
| | X <u>1</u> X 2 | .498 -0.090 | ⊢() ₀ ()()() ······•() ₀ () ₀ ()······ | -0.000 1.000 | =(),()()() | 80,000 | 000.00 | 80,000 | -0.000 | ~0.000 | -0.000 | | |
| | X3 | 10.000 | ~0.000 | -0.000 | 15,000 | 9.000 | -0.000 | -0.000 | 10.000 | -0.000 | -0.000 | | (|
| | BT | 34-000 | 786.000 | 19.000 | -0.000 0.000 | -0.000 787.000 | -0.000 19.100 | -0.000 8.500 | 18.900 794.000 | 9.000 19.200 | -0.000 8.500 | | |
| | BT | 806.000 | 19.500 | 10.000 | 821,000 | 20.000 | 12.200 | 837.000 | 20.200 | 10.400 | 856.000 | | |
| | ВТ | 19.800 | 3.000 | 866.100 | 21.000 | 3.500 | 876.000 | 21.100 | 9.500 | 688.000 | 21.500 | | { |
| | ВŤ | 13.400 | 904,000 | 21.700 | 13.700 | 930,000 | 22.100 | 4.200 | 960.000 | -22.800 | 0.000 | | |
| 1 | BT - | 960.100 | 18.900 | 9.400 | 980.000 | 19,100 | 12.800 | 1000.000 | 19.500 | 15.000 | 1020.000 | | ,.1., |
| 1. | ВТ | 19.200 | 13.500 | 1042.000 | 18.800 | 9.400 | 1043.000 | 22.800 | 0.000 | 1068.000 | 22.200 | | |
| I | 81 | 3.800 | 1089.000 | 22.000 | 13.200 | 1102.000 | 21.800 | 14,400 | 1121.000 | 21.300 | 10.700 | 4 | 1 |
| | BT | 1133.000 | 21.000 | 3.000 | 1143.100 | 20.700 | 3.200 | 1157.000 | 20.300 | 10.200 | 1174.000 | | |
| | В.Т. | 19,900 | 12.800 | 1187.000 | 19,400 | 11,800 | 1202.200 | 19.300 | 6.400 | 1265.900 | 19.000 | | (|
| | BT | 0.000 | 1266.000 | 14.400 | 0.000 | 1336.000 | 14.000 | 0.000 | 1550.000 | 9,000 | 0.000 | | |
| | | 1560.000 | 25,000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | ~0.000 | organisas (1 a. | |
| | NC | .035 | .045 | .025 | .300 | • 500 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | • | • |
| | | | | | | | | | | | | | - 1 |

| ET -0.000 | -0.000 | -0.000 | -() • () () () | -0.000 | -0.000 | | 9.100 | 880,000 | 11.20.000 | (| ĺ |
|---------------------------------|--------------------|----------------|----------------------------|------------------|------------------|----------------------------|-----------------|--|------------------------|--|---|
| | | | | | | | | | | | |
| -X1 | 19,000 | 384,000 | 1120.000 | 440.000 | 380.000 | 410.000 | -0.000 | -0.000 | ~0.000 | | Ĺ |
| GR 12.800 | 600.000 | 12.500 | 640.000 | 11.000 | 760.000 | 9.000 | 830.000 | 8.500 | 884.000 | | |
| GR 0.000 | 885.000 | -10.000 | 895.000 | -18.000 | 925.000 | -20.000 | 1000.000 | -18.000 | 1075.000 | 4 | |
| GR | 1100.000 | 0.000 | 1110.000 | 5.000 | 1120.000 | 8.500 | 1150.000 | 9.000 | 1220.000 | (| (|
| GR | 1280.000 | 10.500 | 1:350.000 | 11.000 | 1380.000 | 22.500 | 1400.000 | -0.000 | ~0.000 | | |
| NC -0.000 | -0.000 | .030 | .400 | .700 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | | / |
| X1 | 28.000 | 851.000 | | | | | D-00 | A - Z - Z - Z | | ! | |
| X3 10.000 | -0.000 | -0.000 | 1034.000 ······· | -0.000 -0.000 | 740,000 | 670.000 -0.000 | -0.000 9.100 | -0.000 9.100 | -0.000 -0.000 | • | |
| -GR 17.000 | 610.000 | 16.800 | -0.000 | 16.006 | 710.000 | 15.000 | 835.000 | 8.300 | 851,000 | | : |
| GR -2.800 | 851,100 | -13.400 | 874.000 | -17.400 | 897.000 | 8.900 | 897.100 | 9.000 | 904,900 | | |
| GR -15.600 | 905.000 | -13.800 | 929.000 | -15.300 | 952.000 | 9.100 | 952.100 | 9.100 | 959,900 | | |
| GR 6.600 | 963.000 | 6.600 | 966.000 | -18.300 | 966.100 | -19.200 | 983.000 | -18.700 | 1000.000 | (| |
| -GR17.400 | 1014.000 | -13.500 | 1031.000 | 7.500 | 1031,100 | 8 400 | 1034.000 | 14.800 | 1093.000 | | |
| GR 14.500 | 1200.000 | 15.500 | 1700.000 | 25.000 | 1715.000 | -0.000 | ~0.000 | -0.000 | -0.000 | , | , |
| -0.000 | 1.560 | 2.600 | -0.000 | 131.000 | -0.000 | 3900.000 | | -19,200 | -19.200 | | |
| , | | | | | | | | | | | |
| X1 .711 | -0.000 | -0.000 | -0.000 | 70.000 | 70.000 | 70.000 | -0.000 | -0.000 | ~U.000 | (| |
| $\hat{\mathbf{x}}_{2}$ -0.000 | -0.000 | 1.000 | 9.100 | 14.500 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | | |
| X3 10.000 | -0.000 | ~0.000 | -0.000 | -0.000 | -0.000 | -0.000 | 15.000 | 14.500 | -0.000 | | |
| 8.000 | 610.000 | 17.000 | 0.000 | 660.000 | 16.800 | 0.000 | 710.000 | 16.000 | 0.000 | (| |
| BT 835.000 | 15.000 | 0.000 | 1093.000 | 14.800 | 0.000 | 1200.000 | 14.500 | -0.000 | 1700.000 | | |
| -BT 15.500 | | -1715.000 | 25.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | | |
| NC .035 | .045 | .025 | .300 | .500 | -0.000 | ~0.000 | -0.000 | ~() ₀ () () () | ~0.000 | (| |
| ET -() () () () | -0.000 | -0.000 | -0.000 | 0.000 | ~0.000 | -0.000 | 9.100 | 870.000 | 1140.000 | | |
| | | | · | | | | | | | (| |
| X1 .834 | 17.000 | 870.000 | 1140,000 | 660.000 | 660.000 | 660.000 | -0.000 | -0.000 | -0.000 | *************************************** | |
| GR - 15.000 | 550.000 | 12.500 | 560.000 | 12.500 | 590.000 | 11.000 | 670.000 | 7.500 | 870.000 | | |
| GR / 1.000 | 880.000 | -10.000 | 910.000 | -18.000 | 930.000 | -19.000 | 1000.000 | -18.000 | 1070.000 | . (| |
| -GR -10.000 | 1090-000 | 1.000 | 1100.000 | 9,500 | 1140.000 | 10.500 | 1220.000 | 10,500 | 1270.000 | | İ |
| GR 11.500 | 1330.000 | 13.500 | 1395.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | | |
| | | • | | | | | | | | and the second s | 1 |
| -X1 | 55.000 | 817.000 | 1179.600 | 600.000 | 660.000 | 630.000 | -0.000 | -0.000 | -0.000 | | 1 |
| X3 10.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | 13.000 | 13.000 | ~0.000 | (| |
| GR 19.000 | 600.000 | 17.000 | 650.000 | 16.500 | 710.000 | 17.800 | 748.000 | 13.000 | 817.000 | ······································ | |
| GR 7.400 | 818.000 | 7.700 | 860.500 | 1.800 | 861.000 | -3.400 | 880.000 | 16.000 | 880.100 | | |
| GR -10,200 | 888.100 | -14.500 | 918.000 | -13.900 | 937.900 | 8.000 | 938.000 | 8.000 | 941.000 | | |
| GR ~13.800 | 941.100 | -13.600 | 947,900 | 7.400 | 948.000 | 12.500 | 950.500 | 16.000 | 950.600 | | |
| GR14.000 | 954.000 | 7.400 | 957.400 | -15.200 | 957.500 | -18.100 | 962.400 | 8.400 | 962.500 | | ļ |
| GR 8.400 | 965.000 | -18.200 | 965.100 | -18.600 | 1000.000 | -16.600 | 1022.000 | -16.300 | 1033.400 | (| |
| -GR8-000 | 1033.500 | 8.000 | 1036-006 | -16.300 | 1036.100 | -13.100 | 1042.500 | 7.400 | 1042,600 | | |
| GR 13.100 | 1045,500 | 15,600 | 1052.300 | -10,400 | 1052.500 | ~9 * 800 | 1059.900 | 6.400 | 1060.000 | (| J |
| GR 6.400 | 1062.500 | -9.600 | 1062.600 | -8.600 | 1082,500 | -3,900 | 1111.500 | 16.000 | 1111.600 | | . |
| GR 16.000 | 1119.400 | -1.200 | 1119.500 | 1.900 | 1135.500 | 6.500 | 1147.500 | 6.500 | 1148.500 | | İ |
| GR 4.800 | 1152.500 | 5.300 | 1179.500 | 15.200 | 1179.600 | 22.700 | 1179.700 | 22.700 | 1208.000 | | |
| \$8 -0.000 | 1.560 | 2.600 | ~O.OOO | 107.000 | -0.000 | 6290.000 | 3.510 | 18.000 | -18.000 | | |
| | | | | | | | | | | ı. | |
| ~X1 · · · · · • 962 · | -0.000 | ~O • O O O | = () ₀ () () () | 60.000 | 60.000 | 60.000 | -0.000 | ~0.000 | | | |
| X2 -0.000 | -0.000 | 1.000 | 17,000 | 16.500 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | | . |
| X310.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | 16.500 | 22.700 | ~0.000 | | |
| BT 16.000 | 600.000 | 19.000 | 0.000 | 650.000 | 17.000 | 0.000 | 710.000 | 16.500 | 0.000 | , | |
| BT 748,000 | 17,800 | 0.00.0 | 817.000 | 20.100 | 13.000 | 880.000 | 21.200 | 16.000 | 830.100 | | |
| 8T 21.400 | 16.000 | 950.600 | 22.100 | 16.000 | 954.000 | 22.300 | 14.000 | 1000.000 | 23.000 | | |
| BT 1119.400 | 1045.500 22.800 | 23,000 | 1:2:300 | 1052,300 | 22,900 | 15.600 | 1111.600 | 22800 | 16.000 | | |
| NC .055 | .030 | 16.000 .025 | 1179.500 .300 | 22.760 .500 | 15.200 -0.000 | 1208.000 -0.000 | 22.700 | -(),()()() -(),()()()()()()()()()()()()()()()()()() | ~0.000 ~0.000 | | |
| ET -0.000 | -0.000 | -0.000 | -0.000 | ~0.000 | -0.000 -0.000 | -0.000 | 9.100 | 875.000 | 1130.000 | į į | |
| | ₩ ₩ ₩ ₩ | OFIGUR | 4 9 41 3 40 | V C V VV | C A F A A | \$ 9 \$ \$ \$ \$ \$ | 7 0 V V V | 0130000 | Sec. 14 64 64 64 64 64 | | |

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|--------------------|--|--------------------|---------------|--------------------|------------------|--------------------|--------------------|--|-----------------|--------------------|--|---|
| | /1 1 00/ | 10.000 | 076 000 | 1100 000 | 700 000 | 110 000 | | 0.000 | 0.000 | 0.000 | | * * * |
| | (1 1.096 | 19.000 | 875.000 | | 680.000 | 640.000 | 660,000 | -0.000 | ~0.000 3.500 | -0.000 | | |
| | SR 15.000 | 680.000 | 10.000 | | 9,000 | 720.000 | 8,500 | 775.000 | 7.500 | 835,000 | | (|
| | SR = 5.000 | 875.000 | 1.000 | | -5.000 | 890.000 | -12.000 | 925.000 | -13.300 | 1000.000 | | |
| _ | SR / -12.000 | 1075.000 | -5.000 | | 1.000 | 1120.000 | 5.000 | 1130.000 | 9.500 | 1155.000 | | |
| | SR 10.000 | 1170.000 | 10.500 | 1225.000 | 12,000 | 1275.000 | 12.800 | 1330,000 | ~0.000 | -0.000 | | (|
| | \C .075 | | .025 | .100 | .300 | -0.000 | -0.000 | ~0.000 | ~0.000 | -0.000 | | |
| t: | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | 9.100 | 865.000 | 1160.000 | | |
| | | | | | | | | | | | | (|
| v | 1 1 250 | 10 000 | | | | | . 1000 | ······································ | Α | (2 | | |
| | 1.250 | 10.000 | 867:000 | 1160.000 | 780.000 | 1000.000 | 1000.000 | -0.000 | -0.000 | -0.000 | | • |
| | SR (15.000 | 867.000 | 5.000 | 870.000 | 2.000 | 875.000 | -5.000 | 900.000 | -7.100 | 1000.000 | 3 | (|
| | R- ()5.000- | -1100.000 | 2.000 | 1120.000 | 5.000 | 1125.000 | 10.000 | 1135.000 | 15,000 | 1160.000 | | |
| IN | IC •050 | • 050 | .025 | .300 | .500 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | | |
| | | | | | | | | | | | | (|
| v | /1111 | 26000 | 917.500 | 1026.000 | 100 - 00 c | | | | | | | |
| X | | 26,000 | | | 380.000 | 400,000 | 390.000 | -0.000 15.000 | -0.000 | -0.000 | | j |
| | 10.000 | -0.000 | -0.000 | -0.000 | 00000 | ≈0.000 | -0.000 A - 6444 | 15.000 | 15.000 | -0.000 | | . (|
| | iR 20.000 | 870.000 925.500 | 19.500 200 | 880.000 934.000 | 16.100 -2.900 | 914.500 943.500 | 6,500 ··· | 917.500 953.000 | -4.500 | 917.600 969.500 | | |
| | $\begin{array}{ccc} R & 2 & 300 \\ \hline R & 6 & 500 \end{array}$ | 969.600 | 6.500 | 974.000 | -3.700 | 974.100 | -3.300 ··· | 993.000 | ~3.600 | 1000.000 | | |
| | R = -1.300 | 1009.500 | 6.700 | 1026.000 | 9,000 | 1045.000 | 10.700 | 1055.000 | 11.300 | 1080.000 | | (|
| ⊸ G | | 1099.000 | 16.500 | 1026.000 | 15,500 | 1150.000 | 15.300 | 1270.000 | 17.000 | 1390.000 | | |
| | R 20.000 | 1500.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | ~0.000 | -0.000 | -0.000 | | 1 |
| | -0.000 | 1,560 | 2.600 | -0.000 | | -0.000 | 1030.000 | 3.310 | -3.700 | ~3.700 | | (|
| 3 | n =0.0000 | 3.6000 | C # OU O | -0 a 1/3/U | 44,000 | 20.000 | 10304000 | 20210 | ~5.100 | ~3.100 | | |
| | | | | | | | | | | | | |
| X | 1 1.329 | -0.000 | -0.000 | -0.000 | 50,000 | 50.000 | 50.000 | -0.000 | -0.000 | .~U.000 | | (|
| X | | -0.000 | 1.000 | 9.500 | 15.300 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | | |
| | 3 10.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 -0.000 | -0.000 | 1.6.100 | 15.300 | -0.000 | • | |
| - 8 | | 870.000 | 20.000 | 0.000 | 880,000 | 19.500 | 0.000 | 914.500 | 16.100 | 0.000 | | (|
| 8 | | 16.100 | 6.500 | 934.000 | 16.100 | 9.100 | 943.500 | 16.000 | 9.500 | 953.000 | | |
| B | | 9.100 | 969.600 | 16.000 | 6.500 | 974.000 | 16.000 | 6.500 | 990-600 | 15,900 | | |
| 8 | | 1000.000 | 15.900 | 9.100 | 1026.000 | 15.900 | 6.700 | 1030.000 | 15.900 | 7.200 | | (|
| B. | | 15.900 | 9.000 | 1055.000 | 15,900 | 10.700 | 1080.000 | 15.900 | 11.300 | 1090.000 | | |
| B | | 0.000 | 1105.000 | 16.500 | 0.000 | 1150.000 | 15.500 | 0.000 | 1270.000 | 15.300 | | |
| | T 0.000 | | 17.000 | 0.000 | 1500.000 | 20.000 | -0.000 | 0.000 | -0.000 | -0.000 | | (|
| N | | •040 | .035 | •600 | ,800 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | | |
| E | | -0.000 | 0.000 | -0.000 | -0.000 | -0.000 | -0.000 | 9.100 | 960.000 | 1055.000 | | |
| t. | 1 0000 | 0.000 | 0,000 | 0.000 | 0.000 | 0,000 | 0,000 | 76100 | 700 8000 | £033 6 000 | | (|
| ţ | | | | | | | | | | | | - 4 |
| Χ | 1 1.349 | 11.000 | 962.000 | 1055.000 | 130.000 | 130.000 | 130.000 | -0.000 | -0.000 | -0.000 | | |
| G | | 962.000 | 5.000 | 965,000 | 5.000 | 970.000 | -3.500 | 975.000 | -4.400 | 1000.000 | | . (|
| C. | | 1025.000 | 2.000 | 1030.000 | 5.000 | 1040.000 | 10,000 | 1045.000 | 15.500 | 1055.000 | | |
| G | | 1425.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | | |
| N | | -0.000 | ~0.000 | .100 | .300 | -0.000 | ~0.000 | -0.000 | -0.000 | -0.000 | | (|
| - NI | | .055 | 925.000 | .030 | 1070.000 | .075 | 1095.000 | .025 | 1700.000 | .040 | | -9 |
| NI | | -0.000 | -0.000 | -0.000 | ~~ O • O O O | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | | |
| E | | -0.000 | -0.000 | -() · () () () | -0.000 | -0.000 | -0.000 | 9.100 | 910.000 | 1075.000 | | (. |
| | • • • | . • | | | | | | , | 9. | . , | | |
| | | | | | | | | | | | | · , |
| X: | 1 1,490 | 19.000 | 910.000 | 1075.000 | 800.000 | 670.000 | 740.000 | -0.000 | -0.000 | -0.000 | | (|
| - X | | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | 11.500 | 11.500 | -0.000 | | 3 |
| GI | | 900.000 | 10.000 | 910.000 | 5.000 | 925.000 | 2.000 | 940.000 | -3.000 | 980.000 | | , [|
| -G | | 1000.000 | -3.000 | 1020.000 | 2.000 | 1060,000 | 5.000 | 1070.000 | 9.800 | 1075.000 | | [|
| GI | | 1140.000 | 10.500 | 1180,000 | 11.500 | 1300.000 | 12.000 | 1435.000 | 14.300 | 1550.000 | | |
| e e i | , | 1700.000 | 12.000 | 1920.000 | 15.000 | 2020.000 | 20.000 | 2170.000 | -0.000 | -0.000 | | - , L, L |
| N(| | .050 | .030 | .600 | .800 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | | 1,1" |
| - Q] | | 2375.000 | 6035.000 | 8615.000 | 19140.000 | -8615.000 | 8615.000 | 8615.000 | 8615.000 | -8615.000 | | -3 |
| E 1 | | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | 9.100 | 970.000 | 1750.000 | | , [|
| | | 77 72 | | | | | | | | | | , (|
| | | | | | | | | | | | | *************************************** |
| · · · X ·] | 1,583 | 17.000 | 985 6000 | 1015.000 | 480,000 | 540.000 | 510.000 | -0.000 | -0.000 | -0.000 | en en en en en en en en en en en en en e | - |
| GF | | 750.000 | 15.000 | 950.000 | 12,500 | 960.000 | 10.000 | 970.000 | 5.000 | 980.000 | | t l |
| | | | | | | | | | - | | | j |

| GR | - Table | 2.500 | 985.000 | -3.000 | 988.005 | -2.800 | 1000.000 | -3.000 | 1010.000 | 2.500 | 1015.000 | |
|---------------|-----------|-------------|---------------------------------------|-------------|------------------|-----------------|-----------------|-------------|---------------------------------------|----------------|-------------------|--|
| GR | | 5 - 600 | 1025.060 | 10.000 | 1030.000 | 12.000 | 1220.000 | 11.500 | 1700.000 | 11.500 | 2100.000 | (|
| GR | V | 15.000 | 2190.000 | 20.000 | 2340.000 | -0 ()()() | -0.000 | -0.000 | -6.000 | -0.000 | -0.000 | |
| NC | | -0000 | .060 | .025 | 300 | -500 | -0.000 | -0.000 | -0.000 | ~0. 000 | -0.000 | |
| ganna taka ya | ., | | ····· | | x | | | | | | 0.000 | |
| X1 | | 1.590 | 30.000 | 972.000 | 1018.100 | 40,000 | 70.000 | 60.000 | -0.000 | ~0.000 | -0.000 | , |
| Х3 | | 10.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | 8.800 | 10.000 | -0.000 | |
| GR | | 25.000 | 460.000 | 24.000 | 500,000 | 20.000 | 740.000 | 18.000 | 800.000 | 17.000 | 930.000 | |
| GR | | 16.300 | 952.000 | 16,600 | 969.000 | 10.000 | 972.000 | • 900 | 972,100 | -1.300 | 1000,000 | |
| GR | | -2.500 | 1010.000 | -2.900 | 1018,000 | 8.800 | 1018.100 | 15.300 | 1022.000 | 14.100 | 1042.000 | |
| GR | | 13-000 | 1120.000 | 13.500 | 1180.000 | 12,300 | 1250.000 | 10.500 | 1305.000 | 11.000 | 1370.000 | , |
| GR | | 10.800 | 1430.000 | 12.300 | 1730.000 | 12.800 | 1860.000 | 12.500 | 2100.000 | 12.500 | 2430.000 | |
| GB | | 11.300 | 2670.000 | 12.000 | 2770.000 | 15.000 | 2940.000 | 20.000 | 2950:000 | 25.000 | 2970.000 | |
| \$8 | | -0.000 | 1.560 | 3.000 | -0.000 | 41.000 | ~O.OOO | 470.000 | .231 | -1.300 | -1,300 | |
| | • | | | · · · · | | | | | | | | · · · · · · · · · · · · · · · · · · · |
| , X.1 | | 1.600 | -0.000 | -0.000 | -0.000 | 50.000 | 50.000 | 50.000 | · · · · · · · · · · · · · · · · · · · | -0.000 | -0.000 | |
| X2 | | -0.000 | -0.000 | 1.000 | 10.000 | 10.500 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | |
| - X3 | | 10.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | 16.300- | 10.500 | -0.000 | |
| BT | | 23,000 | 930.000 | 17.000 | 0.000 | 952.000 | 16.300 | 0.000 | 969.000 | 16,600 | 0.000 | |
| BT | | 69 • 1:00 - | 20.100 | 0.000 | 972.000 | 19.900 | 10.000 | 1018.100 | 19,000 | 8-800 | 1021.900 | |
| вт | 1 | 18.800 | 0.000 | 1022.000 | 15.300 | 0.000 | 1042.000 | 14.100 | 0.000 | 1120.000 | 13.000 | (|
| 9 B-T- | | -0.000 - | 1180.000 | 13.500 | 0.000 | 1-250-000 | 12.300 | 0 • 0 0 0 | 1305.000 | 10.500 | 0.000 | |
| BT | 1.37 | 70.000 | 11.000 | 0.000 | 1430.000 | 10.800 | 0.000 | 1730.000 | 12.300 | 0.000 | 1860.000 | |
| • ·B.T | • •] | 12.800 | 0.000 | 2100.000 | 12.500 | 0.000 | 2430.000 | 12.500 | 0.000 | 2670.000 | 11.300 | · · · · · · · · · · · · · · · · · · · |
| BT | | 0.000 | 2770.000 | 12.000 | 0.000 | 2940.000 | 15.000 | 0.000 | 3020.000 | 18.000 | ~0.000 | |
| - NC | | .065 | . 075 | .030 | ~ 300 | •500 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | |
| ET | × | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | 9.100 | 940.000 | 1700.000 | (|
| | | | · · · · · · · · · · · · · · · · · · · | | | | | | | | 21,000,000 | |
| X 1 | | 1.604 | 24,000 | 960.000 | 1055.000 | 20 000 | 26 666 | 20 000 | A AAA | e sée | | (|
| GR. | | 25.000 | 670.000 | 23.500 | 730.000 | 20.000 | 20.000 | 20.000 | -0.000 | -0.000 | -0.000 | |
| GR | | 15.000 | 960.000 | 5.000 | 970.000 | 20.000 | 890.000 | 18,000 | 900.000 | 16.000 | 940.000 | |
| GR | | -1.500 | 1020.000 | 2.500 | 1025.000 | 2.500 | 975.000 | -1.500 | 980-000 | -2.800 | 1000.000 | (|
| -GP | | 14-300 ··· | 1090.000 | 14.300 | 1130.000 | 5.000 | 1030.000 | 10.000 | 1040.000 | 13.500 | 1055.000 | |
| GR | | 12.000 | 2740.000 | 15.000 | | 11.000 | 1300.000 | 11.700 | 1560.000 | 12.300 | 2400.000 | |
| NC. | | -0.000 ·· | -0.000 | -0.000 | 2880.000 | 18.000 | 2950.000 | 25.000 | 2970.000 | -0.000 | -0.000 | (|
| NH | | 4.000 | .045 | 960.000 | .100 .035 | .300 | -0.000 | -0.000 | -0.000 | ~0.000 | -0.000 | e temperatura de la companya de la c |
| ET | | -0.000 | -0.000 | ~0.000 | -0.000 | 1040.000 | .015 | 1165.000 | .050 | 2570.000 | 0.000 | |
| ŧ., • | | 00000 | G & Q O O | -04000 | -0.000 | ··· () () () () | ~(),()() | -0.000 | 9.100 | 950.000 | 1950-000 | (|
| | | | ***** | | • | | | | | | | |
| X 1 | | 1.714 | 25.000 | 950.000 | 1040.000 | 610.000 | 610.000 | 610.000 | -0.000 | -0.000 | -0.000 | |
| ··· GR·· | | 25.600 | 790.000 | 20.000 | 900.000 | 19.000 | 910.000 | 18.000 | 950.000 | 15.000 | 960.000 | |
| GR | | 5.000 | 976.000 | 4.000 | 980.000 | 1.600 | 1000.000 | 4.000 | 1020.000 | 5.000 | 1025.000 | |
| GR- | 1 | . O • O O O | 1035.000 | 14.000 | 1040.000 | 13.000 | 1075.000 | 13.000 | 1125.000 | 12.500 | 1165.000 | |
| GR | 1 | 1.200 | 1300.000 | 12.500 | 1490.000 | 13.500 | 1640.000 | 12.000 | 1.765.000 | 11.000 | 1900.000 | (|
| G R | 1 | 5.000 | 5550.000 | 18.000 | 2350,000 | 19.000 | 2570.000 | 20.500 | 2770.000 | 25.000 | 3190.000 | |
| NC | | .065 | .050 | .030 | .100 | .300 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | |
| | | | | | | | | | | | | |
| X1 | | 1.732 | 29.000 | 961.000 | 1037.000 | 150.000 | 90 666 | 338 000 | 0 5AA | 0.000 | 0.000 | |
| X3 | | 0.000 | -0.000 -0.000 | -0.000 | =0.000 =0.000 | -0.000 | 000.08 | 110.000 ··· | 11 300 | -0.0000 | ~0,000 | (|
| -GR- | | 5.000 | 790.000 | 22.800 | 825.000 | 1.5.000 | | | 11.300 | 11.300 | -0.000 | |
| GR | ۲., | .300 | 972.000 | •800 | 986.000 | | 940.000 | 11.300 | 961.000 | 2.200 | 962.000 | ······································ |
| GR | | 1.900 | 1001.010 | • 700 | 1014.000 | 1.900 1.400 | 1000.000 | 11.300 | 1000.010 | 11.300 | 1001.000 | (|
| GR | | 4.000 | 1065.000 | 12.500 | 1550.000 | 12.000 | 1026.000 | 3.300 | 1036.000 | 11.300 | 1037.000 | |
| GR | | 1.500 | -1800.000 | 11.000 | 1880.000 | 12.300 | 1370.000 | 12.500 | 1500,000 | 13.500 | 1630.000 | |
| GR | | 8.000 | 2465.000 | 19.000 | | | 2130.000 | 15.000 | 2200,000 | | 2300-000- | √ |
| , | J. | | 2702 0 000 | 1 4 0 0 0 0 | 2560.000 | 20.500 | 2770.000 | - 25.000 | 3190.000 | ~0.000 | -0.000 | |
| . د ر | | معرضه | . | | _ | | | | | | | |
| X1 | | 1.733 | ·· -0.000 | -0.000 | -0.000 | 1.000 | 1.000 | 1.000 | 0 • 0 0 0 | -0.000 | →()•(/()() | |
| X2 | | 0.000 | -0.000 | -0.000 | 11.300 | 11.000 | -0.000 | -0.000 | -0.000 | -0.000 | ~0.00u | |
| BT | | 8.000 | 790.000 | 25.000 | 0.000 | 825.000 | 22.800 | 0.000 | 9407000 | 15.000 | | The state of the s |
| BT | 96 | 1.000 | 14,300 | 11.300 | 970.000 | 14.000 | 11.300 | 1025.000 | 13.500 | 11.300 | 1037.000 | · · |
| | | | | | | | | | | | | |

| | вт | 13,600 | 11.300 | 1065.000 | 14.000 | 0.000 | 1220.000 | 12.500 | 0.000 | 1370.000 | 12.000 | | 7 |
|-----|------------------|-----------------------|----------------------|------------------|--------------------|--------------------|----------------------|------------------|--------------------|-------------------|----------------------|--|-----------------------|
| 1 | - B T | 0.000 | 1500.000 | 12.500 | 0.000 | 1630.000 | 13.500 | 0.000 | 1800,000 | 11.500 | 0.000 | | (|
| | вт | 1880.000 | 11.000 | 0.000 | 2130.000 | 12 + 300 | 0.000 | 2200.000 | 15.000 | 0.000 | 2300.000 | | |
| , | -BT | 18.000 | 0.000 | 2465.000 | 18.000 | 0.000 | 2560.000 | 19.000 | 0.000 | 2770.000 | 20.500 | | |
| • | BT | 0.000 | 3190.000 | 25.000 | ~0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | • | |
| | - NC | -0.000 | -0.000 | -0.000 | 500 | | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | | |
| | | | | | | • | | | | | **** | | (|
| | X1 | 1.884 | 31.000 | 959.400 | 1041.000 | 800.000 | 800.000 | 800.000 | -0.000 | -0.000 | -0.000 | | |
| | - X 2 | -0.000 | -0.000 | -0.000 | 1200.000 | 8.800 | -0.000 | -0.000 | -0.000 | -0.000 | -v.000 | | |
| | BT | 21.000 | 0.000 | 25.000 | 0.000 | 60.000 | 20.000 | 0.000 | 90.000 | 15.000 | 0.000 | | l l |
| | - 8 T | 200.000 | 10.000 | | ~580¥000 · | 8 4.800 | 0.000 | 670.000 | 9.500 | 0.000 | 730.000 | | and the second second |
| | 8 T | 10.500 | 0.000 | 840.000 | 10.500 | 0.000 | 930.000 | 11.500 | 0.000 | 957.000 | 14.200 | | , |
| | ·· B T | 1.2.000 | 1041.000 | 14.200 | 12.000 | 1050.000 | 12.500 | 0.000 | 1100.000 | 13.000 | 0.000 | | |
| | 8 T | 1150.000 | 12.500 | 0.000 | 1400.000 | 12,300 | 0.000 | 1470.000 | 15.000 | 0.000 | 1640.000 | | |
| | BT | 18.000 | 000 | 1720.000 | 18.000 | 0.000 | 1730.000 | 60000 | 0.000 | 2100.000 | 20.000 | | |
| | BT | 0.000 | 2170.000 | 25.000 | 00000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | ~0.000 | | , |
| | -GR | 25.000 | 0.000 | 20.000 | 60.000 | 15.000 | 90.000 | 10.000 | 200.000 | 8,800 | 580.000 | | |
| | GR | 9.500 | 670,000 | 10.500 | 730.000 | 10.500 | 840.000 | 11.500 | 930.000 | 11.700 | 957.000 | 1 | (|
| | GR | 12.000 | 959.400 | 6.400 | 959.500 | 2.100 | 986.000 | 2.400 | 1000.000 | 12.000 | 1000.010 | | |
| | GR GR | 11.900 12.000 | 1001.000 | 2.400 | 1001.010 | 2.600 | 1015.000 | 4.100 | 1038.000 | 6.000 | 1040.000 | | |
| 2 | GR | 15.000 | 1041.000 1470.000 | 12.500 18.000 | 1050.000 | 13.000 18.000 | 1100.000 1720.000 | 12,500 | 1150.000 | 12,300 | 1400.000 | | (|
| | GR | 25,000 | 2170.000 | -0.000 | -0.000 | -0.000 · · | -0.000 | 20.000 | 1730.000 | 20.000 -0.000 | 2100.000 | | |
| | GN | & J • O O O | 21100000 | -0,000 | -0.000 | -0.000 | ~ O . O O O | -0.000 | -0,000 | -0.000 | -0,000 | | |
| | | | | | a service process | | | | | | | | |
| | X 1. | 1.885 | -0.000 | -0.000 | -0.000 | 1.000 | 1.000 | 1.000 | -0.000 | -0.000 | ~O•000 | | |
| | E T | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | 9.100 | 800.000 | 1200.000 | | |
| | | | | | | | | | | | | | (|
| | | 1 000 | | | | | | | | | | | y |
| | X1 | 1.895 | 30.000 | 976.000 | 1031.000 | 60.000 | 60.000 | 60.000 | -0.000 | -0.000 | ~0.000 | | (|
| | GR | 25:000 | 0.000 | 20.000 | 90,000 | 15.000 | 110.000 | 11.000 | 190.000 | 10.000 | 210.000 | | |
| | GR | 9.800 | 240.000 | 9,800 | 380.000 | 9.500 | 430.000 | 8.500 | 490.000 | 9.000 | 545.000 | | |
| | GR GR | / 8.800 | 590.000 976.000 | 9,300 4,500 | 640.000 977.000 | 9.500 2.500 | 680,000 | 10.000 | 700.000 | 10.500 | 9207000 | | (|
| | -GR- | 4.500 | 1025.000 | 10.000 | 1030,000 | 12.000 | 980.000 1031.000 | 2,000 | 1000.000 | 2.500 11.000 | 1020.000 1270.000 | | |
| | GR | 15.000 | 1420.000 | 18.000 | 1580.000 | 20.000 | 1650.000 | 20.000 | 2040.000 | 25.000 | 2080.000 | | |
| | NC | -0.000 | -0.000 | -0.000 | .100 | •300 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | | (|
| | NH | 5.000 | .050 | 705.000 | .025 | 860.000 | .050 | 980.000 | .035 | 1060.000 | .050 | | |
| | NH | 1480.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | | |
| | EΤ | ~() • () () () | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | 9.100 | 750.000 | 1250.000 | | (|
| | , | | | | | | • | | | | | | , |
| | V.1 | 1 0/0 | 22 000 | 000 000 | 10/0 000 | 2/0.000 | 270 000 | 254 002 | 0.000 | 0.000 | 3 8 8 W | | (|
| | X1 | <u>1960</u> 25-000 | 0.000 0.000 | 980.000 | 1060.000 | 340.000 | 370.000 | 350.000 | -0,000 | ~0.000 € | 000000 | | |
| | GR | 8.800 | | 20.000 | 220.000 | 15.000 | 230.000 | 12.500 | 295.000 | 10.000 | 340.000 | | |
| | GR GR | 11.500 | 395.000 780.000 | 10.300 11.000 | 475.000 815.000 | $10.500 \\ 10.500$ | 660.000 860.000 | 10.500 10.300 | 705-000 955-000 | 11,500 10,000 | 7607000 | | (|
| | | V 5.000 | 984.000 | 2.500 | 990.000 | 1.600 | 1000.000 | 2.500 | 1010.000 | 4.500 | 980.000 1015.000 | | |
| | $-\frac{G}{GR}I$ | 5.000 | 1016.000 | 10.000 | 1060.000 | 10.200 | 1090.000 | 10.500 | 1135.000 | 10.800 | 1175.000 | | |
| | GR | 11.300 | 1230.000 | 11.300 | 1280.000 | 13.500 | 1330.000 | 18.000 | 1410.000 | 20.000 | 1480.000 | | · (|
| | GR | 20.000 | 2000.000 | 25.000 | 2100.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | ~0.000 | | |
| | NC | | | | .400 | .700 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | | |
| | - | | | | ▼ · ✓ · · | • • • • • | | W + V W M | and the second | er we har har har | 0 4 4 9 6 | | (|
| | 200 - 100 - 100 | | | | • | | | | | | | | |
| | X 1 | 1,979 | 29.000 | 974.000 | 1026.300 | 120.000 | 100.000 | 110.000 | -0.000 | -0.000 | -0.000 | | |
| | GR | 20.000 | 210.000 | 15.000 | 230.000 | 10.000 | 380.000 | 11.000 | 660.000 | 11.000 | 720.000 | | |
| | GR | 13.000 | 855.000 | 13.500 | 900.000 | 13.300 | 953.000 | 13.300 | 973.000 | 10.000 | 974.000 | | , |
| ' L | GR | 3.300 | 974.100 | 1.800 | 990.100 | 10.000 | 990.200 | 10.000 | 991.500 | 1.800 | 991.600 | | []. [|
| , ' | GR | 1.300 | 1007.800 | 10.000 | 1007.900 | 10.000 | 1009.200 | 1300 | 1009.300 | 3.800 | 1026.200 | | 11 |
| | GR | 0,900 | 1326.300 | 12.500 | 1.00.000 | | 1080.000 | 10,000 | 1130.000 | 10.300 | 1260.000 | | |
| | GR | 11.000 | 1300.000 | 15.000 | 1400.000 | 18.000 | 1470.000 | 20.000 | 1550.000 | -0.000 | -0.000 | | |
| | | | • | | | | | | | | | | |
| | X 1 | 1.980 | | -0.000 | | 1.600 | 1.000 | 1-000 | | -0.000 | -()()() | garagan garagan garagan garagan kan dada dan sebesah dan kan dan dan sebesah dan kan dan dan sebesah dan dan d | |
| | XŽ | -0.000 | -0.000 | -0.000 | 10.000 | 10.000 | -0.000 | -0.000 | -0.000 | -0.000 | ~0.060 | | (|
| | | | | | | | - | | | <u> </u> | | | |

| | 8T | 82.000 | 0.000 | 25.000 | 0.000 | 000.0US | 20.000 | 0.000 | 230,000 | 15.000 | 0.000 | , . | (|
|-------|--------------|--------------------|-------------------|-------------------|---------------------|---------------------|------------|-------------------------------|------------------|--|-------------------------|---------------------------------------|----|
| | BT ··· | 380.000 | 10.000 | 0.000 | 660.000 | 11:000 | 0.000 | 720.000 | 11.000 | 0.000 | 855,000 | | ţ |
| | BT | 13.000 | 0.000 | 900.000 | 13.500 | 0.000 | 953.000 | 13.300 | 0.000 | 973.000 | 13.300 | | |
| | BT BT | 0.000 | 974-000 | 15.300 | 1110.000 | 1026.300 | 14.900 | 10.000 | 1050.100 | 12.500 | 0.000 | | (|
| | BT | 1080.000 | 11.000 | 0.000 | 1130.000 | 10.000 | 0.000 | 1260.000 | 10.300 | 0.000 | 1300.000 | | |
| | BT | 0.000 | 0.000 1900.000 | 1400.000 | 15.000 | 0.000 | 1470.000 | 18,000 | 0.000 | 1550,000 | 20.000 | 9 | |
| | | | 1.400.000 | 20.000 | 0.000 | 5000.000 | 25.000 | -0.000 | ~0 o 0 0 0 o | ∞0.000 | ~0.000 | | (|
| | | | | | | | | | | | | | |
| | X 1 | 2.057 | 22.000 | 971.000 | 1029,500 | 450.000 | 350.000 | 400.000 | | ······································ | | | |
| | X2 | -0.000 | -0.000 | -0.000 | 10.000 | 11.500 | -0.000 | -0.000 | -0.000 -0.000 | -0.000 | -0.000 | | (|
| - | 8T | 9.000 | 195.000 | 25.000 | 0.000 | 210.000 | 50.000 | 0.000 | 260,000 | -0.000 | -0.000 | , | |
| | 8 T | 640.000 | 11.500 | 0.000 | 720.000 | 12.500 | 0.000 | 850.000 | 15.000 | 15.000 0.000 | 0.000 | | |
| | ВТ | 19.000 | 10.000 | 1029.500 | 2100.000 | 1000.000 | 112000.000 | 2500.000 | -0.000 · | -0.000 | 971.000 | | { |
| | GR | 25.000 | 195.000 | 20.000 | 210.000 | 15,000 | 260.000 | 11.500 | 640.000 | 12.500 | 720.000 720.000 | | |
| | GR | 15.000 | 850.000 | 10.000 | 971.000 | 1.100 | 971.100 | 3.200 | 979.000 | 3.100 | 988.305 | | |
| | GR | 10.000 | 988.400 | 10.000 | 989.700 | 2.700 | 989.800 | 1.600 | 1000.000 | .100 | 1010.800 | | (|
| | GR | 10.000 | 1010.900 | 10,000 | 1012.200 | 900 | 1012.300 | .900 | 1021.000 | •100 •100 | 1029,400 | | |
| | GR | 10.000 | 1029.500 | 25.000 | 1120.000 | -0.000 | ≈0.000 | -0.000 | -0.000 | -0.000 | -0.000 | | |
| | | | | | | 0 • 0 0 | | | | | | | (|
| | | | | | | | | | | | | | |
| | X1 | 2.058 | 0 . 000 | -0,000 | -0.000 | 1.000 | 1.000 | 1.000 | -0.000 | -0.000 | -0.000 | | |
| | Х3 | 10.000 | -0.000 | -0.000 | -0.000 | ~0.000 | -0.000 | -0.000 | 11.500 | 11.500 | -0.000 | | (|
| 4 | ET | -0.000 | -0.000 | -0.000 | ···· -0 • 0 0 0 · | 0.000 | -0.000 | -0.000 | 9.100 | 750.000 | lujv, too | | |
| | NC | .035 | .035 | .030 | .300 | .500 | -0.000 | -0.000 | ~O.OOO | -0.000 | -0.000 | | |
| - | | | | | | | | e e e e e e e e e e e e e e e | | | | | (|
| | | | | | | | | | | | | | |
| | X1 · · · | ··· 2 • 063 · | 17.000 | 920,000 | 1041.000 | 50.000 | 30.000 | 40.000 | -0.000 | -0.000 | ~0.000 | | į. |
| | GR | 25.000 | 250,000 | 20.000 | 320.000 | 18.000 | 360.000 | 15.000 | 530.000 | 12.000 | 710.000 | • | 1 |
| | GR 1 | 12.000 | 830.000 | 11.500 | 900.000 | 10.000 | 920.000 | 4.500 | 965.000 | 2.000 | 970.000 | | |
| | GR A | 1.800 | 1000.000 | 2.000 | 1030.000 | 4.500 | 1040.000 | 9.500 | 1041.000 | 15.000 | 1100.000 | | , |
| | ·GR·1 | 20.000 | 1130.000 | 25.000 | 1160.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | ~0 · 0 0 0 | | į. |
| | NC | .035 | .035 | .030 | .600 | .800 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | | |
| | ET | - 0.9000 | ····-0.000 | -0.000 | -0.000 | ····· • () • () 0 0 | -0.000 | -0.000 | 9.100 | 960.000 | 1200.000 | | (|
| | | | | | • | | | | | | | | , |
| 1 | X1 | 2 1 4 1 | 22 000 | 060 000 | 1020 000 | (20.000 | | | | | | | |
| | GR | 2.141 25.000 | 22.000 700.000 | 960.000 20.000 | 1030.000 701.000 | 420.000 | 420.000 | 420.000 | -0.000 | -0.000 | -0.000 | | ĺ |
| | | 7 17.500 | 890.000 | 15.000 | 920.000 | 20.000 11.000 | 715.000 | 17.300 | 800.000 | 17.500 | 860,000 | | ` |
| | GR. | 7.000 | 1000.000 | 7.500 | 1025.000 | 10.000 | 940.000 | 10.000 | 960.000 | 7.500 | 975.000 | | |
| | GR | 13.000 | 1190.000 | 12.300 | 1260.000 | 12.500 | 1030.000 | 15.000 | 1050-000 | 12.500 | 1110.000 | | ĺ |
| | GR | 17.000 | 1449.000 | 25.000 | 1450.000 | -0.000 | -0.000 | 15.000 -0.000 | 1370.000 | 16.300 | 1410.000 | | |
| | NC | -0.000 | -0.000 | -0.000 | .600 | .800 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | | |
| | | | | W • O O O | 0.000 | 0 0 0 0 | -0.000 | -0.000 | ~0.000 | ~0.000 | -() ₆ ()()() | | (|
| | | | | | | | | | | | | | |
| | X.1 | 2.150 | 1.9.000 | 968,000 | 1032.000 | 50.000 | 50.000 | 50.000 | -0.000 | -0.000 | | | |
| | Х3 | 10.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | 14.000 | 13.900 | -0.000 | | (|
| 24144 | GR | 25,000 | 800.000 | 20.000 | 855.000 | 19.000 | 942.000 | 18.500 | 951.800 | 14.000 | 968.000 | | |
| | GR | 8.100 | 970.000 | 7.700 | 980.000 | 7.400 | 1000.000 | 7.500 | 1012.000 | 7.900 | 1030.000 | | |
| | GR ·· | 13,900 | - 1032-000 | 19.000 | 1049,000 | 18,800 | 1068,000 | 17.500 | 1100.000 | 15.000 | 1220.000 | | (|
| - | GR | 13.000 | 1340,000 | 15.000 | 1430,000 | 16,500 | 1490.000 | 25.000 | 1491.000 | -0.000 | -0.000 | | |
| | S B | -0.000 | ····· 1.560 | 2.600 | -0.000 | 63.000 | -0.000 | 400.000 | 7.93 | 7.700 | 7.700 | | |
| | | | | | | | | | | | | | (|
| | | | | | | | | | | | | | |
| | X 1 | 2.157 | -6.000 | -0.000 | -0.000 | 35.000 | 35.000 | 35.000 | -0.00 | -0.000 | -0.000 | | - |
| | X-2 | -0.000- | -0.000 | 1.000 | 14.000 | 13.000 | -0.000 | -0.000 | - (i o (j (i () | -0.0000 | -0.000 | | ı |
| | X3 | 10.000 | -0.000 | =(),()()() | ~(),()()() | ~0.000 | -0.000 | -0.000 | 18.500 | 13.000 | ~0.000 | | |
| | P.T | 19.000 | 800.000 | 25.000 | 0.000 | 855,000 | 20.000 | 0.000 | 942.000 | 19.000 | 0.000 | | |
| | 8 T | 951.800 | 18.500 | 0.000 | 953.000 | 23.400 | 0.000 | 965.000 | 23,600 | 0.000 | 965.400 | | • |
| | BT or | 21,800 | 0.000 | 1000.000 | 22,100 | 13.900 | 1035.000 | 21.800 | 0.000 | 1035.100 | 23.600 | | |
| | BT BT···· | 0.000 -1100.000 | 1047.000 | 23.400 | 0,000 | 1049.000 | 19.000 | 0.000 | 1068.000 | 18.800 | 0.000 | | (|
| | n T | 15.000 | 17.500 0.000 | 1490 000 | 1220.000 | 15.000 | 0.000 | 1340.000 | 13.000 | 0.000 | 1430 000 | | . |
| | NH NH | 5.000 | .050 | 1490.000 | 16,500 | 0.000 | 1491,000 | 25.000 | -0.000 | -0.000 | ~0.000 | , | |
| | NH NH | 1501.000 | -0.000 | 890.000 -0.000 | •025 •0•000 | 945.000 | .060 | 960.000 | 0.000 | 1040.000 | | · · · · · · · · · · · · · · · · · · · | 1 |
| , | . 1 1 1 | * > O * O O O O | 0.000 | 0.000 | | -0.00 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | | |

| | ET | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | 9.100 | 900.000 | 1350.000 | ſ |
|-------|--------------------------------------|---------|---|------------------------|---------------|-----------------|-----------------|------------------|------------------|------------------|------------------|--|
| | | | | · | | | | | | | | |
| - | X1. | 2.161 | 19,000 | 960,000 | 1040.000 | 20.000 | 20.000 | 20.000 | -0.000 | -0.000 | -0.000 | |
| | X3 | 10,000 | -0.000 | -0.000 | ~0.000 | -0.000 | ~0 . 000 | -0.000 | 16.500 | 16.500 | -0.000 | (|
| | GR | 25.000 | 850,000 | 20,000 | 890,000 | 18.500 | 920,000 | 19,000 | 945.000 | 15.000 | 960.000 | |
| | GR [] | 10.000 | 965.000 | 8.000 | 975.000 | 8.000 | 1025.000 | 10.000 | 1030.000 | 15.000 | 1035.000 | |
| | GR / | 16.000 | 1040.000 | 15.500 | 1060.000 | 16.500 | 1100.000 | 17.500 | 1160.000 | 16.000 | 1305.000 | |
| | GR . | 15.000 | 1320.000 | 15.000 | 1440.000 | 16,300 | 1500.000 | 25.000 | 1501.000 | -0.000 | ~0 • 0 0 0 | |
| | NC | | | ()45 | .100 | .300 | ~0.000 | -0.000 | -0.000 | -0.000 | -0.000 | |
| | ET | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | 9.100 | 950.000 | 1450.000 | (|
| 4 | | | ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, | | | | | | | | | 4 |
| : - | X1 | 2.265 | 10.000 | 965.000 | 1021.000 | 600.000 | 520.000 | 560.000 | -0.000 | ~0.000 | -0.000 | |
| | GR 🔨 | 25.000 | 885.000 | 20,000 | 895.000 | 15,000 | 965.000 | 10.000 | 980.000 | 10.000 | 1020.000 | |
| | GR (🗘 | 13.000 | 1021-060 | 15,000 | 1065.000 | 16.000 | 1250.000 | 16.000 | 1600.000 | 25,000 | 1601.000 | |
| | NC | .080 | .030 | •030 | •100 | .300 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | (|
| | ET | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | 9.100 | 890.000 | 1050.000 | |
| | | | | | | | | | | | | · · · · · · · · · · · · · · · · · · · |
| | X1 | 2.788 | 16.000 | 890.000 | 1046.000 | 2220.000 | 2480.000 | 2530.000 | -0.000 | -0.000 | ~0.000 | |
| | X:5 · · · · · | 6%000 | 37.750 | 40,250 | 41.700 | 45,450 | 41.700 | -() () () () -() | 41.700 | = 0 0 0 0 | ~0.000 | |
| | GR 🛌 | 58.500 | 832.000 | 36.800 | 890.000 | 35,000 | 897.000 | 31.500 | 911.000 | 29.400 | 919.000 | (|
| 1000 | GR Jan | 58.000 | 940.000 | 28.000 | 971.000 | 25,100 | 1000.000 | 29,600 | 1022.000 | 30.800 | 1029,000 | · · · · · · · · · · · · · · · · · · · |
| | GR I 1 | 33,400 | 1039.000 | 35.000 | 1040.000 | 40.100 | 1046.000 | 42.500 | 1075.000 | 45.000 | 1085.000 | |
| | GR | -50,000 | 1090.000 | -0.000 | (),()()() | -0.000 | -0.000 | -0.000 | -0.000 | | -0.000 | |
| | NC | .040 | • 055 | .030 | 005. | • 400 | -0.000 | -0.000 | -0.000 | -0.000 | ~0.000 | |
| | ET | | 0 -0 000 | -0.000 | ~O.OOO. | -0.000 | -0.000 | =0.000 | 9 • 100 | 945.000 | 1055.000 | |
| Ç-5- | | | | | | | | | | | | |
| | X 1 | 3.096 | 15.000 | 945.000 | 1055.000 | 1630.000 | 1630.000 | 1630.000 | -0.000 | -0.000 | -0.000 | |
| | GR | 50.000 | 560.000 | 45.000 | 590.000 | 41.500 | 650.000 | 43.000 | 700.000 | 40.500 | 760.000 | (|
| | GR S | 40.200 | 840.000 | 38.600 | 880.000 | 38.000 | 945.000 | 35.200 | 960.000 | 32.500 | 970.000 | |
| | GR U | 32.300 | 1030.000 | 35.200 | 1040.000 | 39.000 | 1055.000 | 40.000 | 1060.000 | 50.000 | 1070.000 | |
| | NC | 035 | .045 | .030 | .100 | .300 | -0.000 | -0.000 | 0.000 | -0.000 | -0.000 | (|
| | FT | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | 9.100 | 940.000 | 1050,000 | |
| | •- • | 0.00 | | | 0,000 | 0.000 | 0.000 | 0.000 | 7.100 | 710.000 | 1070,000 | 1 |
| | X1 | 3.351 | 21.000 | 940.000 | 1050.000 | 1330.000 | 1300.000 | 1310.000 | -0.000 | -0.000 | ~0.000 | |
| | GR | 55.000 | 390*000 | 52.000 | 420,000 | 50.000 | 450.000 | 48.500 | 470.000 | 48.000 | 525.000 | |
| | GR | 45.200 | 575.000 | 46.600 | 645.000 | 46.000 | 710.000 | 48.000 | 785.000 | 45.000 | 860.000 | (|
| | GR T | 44.600 | 975.000 | 43.500 | 940,000 | 40.000 | 965.000 | 38.500 | 970.000 | 38.000 | 1000.000 | |
| | GR / | 38,500 | 1030.000 | 40.000 | 1035.000 | 41.500 | 1050.000 | 45.000 | 1100.000 | 50.000 | | |
| | GR · | 55.000 | 1125.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | | 1135.000 | (|
| | VC | .035 | .035 | .030 | .200 | •400 | -0.000 | -0.000 | | -0.000 | -0.000 -0.000 | |
| | ET | 0.000- | ····· ·-0.000 ·· | 0.000 | -().()()() | -0.000 | -0.000 | -0.000 | -0.000 9.100 | 910.000 | 1050.000 | |
| , | im I | 0.000 | 0.000 | ~ 0.000 | - (4 8 0 (7 0 | -0,000 | -0.000 | -0.000 | 7 . 3.00 | 310,000 | 10000000 | (|
| g.v.v | X] | 3.475 | 13.000 | 975.000 | 1050.000 | 640.000 | 680.000 | 660.000 | -0.000 | -0.000 | ~O.000 | |
| | ^ 1 3 R ₂ ₂ | -55,000 | 840.000 | 52.500 | 865.000 | 50.000 | 890.000 | 49.000 | 920.000 | 49.500 | 945.000 | ······································ |
| | GR / | 49.000 | 975.000 | 45.000 | 980.000 | 41.000 | 985.000 | | | | | |
| | SR U | 47.000 | -1045.000 | 50.000 | 1050.000 | 55 . 000 | 1060.000 | 41,000 | 1015.000 | 47.000 | 1025.000 | |
| | J | ~0.000 | -0.000 | -0.000 | -0.000 | -0.000 | 0.000°000 | -0.000 -0.000 | -0.000 -0.000 | -0.000 -0.000 | -0.000 | (|
| , | | | | · | - , , - | | 🗸 🗸 🗸 | | | | | · · · · · · · · · · · · · · · · · · · |
| | | | | | | | | | | | | |

HEC2 RELEASE DATED NOV 76 UPDATED AUG1977

ERROR CORR - 01,02

MODIFICATION - 50,51,52,53

NOTE- ASTERISK (*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

PEQUONNOCK RIVER

SUMMARY PRINTOUT

| | SECNO | CWSEL | Q | VCH | ₽ G | DIFWSP | DIFEG | SSTA | STENCL | STCHL | STCHR | STENCR | ENDST |
|-------------------------|------------------------|--------------|--------------------|--------------------------------------|--------------------|-------------|-------|------------------|----------------|----------|---------------------|-----------------|------------------------|
| floodway no floodway A | .057 .057 | 3.60 3.60 | 9560.00 9560.00 | •52 •52 | 3.60 3.60 | 0.00 | 0.00 | 618.30 618.30 | 0.00 615.00 | 615.00 | 1270.00 | 0.00 | 1269.95 |
| floodway no floodway | .116 | 3.59 3.59 | 9560.00 9560.00 | 1.55 | 3 • 63 3 • 63 . | 0.00 | 0.00 | 824.82 | 0.00 | 743.50 | 1270.00 1243.30 | 1270.00 | 1269.95 |
| floodway | • 1.3 1 | 3.59 | 9560.00 | 1.55 | 3.63 | 0.00 | 0.00 | 824.82 824.82 | 0.00 | | 1243.30 | 0.00 | 1243.25 |
| no floodway | .257 | 3.59 | 9560.00 | 1,55 | 3 - 63 | •00 | • 00 | 824.82 | 0.00 | | 1243.30 | 0.00 | 1243.25 1243.25 |
| no floodway B | . 257 | 3 • 6 1 | 9560.00 | 1.29 | 113.64111 3.64 | 00 | 00 | 842.75 842.75 | 0.00 830.00 | |) 175.00 1175.00 | 0.00 1175.00 | 1170.13 1170.13 |
| floodway no floodwa | •390 ay•390 | 3.61 3.61 | 9560.00 9560.00 | 2.55 2.55 | 3.69 3.69 | 0.00 | 0.00 | 784.08 784.08 | 0.00 | | 1068.10 | 0.00 | 1178.56 1178.56 |
| floodway no floodway | .437 .437 | 3.68 3.68 | 9560.00 9560.00 | 1.02 | 3.70 3.70 | 0.00 | .00 | 799.69 800.00 | 0.00 | | 1201.00 1201.00 | 0.00 1205.00 | 1200.53 (1200.53) |
| | •481 •481 | 3.67 3.67 | 9560.00 9560.00 | 2.14 2.14 | 3.74 3.74 | 0.00 .00 | 0.00 | 796.03 796.03 | 0.00 | | 202.20 | 0.00 | 1202.17 |
| | •498 •498 | 3.67 3.67 | 9560.00 9560.00 | 2.16 2.16 | 3.75 3.75 | 0.00 | 0.00 | 796.03 796.03 | 0.00 0.00 | | 202.20 202.20 | | 1202.17 1202.17 |
| | .573 .573 | 3.70 3.70 | 9560.00 9560.00 | 2 • 09 2 • 09 | 3.77 3.77 | 0.00 | 0.00 | 884.56 884.56 | 0.00 680.00 | | 120.00 | | 1117.41 |
| , | • 701 • 701 | 3.71 3.71 | 9560.00 9560.00 | "3 • 2 2 3 • 2 2 | 3.87 3.87 | 0.00 | 0.00 | 851.04 851.04 | 0.00 0.00 | | 034.00 034.00 | 0.60 | 1031.08 |
| *********** | • 711 ••• 711 ····· | 3.70 3.70 | 9560.00 9560.00 | 4.01 4.01 | 3.95 3.95 | 0.00 | 0.00 | 851.04 851.04 | 0.00 | | 034.00 034.00 | | 1031.08 |
| E | .834 .834 | 3.98 | 9560.00 | 2 6 2 6 2 6 2 6 | 4.06 4.06 | 0.00 | 0.00 | 875.43 ··· | 0.00 870.00 | | 140.00 | | 1113.99 |
| | •952 · •952 | 4.00 | 9560.00 9560.00 | 2.70 2.70 | 4 • 1 1 4 • 1 1 | 0.00 | 0.00 | 860.81 | 0.00 | 817.00 1 | 179.60 179.60 | 0.00 | 1140.98 1140.98 |

| Accessed to the Control of | SECNO | ······ CWSFL····· | o | vcH- | E G | OIFWSP | DIFFG | SSTA | STENCL | sтонь | | STENCR | ENDST | (|
|---------------------------------------|----------------|-------------------|---------------------|--------------------------------|----------------|------------------|---|-------------------------|------------------|------------------|--------------------|-----------------|--------------------|---------------------------------------|
| | .962 .962 | 4.01 | 9560.00 9560.00 | 2.70 2.70 | 4.12 4.12 | 0.00 | 0.00 | 860.81 860.81 | 0.00 0.00 | 817.00 817.00 | 1179.60 1179.60 | 0.00 0.00 | 1141.01 1141.01 | . (|
| Ľ | 1 096 | 4.07 | 9560.00 | 2.71 | 4.18 | 0.00 | 0.00 | 876.16 | 0.00 | 875.00 | 1130.00 | 0.00 | 1127.68 | (|
| | 1.096 | 4.07 | ···9560.00 | 2.71 | 4.18 | • 00 | • | 876.16 | 875.00 | 875.00 | 1130.00 | 1130.00 | 1127.68 | |
| G | 1.250 1.250 | 4.07 4.07 | 9560.00 9560.00 | 4.19 4.19 | 4.35 4.35 | 0.00 00 | 0.00 | 871.54 871.54 | 0.00 865.00 | 867.00 867.00 | 1160.00 1160.00 | 0.00 1160.00 | 1123.46 1123.46 | (|
| * * * * * * * * * * * * * * * * * * * | 1.319 1.319 | 4.76 4.76 | 9560.00 -9560.00 | 14.64 14.64 | 8.09 8.09 | 0.00 | 0.00 .00 | 918.30 918.30 | . 0.00 | 917.50 917.50 | 1026.00 | 0.00 0.00 | 1022.00 | (|
| | 1.329 1.329 | 6.79 6.79 | 9560.00 9560.00 | 11.20 11.20 | 8.74 8.74 | 0.00 | 0.00 .00 | 917.50 917.50 | 0.00 | 917.50 917.50 | 1026.00 1026.00 | 0.00 | 1026.00 1026.00 | · · · · · · · · · · · · · · · · · · · |
| Н | 1.349 | 7.20 7.20 | 9560.00 9560.00 | 13.74 13.74 | 10.13 10.13 | 0.00 | 0.00 | 964.34 964.34 | 0.00 960.00 | 962.00 962.00 | 1055.00 | 0.00 1055.00 | 1042.20 1042.20 | (|
| I | 1.490 1.490 | 10.85 | 9560.00 9560.00 | 5.55 5.55 | 11.32 11.32 | 0.00 00 | 0.00 | 910.00 910.00 | 910.00 | 910.00 910.00 | 1075.00 1075.00 | 0,00 1075.00 | 1075.00 | . (|
| * J | 1.583 1.583 | 13.11 13.31 | 8615.00 8615.00 | 10.69 11.37 | 14.15 14.53 | 00.0 | 0.00 | 957.56 970.00 | 0.00 970.00 | 985.00 985.00 | 1015.00 | 0.00 1750.00 | 2141.43 1750.00 | . (|
| · * | 1.590 1.590 | 13.23 14.63 | 8615.00 8615.00 | 9.86 6.00 | 14.36 14.92 | 0.00 | 0.00 .56 | 970.53 969.89 | 0.00 | 972.00 | 1018.10 | 0.00 | 2839.44 2919.17 | . (|
| | 1.600 1.600 | 13.63 14.66 | 8615.00 8615.00 | 8.44 5.81 | 14.36 14.92 | 0.00 1.03 | 0.00 .56 | 972.00 972.00 | 0.00 | 972.00 972.00 | 1018.10 1018.10 | 0.00 0.00 | 2862.42 2920.59 | . (|
| | 1.604 1.604 | 14.19 14.54 | 8615.00 8615.00 | 5 . 49 6 . 47 | 14.50 15.06 | 0 • 0 0 • 3 5 | 0.00 .56 | 960.82 960.46 | 940.00 | 960.00 | 1055.00 | 0.00 1700.00 | 2841.93 1700.00 | . (|
| K | 1.714 | 14.70 15.34 | 8615.00 8615.00 | 5 • 2 5 4 • 3 9 | 14.93 15.49 | 0.00 | 0.00 .56 | 960.30 958.86 | 0.00 950.00 | 950.00 950.00 | 1040.00 | | 2196.36 1950.00 | (|
| | 1.732 | 14.76 15.38 | 8615.00 8615.00 | 5.04 4.21 | 15.00 15.53 | 0.00 | 0.00 .53 | 941 • 38 · · · 934 • 41 | 0 • 00 0 • 00 | 961-00 961-00 | 1037.00 | | 2193.67 2212.64 | (|
| | 1.733 1.733 | 14.76 15.38 | 8615.00 8615.00 | 5.04 4.21 | 15.00 15.53 | 0.00 | 0.00 | 941.38 934.40 | 0.00 | 961.00 961.00 | 1037.00 | | 2193.69 2212.65 | (|
| | 1.884··· | 15.42 15.82 | 8615.00 8615.00 | 1.86 1.69 | 15.45 15.84 | 0.00 | 0.00 | 87.50 85.10 | 0.00 | 959,40 959,40 | 1041.00 | | 1493.64 1516.28 | . (|
| | 1.885 1.885 | 15.41 15.81 | 8615.00 8615.00 | 3.03 2.77 | 15.47 15.86 | 0.00 | 0.00 | 87.49 85.10 | 0.00 | 959.40 959.40 | 1041.00 | | 1493.68 1516.30 | . (|
| 4 | 1.895 1.895 | 15.42 15.65 | 8615.00 8615.00 | · · · · 3 • 58 7 • 89 | 15.49 16.29 | 0.00 | 0.00 | 108.30 | 0.00 | 976.00 976.00 | 1031.00 | 0.00 1200.00 | | . { |
| M | 1.960 1.960 | 15.52 16.41 | 8615.00 8615.00 | 2.65 3.84 | 15.56 16.55 | 0.00 .89 | 0.00 .98 | 228.99 750.00 | 0.00 | 980.00 | 1060.00 | 0.00 1250.00 | 1365.67 1250.00 | . (|
| | 1.979 | | 8615.00 8615.00 | 5.38 4.35 | 15.70 16.59 | 0.00 | 0.00 .89 | 228.00 · 224.08 | 0.00 | 974.00 974.00 | 1026.30 1026.30 | | 1411.67 1434.52 | (|

| S-ECNO CWS-EL O | VCH EG | OIFWSP | DIFEG | SSTA | STCHL STCHR | STENCE ENDST |
|--|----------------------------|--------|-------------|------------------------------|----------------------------------|--------------|
| 1.980 15.70 8615.00 1.980 16.58 8615.00 | 3.34 15.76 2.68 16.62 | | 0.00 | 227.21 0.00 223.68 0.00 | 974.00 1026.30 974.00 1026.30 | |
| 2.057 15.81 8615.00 2.057 16.64 8615.00 | 8.30 16.63 7.11 17.18 | | 0.00 .56 | 251.93 0.00 243.64 0.00 | 971.00 1029.50 971.00 1029.50 | |
| 2.058 16.18 8615.00 2.058 16.84 8615.00 | 7.17 16.73 6.30 17.24 | | 0.00 .51 | 248.25 0.00 241.53 0.00 | 971.00 1029.50 971.00 1029.50 | |
| N 2.063 16.72 8615.00 2.063 17.08 8615.00 | 3.66 16.87 4.24 17.31 | | 0.00 | 432.29 0.00 750.00 750.00 | 920.00 1041.00 920.00 1041.00 | |
| O 2.141 16.83 8615.00 2.141 17.20 8615.00 | 7.46 17.83 | | 0.00 | 897.99 0.00 960.00 960.00 | 960.00 1030.00 960.00 1030.00 | |
| 2.150 16.71 8615.00 2.150 17.24 8615.00 | 10.23 17.89 8.83 18.06 | | 0.00 | 958.22 0.00 956.33 0.00 | 968.00 1032.00 968.00 1032.00 | |
| 2.157 17.35 8615.00 2.157 17.72 8615.00 | 8.50 1.8.11 7.71 18.32 | | 0.00 | 968.00 0.00 968.00 0.00 | 968.00 1032.00 968.00 1032.00 | |
| * P 2.161 17.39 8615.00 2.161 17.67 8615.00 | 8.36 18.22 9.74 18.89 | | 0.00 | 951.02 0.00 949.98 900.00 | 960.00 1040.00 960.00 1040.00 | |
| Q 2.265 19.27 8615.00 2.265 20.00 8615.00 | 5.35 19.49 5.29 20.23 | | 0.00 .74 | 905.29 0.00 950.00 950.00 | 965.00 1021.00 965.00 1021.00 | |
| * R 2.788 41.70 8615.00 * R 2.788 41.70 8615.00 | 4.49 42.01 4.51 42.02 | | 0.00 | 876.90 0.00 890.00 890.00 | 890.00 1046.00 890.00 1046.05 | |
| S 3.096 42.36 8615.00 3.096 42.17 8615.00 | 7.42 43.07 9.43 43.55 | | 0.00 .48 | 635.17 0.00 945.00 945.00 | 945.00 1055.00 945.00 1055.00 | |
| * 7 3.351 45.53 8615.00 46.04 8615.00 | 11.62 47.44 11.94 48.25 | | 0.00 | 569.08 0.00 940.00 940.00 | 940.00 1050.00 940.00 1050.00 | |
| * U 3.475 51.78 8615.00 * U 3.475 51.61 8615.00 | 12.84 54.05 13.63 54.26 | | 0.00° | 872.22 0.00 910.00 910.00 | 975.00 1050.00 975.00 1050.00 | |

SUMMARY OF ERRORS

| CAUTION | SECNO= | 1.319 | PROFILE= | 1 | CRITICAL DEPTH ASSUMED |
|----------|--------|--------|-----------|-----|-------------------------------------|
| CAUTION | SECNO= | 1.319 | PROFILE= | 1 | PROBABLE MINIMUM SPECIFIC ENERGY |
| CAUTTON | SECNO= | 1.319 | PROFILE= | 1 | 20 TRIALS ATTEMPTED TO BALANCE WSEL |
| CAUTION | SECNO= | 1.319 | PROFILE= | 2 | CRITICAL DEPTH ASSUMED |
| CAUTION | | | PROFILE = | 2 | PROBABLE MINIMUM SPECIFIC ENERGY |
| CAUTION | SECNO= | 1.319 | PROFILE = | 2 | 20 TRIALS ATTEMPTED TO BALANCE WSEL |
| CAUTION | SECNO= | 1.583 | PROFILE= | 1 | CRITICAL DEPTH ASSUMED |
| | | | PROFILE: | | MINIMUM SPECIFIC ENERGY |
| CAUTION | | | PROFILE= | | CRITICAL DEPTH ASSUMED |
| CVALLON- | SECNO= | 1.583 | PROFILE | 2 | MENTMUM SPECIFIC ENERGY |
| CAUTION | SECNO= | -1.590 | PROFILE: | j . | CRITICAL DEPTH ASSUMED |
| | | | | | MINIMUM SPECIFIC ENERGY |
| CAUTION | SECNO= | 2.161 | PROFILE | 2 | CRITICAL DEPTH ASSUMED |
| | | | | | MINIMUM SPECIFIC ENERGY |

| | NOTE SECNO= | | | WSEL BASED ON X5 CARD WSEL BASED ON X5 CARD | | | (|
|----|---|----------------|--------------------------|--|----------|---------------------------------------|---|
| į. | CAUTION SECNO= | 3.351 3.351 | | CRITICAL DEPTH ASSUMED MINIMUM SPECIFIC ENERGY | | · · · · · · · · · · · · · · · · · · · | (|
| (| CAUTION SECNO= | | | CRITICAL DEPTH ASSUMED | A PURBAL | | (|
| | CAUTION SECNO= CAUTION SECNO= CAUTION SECNO= CAUTION SECNO= | 3.475 3.475 | PROFILE= 1 PROFILE= 2 | PROBABLE MINIMUM SPECIFI 20 TRIALS ATTEMPTED TO B CRITICAL DEPTH ASSUMED MINIMUM SPECIFIC ENERGY | | | 1 |
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***************** HECZ RELEASE DATED NOV 76 UPDATED AUG1977 FRROR CORR - 01.02 MODIFICATION - 50,51,52,53 ******************************* T1 CONNECTICUT FLOOD INSURANCE STUDY T2 CITY OF BRIDGEPORT 13 STA. 0.057 TO STA. 3.500 METHOD 1 FLOODWAY PEQUONNOCK RIVER J1 ICHECK INO NINA IDIR STRT METRIC HVINS Q WSEL FQ -0. 8. - () • -0. -0.000000 -0.00 -0.0**-0**. .3.600 -0.000 J2 NPROF. TPLOT PRFVS XSECV XSECH FN ALLDC 18W CHNIM TRACE 15.000 -0.000 -1.000 -0.000 -0.000 -0.000 -0.000 -0.000 -() o () () () ~0.000

| | STATION | WIDTH | SECTION | MEAN VELOCTTY | HTTW YAWOODJA | | DIFFERENCE | · · · · · · · · · · · · · · · · · · · |
|-----------------|----------------|---------------|----------------|------------------|------------------|--|---------------------------------------|---|
| | AET | / C 2 | 1055/ | | 3.7 | 2.7 | | · · · · · · · · · · · · · · · · · · · |
| f | .057 .116 | 652. 418. | 18504. | .5 1.5 | 3.6 3.6 | 3.6 | 0.0 | |
| | • 131 | 418. | 6178. | 1.5 | 3.6 | 3.6 | 0.0 | |
| | | 327. | 7397 | 1.3 | 3.6 | 3.6 | 0.0 | (|
| | .390 | 394 | 4304. | 2.2 | 3.6 | 3.6 | 0.0 | |
| ., | .437 | 401. | 9344. | 1.0 | 3.7 | 3.7 | 0.0 | |
| | .481 | 406. | 4466. | 2.1 | 3.7 | 3.7 | 0.0 | ϵ |
| ş | 498 | 406. | 4420. | ·····2 • 2 ··· | 3.7 | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~ | 0.0 | ************************************** |
| | .573 | 233. | 4569. | 2.1 | 3.7 | 3.7 | 0 . 0 | |
| | 701 | 180. | 2970. | 3.2 | 3.7 | 3.7 | 0.0 | |
| | .711 | 180. | 2385. | 4.0 | 3.7 | 3.7 | 0.0 | |
| | .834 | 239. | 4231. | 2.3 | 4.0 | 4 . 0 | 0.0 | |
| | • 952 | 280. | 3541. | 2.7 | 4.0 | 4.0 | 0.0 | |
| p | .962 | 280. | 3543. | 2.7 | 4.0 | 4.0 | 0 | ************************************** |
| | 1.096 | 252. | 3527. | 2.7 | 4.1 | 4.1 | 0.0 | , |
| | 1.250 | 252. | 2283. | 4.2 | 4.1 | 4.1 | 0.0 | · · · · · · · · · · · · · · · · · · · |
| | 1.319 | 104. | 653. | 14.6 | 4.8 | 4.8 | 0.0 | đ |
| 10,200 | 1.329 | 109 | ·····-853。· | 11.2 | 6 • 8 | 6.8 | 0.0 | t in the second of the second |
| | 1.349 | 78. | 696. | 13.7 | 7.2 | 7.2 | 0 . 0 | · · |
| 11414 1114111 | 1.490 | 165. | 1722. | 5.6 | 10.8 | 10.8 | 0 • 0 | · |
| | 1.583 | 780. | 1977. | 4 . 4 | 13.3 | 13.1 | • 2 | |
| | 1.590 | 1949. | 5205. | 1.7 | 14.6 | 13.2 | 1.4 | |
| | 1.600 | 1949. | 5249. | 1.6 | 14.6 | 13.6 | 1.0 | |
| | 1.604 | 740. | 2645 | 3 . 3 | 14.5 | 14.2 | · · · · · · · · · · · · · · · · · · · | |
| | 1.714 | 901. | 3629. | 2.4 | 15.3 | 14.7 | • 6 | · |
| Service control | 1.732 | 1278. | 4567 | 1.9 | 15.4 | 14.8 | . 6 | |
| | 1.733 | 1278. | 4567. | 1.9 | 15.4 | 14.8 | • 6 | |
| | 1.884 | 1431. | 7037. | 1.2 | 15.8 | 15.4 | • 4 | |
| | 1.885 | 1431. | 7262. | 1.2 | 15.8 | 15.4 | . 4 | |
| | 1.895 | 400. | 2146. | 4.0 | 15.6 | 15.4 | 6.2 | (|
| | 1.960 | 500. | 3266 | 2.6 | 16.4 | 15.5 | . 9 | |
| | 1.979 | 1210. | 6305 | 1.4 | 16.5 | 15.5 | .) | |
| | 1.980 2.057 | 1213. 826. | 6098. 3112. | 1.4 | 16.6 | 15.7 | 6 9 | |
| | 2.058 | 829. | 3708. | 2.8 2.3 | 16.6 16.9 | 15.8 16.2 | • 8 ··· • 7 | |
| | -2.063 | 300 | 2541. | 3.4 | 17.1 | 16.7 | | |
| | 2.141 | 240. | 1495. | 5 , 8 | 17.2 | 16.8 | o 4 o 4 | |
| y | 2.150 | 534. | 1530. | 5.6 | 17.2 | 16.7 | 5 | |
| | 2.157 | 522. | 1732. | 5.0 | 17.8 | 17.4 | . 4 | |
| | 2.161 | 400. | 1082. | . 8.0 | 17.7 | 17.4 | . 3 | |
| | 2.265 | 500. | 2483. | 3.5 | 20.0 | 19.3 | . 7 | |
| | 2.788 | 1-60. | 1916. | 4.5 | 41.7 | 41.7 | 0.0 | |
| | 3.096 | 110. | 914. | 9.4 | 42.3 | 42.4 | - · 1 | |
| į | 3.351 | 110. | 721. | 11.9 | 46.0 | 45.5 | , ŝ | · |
| | 3.475 | 140. | 723. | 11.9 | 51.7 | 51.8 | 1 | |
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| | | | | | | | | |

HEC2 RELEASE DATED NOV 76 UPDATED AUG1977 FRROR CORR - 01,02 MODIFICATION -50,51,52,53STARTING WATER **SURFACE ELEVATION** T1 CONNECTICUT FLOOD INSURANCE STUDY HUD CONTRACT #H-4560 __T2 CITY OF BRIDGEPORT CEM #3027,921 AUGUST 1978 Т3 PEQUONNOCK PIVER STA.O.O57 TO STA. 3.500 10 YEAR BACKWATER J1 ICHECK NINV IDIR TNO STRT WSEL 🛆 FQ METRIC HVINS Q 2. -0. -0. -0. -0.000000 -0.00 -0.0 -0. 3.600 -0.000 J2 NPROF TPLOT PREVS XSECV **XSECH** FN ALLDC IBW CHNIM ITRACE 1.000 -0.000 -0.000 -0.000 -0.000 -0.000 -0.000 -0.000 -1.000-0.000 VARIABLE CODES FOR SUMMARY PRINTOUT 38.000 1.000 43.000 61.000 51.000 50.000 26.000 4.000 3.000 46.000 10.000 11.000 12,000 0.000 39.000 1.000 40.000 41.000 39.000 42.000 33.000 13.000 14.000 15.000 57.000 53.000 54.000 0.000 207.000 83.000 91.000 99.000 104.000 119.000 145.000 181.000 -0.000 -0.000 -0.000 -0.000 .025 -0.000 .030 .030 .300 .600 -0.000 -0.000 -0.000 -0.000 9.000 9560.000 QT 2630.000 6700.000 9560.000 21240.000 9560.000 9560.000 9560.000 9560.000 ΕT -0.000 -0.000 -0.000 -0.000 -0.000 -0.000 10.400 9.100 101.000 1101.000 X 1 .057 17.000 615.000 1270.000 0.000 0.000 0.000 -0.000 -0.000 -0.000 621.000 GR 20.000 365.000 10.000 390.000 10.000 570.000 8.000 615.000 0.000 GR -12.000 670,000 -16.000 765,000 -23.000 790.000 -33.000 890.000 -35.000 1005.000 GR -33.000 1075.000 -30,000 1125.000 -24.0001200.000 -15.0001269,800 0.000 1269,900 1270.000 GR 7.500 22.500 1.290.000 -0.000 -0.000 -0.000 -0.000 -0.000 -0.000 ET -0.000 -0.000 -0.000 -0.000 -0.000 -0.000 -0.000 -0.000 10.600 -0.000 X 1. .116 52.000 743.500 1243.300 250.000 400,000 310.000 -0.000 -0.000 -0.000 Х3 10.000 -0.000 -0.000 -0.000 -0.000 -0.000 -0.000 11.900 11,900 -0.000 GR 743.400 15.300 9.200 743.500 9.000 779.100 10.400 779.600 10.400 784.600 GR 8.700 785.100 7.900 818.800 819.300 11.000 824.700 -1.300824.900 10.400 GR -3.600 845,400 -3.800 859.100 11.400 859,600 11.400 864.600 -4.500 865.100 -4.900 889.400 -16.300897,400 -12.200912.400 11.900 913.400 933.400 GR 11.300 GR -17.000934.500 -25.200 942,500 8.800 942.600 8.800 945,400 -25.200 945.500 -27,900 974.400 1050,500 1050.600 GR -26.200 1000,000 -26.1008.800 8.800 1053.400 -26.100 GR 1053.500 -24.7001058,500 11.300 1059.600 11.900 1079.500 -22.100 1080.600 GR -22.700 1106,400 -11.800 1123.900 11.200 1124.400 11,900 1126.900 -12.1001129.900 GR -5.700 1164.100 11.000 11.000 1169.600 -4.400 1189.400 -2.700 1164.600 1202.800 GR 11.000 1203.300 11,000 1208.300 -2.700 1208,400 <u>~2.600</u> 1229,400 -1.600 1243,200 7.900 GR 1243.300 13.600 1243.400 -0.000 -0.000 -0.000 -0.000 -0.000 -0.000 SB -0.000 1.560 2.600 -0.000 100.000 -0.000 8900.000 5.020 -27.900-27.900

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| í | BT | 3.800 1133.000 | 1089.000 | 22.000 | 13.200 1143.100 | 1102.000 | 21.800 | 14.400 1157.000 | 1121.000 | 21.300 | 10.700 1174.000 | 1 |
|----------------|------------|-------------------|--|-----------------------------------|--------------------|--------------------|--|--|---|---|--|--|
| , | <u> </u> | 19.900 | 12.800 | 1187.000 | 19.400 | 11.800 | 1202.200 | 19.300 | 6.400 | 1265.900 | 19.000 | |
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| (| вТ | 1560.000 | 25.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | · · · · · · · · · · · · · · · · · · · |
| | <u>NC</u> | .035 | . 045 | .025 | .300 | . 500 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | |
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| | X1 | .573 | 19.000 | 884.000 | 1120.000 | 440.000 | 380.000 | 410.000 | -0.000 | -0.000 | -0.000 | |
| Í | GR | 12.800 | 600.000 | 12.500 | 640.000 | 11.000 | 760.000 | 9.000 | 830.000 | 8.500 | 884.000 | · 1 |
| | GR | 0.000 | 885.000 | -10.000 | 895.000 | -18.000 | 925.000 | -20.000 | 1000.000 | -18.000 | 1075.000 | ernet ne rendermen alle 2012 de 2010 El 2000 de 2010 d |
| | GR | -10.000 | 1100.000 | 0.000 | 1110.000 | 5.000 | 1120.000 | 8,500 | 1150.000 | 9.000 | 1220.000 | ϵ |
| (| <u>GR</u> | 8.500 | 1280.000 | 10.500 | 1350.000 | 11.000 | 1380.000 | 22.500 | 1400.000 | -0.000 -0.000 | -0.000 -0.000 | |
| | NC | -0.000 | -0.000 | •030 | • 400 | .700 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | |
| (| | | | | | | | | | | | |
| | X1 | .701 | 28.000 | 851.000 | 1034.000 | 600.000 | 740.000 | 670.000 | -0.000 | -0.000 | -0.000 | |
| | Х3 | 10.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | 9.100 | 9.100 | -0.000 | |
| Ų, | GR | 17.000 | 610,000 | 16.800 | 660.000 | 1.6.000 | 710.000 | 15.000 | 835.000 | 8.300 | 851.000 | |
| | GR | -2.800 | 851.100 | -13.400 | 874.000 | -17.400 | 897.000 | 8.900 | 897.100 | 9.000 9.100 | 904.900 959.900 | |
| ₹ . | GR GR | -15.600 6.600 | 905.000 963.000 | -13.800 6.600 | 929.000 966.000 | -15.300 -18.300 | 952.000 966.100 | 9.100 -19.200 | 952.100 983.000 | -18.700 | 1000.000 | |
| · | GR GR | 5.600 -17.400 | 1014.000 | -13.500 | 1031.000 | 7.500 | 1031.100 | 8.400 | 1034.000 | 14.800 | 1093.000 | |
| | GR | 14.500 | 1200.000 | 15.500 | 1700.000 | 25.000 | 1715.000 | -0.000 | -0.000 | -0.000 | -0.000 | · · · · · · · · · · · · · · · · · · · |
| (| SB | -0.000 | 1,560 | 2.600 | -0.000 | 131.000 | -0.000 | 3900.000 | .920 | -19.200 | -19.200 | (, |
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| ١, | X1 | .711 | ~0.000 | -0.000 | -0.000 9.100 | 70.000 14.500 | 70.000 | 70.000 -0.000 | -0.000 -0.000 | -0.000 -0.000 | -0.000 | |
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| (| | 8.000 | 610.000 | 17.000 | 0.000 | 660.000 | 16.800 | 0.000 | 710.000 | 16.000 | 0.000 | (|
| | BT | 835.000 | 15.000 | 0.000 | 1093.000 | 14.800 | 0.000 | 1200.000 | 14.500 | -0.000 | 1700.000 | |
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| ţ | NC | •035 | .045 | .025 | .300 | • 500 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | 1 |
| | ET | -0.000 | -0.000 | -0.000 | | -0.000 | -0.000 | <u>=0.000</u> | 9.100 | 105.000 | 1105. • 0.00 announce | |
| V · · · | | | | | | | | | | | | Ç |
| l ` | X1 | .834 | 17.000 | 870.000 | 1140.000 | 660.000 | 660.000 | 660.000 | -0.000 | -0.000 | -0.000 | |
| | ĜR | 15.000 | 550.000 | 12.500 | 560.000 | 12.500 | 590.000 | 11.000 | 670.000 | 7,500 | 870,000 | , |
| , | GR | 1.000 | 880.000 | -10.000 | 910.000 | -18.000 | 930.000 | -19.000 | 1000.000 | -18.000 | 1070.000 | (|
| | GR | -10.000 | 1090.000 | 1.000 | 1100.000 | 9.500 | 1140.000 | 10.500 | 1220.000 | 10.500 | 1270.000 | |
| | GR | 11.500 | 1330.000 | 13.500 | 1395.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | (|
| | | | | | | | | | | | | |
| | X 1 | 952 | 55.000 | 817.000 | 1179.600 | 600.000 | 660.000 | 630.000 | -0.000 | -0.000 | -0.000 | |
| · | X3 | 10,000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | 13.000 | 13.000 | -0.000 | (|
| l . | GR_ | 19.000 | 600,000 | 17,000 | 650.000 | 16.500 | 710.000 | 17.800 | 748.000 | 13.000 | 817.000 | |
| | GR | 7.400 | 818.000 | 7.700 | 860.500 | 1.800 | 861.000 | -3.400 | 880.000 | 16.000 | 880.100 | í |
| | GR | -10.200 | 888.100 | -14.500 | 918.000 | <u>-13.900</u> | 937.900 | 8.000 | 938.000 | 8.000 | 941.000 | (|
| | GR | -13.800 | 941.100 | -13.600 | 947.900 | 7.400 | 948.000 | 12.500 | 950.500 962.400 | 16.000 8.400 | 950.600 962.500 | |
| - | GR GR | 14.000 8.400 | 954.000 965.000 | 7.400 -18.200 | 957.400 965.100 | -15.200 -18.600 | 957.500 1000.000 | -18.100 -16.600 | 1022.000 | -16.300 | 1033.400 | (|
| | GR GR | 8.400 | 1033.500 | 8.000 | 1036.000 | -16.300 -16.300 | 1036.100 | -13.100 | 1042.500 | 7.400 | 1042.600 | |
| - | GR | 13.100 | 1045.500 | 15.600 | 1052.300 | -10.400 | 1052.500 | -9.800 | 1059.900 | 6.400 | 1060.000 | - |
| l . | GR | 6.400 | 1062.500 | -9.600 | 1062,600 | -8.600 | 1082.500 | -3,900 | 1111.500 | 16.000 | 1111.600 | (|
| | GR | 16,000 | 1119.400 | -1.200 | 1119.500 | 1.900 | 1135.500 | 6.500 | 1147.500 | 6.500 | 1148.500 | |
| _ | GR | 4.800 | 1152.500 | 5.300 | 1179.500 | 15.200 | 1179.600 | 22.700 | 1179.700 | 22.700 | 1208.000 | |
| | SB | -0.000 | 1.560 | 2.600 | -0.000 | 107.000 | -0.000 | 6290.000 | 3.510 | -18.000 | -18.000 | • |
| •- | | | AND THE RESIDENCE OF THE PROPERTY OF THE PROPE | ·/Acadaminaterraliamental control | | | ermann-selfgrangger in mensis kerenari se pamunes van dinakt dekalisis kalaktis in mengepagan par em | The second secon | 27007-96-746-7-1-7-7-7-7-7-7-7-7-7-7-7-7-7-7-7-7-7- | general processors - service annual service and a service | | |
| | X 1 | .962 | -0.000 | -0.000 | -0.000 | 60.000 | 60.000 | 60.000 | -0.000 | -0.000 | -0.000 | 9[|
|] - | X2 | -0.000 | -0.000 | 1.000 | 17.000 | 16.500 | ~0.000 | -0.000 | -0.000 | -0.000 | -0.000 | • |
| | X3 | 10.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | 16.500 | 22.700 | -0.000 | Í |
| | 87 | 16.000 | 600.000 | 19.000 | 0.000 | 650.000 | 17.000 | 0.000 | 710.000 | 16.500 | 0.000 | 1 |
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| вт | 748.000 | 17.800 | 0.000 | 817.000 | 20.100 | 13.000 | 880.000 | 21.200 | 16.000 | 880.100 | (|
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| n i BT | 1119.400 | 22.800 | 16.000 | 1179.600 | 22.700 | 15.200 | 1208.000 | 22.700 | -0.000 | -0.000 | |
| NC NC | .055 | .030 | .025 | .300 | •500 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | (|
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| 7 | | | | | | | | | | | (|
| ×1 | 1.096 | 19.000 | 875.000 | 1130.000 | 680.000 | 640.000 | 660.000 | -0.000 | -0.000 | -0.000 | |
| GR | 15.000 | 680.000 | 10.000 | 690.000 | 9.000 | 720.000 | 8.500 | 775.000 | 7.500 | 835.000 | , |
| GR | 5.000 | 875.000 | 1.000 | 880.000 | -5.000 | 890,000 | -12.000 | 925.000 | -13.300 | 1000.000 | (|
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| GR | 10.000 | 1170.000 | 10.500 | 1225.000 | 12.000 | 1275.000 | 12.800 | 1330.000 | -0.000 -0.000 | -0.000 -0.000 | ť |
| NC ST | •075 -0•000 | -0.000 | -0.000 | .100 -0.000 | -0.000 | -0.000 -0.000 | -0.000 -0.000 | -0.000 9.100 | 107.000 | 1107.000 | |
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| (| | | A STATE OF THE STA | | | | | | | | (|
| X1 | 1.250 | 10.000 | 867.000 | 1160.000 | 780.000 | 1000.000 | 1000.000 | -0.000 | -0.000 | -0.000 | and the second |
| GR GR | 15.000 | 867.000 | 5.000 | 870.000 | 2.000 | 875.000 | -5.000 | 900.000 | -7.100 15.000 | 1000.000 1160.000 | (|
| GR_NC | -5.000 .050 | 1100,000 .050 | 2.000 .025 | 1120.000 .300 | 5.000 .500 | 1125.000 -0.000 | 10.000 -0.000 | 1135.000 -0.000 | -0.000 | ~0.000 | *************************************** |
| 141, | • 0 50 | • 020 | • 02.7 | 1300 | • 200 | -0.000 | 000 0 | | | | |
| (| | | | | | | | | | | (|
| <u> </u> | 1,319 | 26.000 | 917.500 | 1026.000 | 380,000 | 400.000 | 390.000 | -0.000 | -0.000 | -0.000 | |
| X3 | 10.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | 15.000 | 15.000 5.000 | -0.000 917.600 | (|
| GR CP | 20.000 | 870.000 | 19.500 200 | 880,000 934,000 | 16.100 -2.900 | 914.500 943.500 | 6.500 -4.400 | 917.500 953.000 | -4.500 | 969.500 | |
| GR GR | 2.300 6.500 | 925.500 969.600 | 6.500 | 974.000 | -3.700 -3.700 | 974.100 | -3.300 | 990.500 | -3.600 | 1000.000 | |
| GR. | -1.300 | 1009.500 | 6.700 | 1026.000 | 9.000 | 1045.000 | 10.700 | 1055.000 | 11.300 | 1080.000 | (|
| GR | 15,900 | 1090.000 | 16.500 | 1105.000 | 15.500 | 1150.000 | 15.300 | 1270.000 | 17,000 | 1390.000 | |
| GR | 20.000 | 1500.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | (|
| SB | -0.000 | 1.560 | 2.600 | -0.000 | 44.000 | -0.000 | 1030.000 | 3.310 | -3.700 | -3.700 | · · |
| | | | | | | | | | | | |
| ₹ X1 | 1.329 | -0.000 | -0.000 | -0.000 | 50.000 | 50.000 | 50.000 | -0.000 | -0.000 | -0.000 | (|
| X2 | -0.000 | -0.000 | 1.000 | 9,500 | 15,300 | -0.000 | -0.000 | -0.000 | -0.000 | _0.000 | |
| X3 | 10.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | 16.100 | 15.300 16.100 | -0.000 0.000 | (. |
| ' BT | 22.000 917.500 | 870.000 16.100 | 20.000 6.500 | 0.000 934.000 | 880.000 16.100 | 19.500 9.100 | 0.000 943.500 | 914.500 16.000 | 9.500 | 953.000 | |
| BT BT | 16.000 | 9.100 | 969.600 | 16.000 | 6.500 | 974.000 | 16.000 | 6.500 | 990.600 | 15.900 | |
| 81 | 9,000 | 1000.000 | 15.900 | 9.100 | 1026.000 | 15.900 | 6.700 | 1030.000 | 15.900 | 7.200 | (|
| <u> </u> | 1045.000 | 15.900 | 9.000 | 1055.000 | 15.900 | 10.700 | 1080.000 | 15,900 | 11.300 | 1090.000 | Control of the second control of the second control of the second of the |
| BT | 15.900 | 0.000 | 1105.000 | 16.500 | 0.000 | 1150.000 | 15.500 | 0.000 | 1270.000 | 15.300 | (|
| ' BT | 70.000 | 1390.000 | 17.000 | 0.000 | 1500.000 | 20.000 | -0.000 -0.000 | -0.000 -0.000 | -0.000 -0.000 | -0.000 -0.000 | |
| NC ET | .045 -0.000 | •040 •0•000 | . •035 -0•000 | .600 -0.000 | .800 -0.000 | -0.000 -0.000 | -0.000 | 9.100 | 108.000 | 1108.000 | |
| <u> </u> | _ U 6 U U | -0.000 | -0.000 | | 7,000 | | 0,000 | | | | (|
| for terroring and the second | | aasamuur on onun uu ammuus an mousean an onun on al annon onun lähinin on alikkilli (1800–1806) killi (1800–1800) | | NO SOUTH OF THE PROPERTY OF | | | greg se sermon de de monte en como con el distinció del 11 de 2000 de 10 gregorio de 10 gregorio de 10 de concesta en con esta el como con esta en con esta | a desiren kiri di Sila di Sila di Sila di Sila di Sila di Sila di Sila di Sila di Sila di Sila di Sila di Sila | | | er menne kilologia (1806-1807) i statutu ilmaatata ya qaragan ee ee ee ee ee ee ee ee ee ee ah ah ah ah ah ah ah ah ah ah ah ah ah |
| X 1 | 1.349 | 11.000 | 962.000 | 1055.000 | 130.000 | 130.000 | 130.000 | -0.000 | -0.000 | -0.000 | (|
| <u>GR</u> | 15.000 | 962.000 | 5.000 | 965.000 | 2.000 | 970.000 | -3.500 10.000 | 975.000 1045.000 | -4.400 15.500 | 1000.000 1055.000 | , |
| GR GR | -3.500 17.000 | 1025.000 1425.000 | 2.000 -0.000 | 1030.000 | 5.000 ⊶0.000 | 1040.000 -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | |
| NC | -0.000 | =0.000 | -0.000 | •100 | •300 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | (|
| NH | 5,000 | .055 | 925,000 | ,030 | 1070.000 | 075 | 1095.000 | 025 | 1700.000 | . 04 0 | THE STATE OF THE ASSESSMENT OF |
| ИН | 2550.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | i l |
| ET | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | 9.100 | 109.000 | 1109.000 | , |
| | | | | | | | | | | | |
| | | | | | | | | | | 0.000 | |
| X 1 | 1,490 | 19,000 | 910.000 | 1075.000 | 800.000 | 670.000 | 740.000 | -0.000 | -0.000 | -0.000 | ` |
| X1 | 1.490 20.000 | 19.000 900.000 | 910.000 10.000 | 1075.000 910.000 | 800.000 5.000 | 670.000 925.000 | 740.000 | 940,000 | -3,000 | 980.000 | |
| | 20.000 -3.500 | 900,000 | 10.000 -3.000 | 910,000 1020,000 | 5.000 2.000 | 925.000 1060.000 | 2.000 5.000 | 940,000 1070.000 | -3.000 9.800 | 980.000 1075.000 | ************************************** |
| | 20.000 -3.500 9.500 | 900.000 1000.000 1140.000 | 10.000 -3.000 10.500 | 910.000 1020.000 1180.000 | 5.000 2.000 11.500 | 925.000 1060.000 1300.000 | 2.000 5.000 12.000 | 940.000 1070.000 1435.000 | -3.000 9.800 14.300 | 980.000 1075.000 1550.000 | \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ |
| | 20.000 -3.500 9.500 10.500 | 900,000 1000,000 1140,000 1700,000 | 10.000 -3.000 10.500 12.000 | 910.000 1020.000 1180.000 1920.000 | 5.000 2.000 11.500 15.000 | 925.000 1060.000 1300.000 2020.000 | 2.000 5.000 12.000 20.000 | 940.000 1070.000 1435.000 2170.000 | -3.000 9.800 14.300 -0.000 | 980.000 1075.000 1550.000 -0.000 | √ (|
| | 20.000 -3.500 9.500 | 900.000 1000.000 1140.000 | 10.000 -3.000 10.500 | 910.000 1020.000 1180.000 | 5.000 2.000 11.500 | 925.000 1060.000 1300.000 | 2.000 5.000 12.000 | 940.000 1070.000 1435.000 | -3.000 9.800 14.300 | 980.000 1075.000 1550.000 | 0 0 |

| Ć | ET | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | 9.100 | 110.000 | 1110.000 | <u> </u> |
|------------|-----------|-----------------|------------------|-----------------|------------------|---------------|----------|----------|--------------|------------------|--|--|
| | X1 | 1.583 | 17.000 | 985.000 | 1017.000 | 480.000 | 540.000 | 510.000 | -0.000 | -0.000 | -0.000 | |
| (| GR | 20.000 | 750.000 | 15.000 | 950.000 | 12.500 | 960.000 | 10.000 | 970.000 | 5.000 | 980.000 | . (|
| | GR | 2,500 | 985.000 | -3.000 | 988,000 | -2.800 | 1000.000 | | 1010.000 | 2.500 | 1015.000 | |
| é . | GR | 5.000 | 1025.000 | 10.000 | 1030.000 | 12.000 | 1220.000 | 11.500 | 1700.000 | 11.500 | 2100.000 | (|
| ί | G.R. | 15.000 | 2190.000 | 20.000 | 2340.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 -0.000 | |
| , | NC | -0.000 | •060 | .025 | .300 | • 500 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | |
| (| <u> </u> | 1.590 | 30.000 | 972.000 | 1018,100 | 40.000 | 70.000 | 60.000 | 0.000 | -0.000 | -0.000 | |
| | X3 | 10.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | 8.800 | 10.000 | -0.000 | , |
| (| GP | 25,000 | 460.000 | 24.000 | 500.000 | 20.000 | 740.000 | 18.000 | 800.000 | 17.000 | 930.000 | (|
| | GR | 16.300 | 952.000 | 16.600 | 969.000 | 10.000 | 972.000 | • 900 | 972.100 | -1.300 | 1000.000 | |
| - | <u>GR</u> | -2.500 | 1010.000 | -2.900 | 1018.000 | 8,800 | 1018.100 | 15.300 | 1022.000 | 14.100 | 1042.000 | |
| • | GR | 13.000 | 1120.000 | 13.500 | 1180.000 | 12.300 | 1250.000 | 10.500 | 1305.000 | 11.000 | 1370.000 | |
| • | <u>GR</u> | 10.800 | 1430.000 | 12.300 | 1730.000 | 12.800 | 1860.000 | 12,500 | 2100.000 | 12.500 25.000 | 2430.000 2970.000 | gyanamin'nimeng-naminananananananananananananananananana |
| (| GR | 11.300 | 2670.000 | 12.000 | 2770.000 | 15.000 | 2940.000 | 20,000 | 2950.000 | -1.300 | <u>-1.300</u> | (|
| , <u>-</u> | \$B | -0.000 | 1.560 | 3.000 | -0.000 | 41.000 | -0.000 | 470.000 | | | -1.000 | |
| (· - | X1 | 1 600 | =0.000 | -A AAA | _^ ^^ | 50.000 | 50.000 | 50.000 | -0.000 | -0.000 | -0.000 | |
| • | X 1. | 1.600 -0.000 | -0.000 -0.000 | -0.000 1.000 | -0.000 10.000 | 10.500 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | |
| | X3 | 10.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | 16.300 | 10.500 | -0.000 | and the second s |
| (| B.T | 23,000 | 930.000 | 17.000 | 0.000 | 952.000 | 16.300 | 0.000 | 969.000 | 16.600_ | 0.000 | (|
| _ | BT | 969.100 | 20.100 | 0.000 | 972.000 | 19.900 | 10.000 | 1018.100 | 19.000 | 8.800 | 1021.900 | |
| | 81 | 18.800 | 0.000 | 1022.000 | 15.300 | 0.000 | 1042.000 | 14.100 | 0.000 | 1120.000 | 13.000 | |
| ₹. | ВT | 0.000 | 1180.000 | 13.500 | 0.000 | 1250.000 | 12.300 | 0.000 | 1305.000 | 10.500 | 0.000 | (|
| | BT | 1370,000 | 11.000 | 0.000 | 1430.000 | 10.800 | 0.000 | 1730.000 | 12.300 | 0.000 | 1860.000 | |
| | 8 T | 12.800 | 0.000 | 2100.000 | 12,500 | 0.000 | 2430.000 | 12.500 | 0.000 | 2670.000 | 11.300 | 1 |
| (| BT | 0.000 | 2770.000 | 12.000 | 0.000 | 2940.000 | 15.000 | 0.000 | 3020.000 | 18.000 | -0.000 | |
| | NC | .065 | .075 | .030 | • 300 | • 500 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | |
| , - | ET | -0.000 | -0.000 | -0.000 | ~0.000 | <u>~0.000</u> | -0.000 | -0.000 | 9.100 | 111.000 | 1111.000 | |
| (| | | | | | | 1,00 | | | | CONTRACTOR OF THE CONTRACTOR O | |
| | X1 | 1.604 | 24.000 | 960.000 | 1055.000 | 20.000 | 20.000 | 20.000 | -0.000 | -0.000 | -0.000 | |
| | GR | 25.000 | 670.000 | 23,500 | 730.000 | 20.000 | 890.000 | 18.000 | 900.000 | 16.000 | 940.000 | (. |
| | GR | 15.000 | 960.000 | 5.000 | 970.000 | 2.500 | 975.000 | -1.500 | 980.000 | -2.800 | 1000.000 | |
| _ | GR | -1.500 | 1020.000 | 2.500 | 1025.000 | 5.000 | 1030.000 | 10.000 | 1040,000 | 13.500 | 1055.000 | (|
| ŧ | GR | 14.300 | 1090.000 | 14.300 | 1130.000 | 11.000 | 1300.000 | 11.700 | 1560.000 | 12.300 | 2400.000 | (|
| _ | GR | 12,000 | 2740.000 | 15.000 | 2880.000 | 18.000 | 2950.000 | 25.000 | 2970.000 | -0.000 | | |
| - | NC | -0.000 | -0.000 | -0.000 | .100 | •300 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | í |
| | NH | 4.000 | .045 | 960.000 | .035 | 1040.000 | .015 | 1165.000 | .050 | 2570.000 | -0.000 | (|
| _ | ET | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | 9.100 | 112.000 | 1112.000 | |
| | X 1 | 1.714 | 25.000 | 950.000 | 1040,000 | 610,000 | 610.000 | 610.000 | -0.000 | -0.000 | -0.000 | |
| | GR | 25.000 | 790.000 | 20.000 | 900.000 | 19.000 | 910.000 | 18.000 | 950.000 | 15.000 | 960.000 | |
| | GR | 5.000 | 970.000 | 4.000 | 980.000 | 1.600 | 1000.000 | 4.000 | 1020.000 | 5.000 | 1025.000 | <u> </u> |
| - | GR | 10.000 | 1035.000 | 14.000 | 1040.000 | 13.000 | 1075.000 | 13.000 | 1125.000 | 12.500 | 1165.000 | · |
| | GR | 11.200 | 1300.000 | 12.500 | 1490.000 | 13.500 | 1640.000 | 12.000 | 1765.000 | 11.000 | 1900.000 | |
| | GR | 15.000 | 2220.000 | 18,000 | 2350.000 | 19.000 | 2570.000 | 20.500 | 2770.000 | 25.000 | 3190.000 | |
| | NC | .065 | .050 | •030 | •100 | .300 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | |
| | | | | | | | | | | | | (|
| | X 1 | 1.732 | 29.000 | 961.000 | 1037.000 | 150.000 | 80.000 | 110.000 | -0.000 | -0.000 | -0.000 | |
| | X 3 | 10.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | 11.300 | 11.300 | -0.000 | |
| | GR | 25.000 | 790.000 | 22.800 | 825.000 | 15.000 | 940.000 | 11.300 | 961.000 | 2,200 | 962.000 | (|
| Wash | GR | ,300 | 972.000 | • 800 | 986.000 | 1.900 | 1000,000 | 11.300 | 1000.010 | 11.300 | 1001.000 | ago anno ago ago ago ago ago ago ago ago ago ag |
| | GR | 1.900 | 1001.010 | .700 | 1014.000 | 1.400 | 1026,000 | 3.300 | 1036.000 | 11.300 | 1037.000 | × 5 |
| | GR | 14.000 | 1065,000 | 12,500 | 1220,000 | 12.000 | 1370.000 | 12.500 | 1500,000 | 13.500 | 1630.000 | |
| | GR | 11.500 | 1800.000 | 11.000 | 1880.000 | 12.300 | 2130.000 | 15.000 | 2200.000 | 18.000 | 2300.000 | · I |
| _ | GR | 18.000 | 2465.000 | 19.000 | 2560,000 | 20.500 | 2770.000 | 25,000 | 3190.000 | <u>-0.000</u> | -0.000 | |
| | | | | | | | | | | | | · |

| (,, | 1 700 | 2 222 | | | | 4 - 2 - 2 - 2 | • • • • | | | | (| , |
|---|---|--|---|--|--|---------------------------------|---|--|---|--|---|--|
| / <u>X1</u> X2 | 1.733 -0.000 | -0.000 -0.000 | -0.000 -0.000 | -0.000 11.300 | 1,000 | 1.000 | 1.000 | -0.000 | -0.000 | -0.000 | | |
| BT | 18.000 | 790.000 | 25.000 | 0.000 | 11.000 825.000 | -0.000 22.800 | -0.000 0.000 | -0.000 940.000 | -0.000 | -0.000 0.000 | | |
| (BI | 961.000 | 14.300 | 11.300 | 970.000 | 14.000 | 11.300 | 1025.000 | 13.500 | 15.000 11.300 | 1037.000 | (| į. |
| <u> 8 T</u> | 13.600 | 11.300 | 1065.000 | 14.000 | 0.000 | 1220.000 | 12.500 | 0.000 | 1370.000 | 12,000 | | |
| 87 | 0.000 | 1500.000 | 12.500 | 0.000 | 1630.000 | 13.500 | 0.000 | 1800.000 | 11.500 | 0.000 | villadett i ser Viller i 18 Standisch Stadisch i senind i destabilistica villadet neverlikus Stadisch i deut erhandisch 1800 delibber 🐧 | |
| · <u> </u> | 1880.000 | 11.000 | 0.000 | 2130.000 | 12.300 | 0.000 | 2200.000 | 15.000 | 0.000 | 2300.000 | ſ | |
| ВТ | 18.000 | 0.000 | 2465.000 | 18.000 | 0.000 | 2560.000 | 19.000 | 0.000 | 2770.000 | 20.500 | | |
| 8 T | 0.000 | 3190.000 | 25.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | | |
| NC NC | -0.000 | -0.000 | -0.000 | •500 | •700 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | | |
| . 14 | | 3,700 | 0.000 | *** | *.00 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | | |
| | | 2.770.000 (1940.00) | | | ter en en en en en en en en en en en en en | | | | | | • | |
| (<u>X1</u> | 1.884 | 31,000 | 959,400 | 1041.000 | 800,000 | 800.000 | 800,000 | -0.000 | -0.000 | -0.000 | į | |
| X2 | -0.000 | -0.000 | -0.000 | 1200.000 | 8.800 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | | |
| <u>8 T</u> | 21.000 | 0.000 | 25.000 | 0.000 | 60.000 | 20.000 | 0.000 | 90.000 | 15.000 | 0.000 | | |
| BT | 200.000 | 10.000 | 0.000 | 580.000 | 8.800 | 0.000 | 670.000 | 9.500 | 0.000 | 730.000 | (| |
| RŢ | 10.500 | 0.000 | 840.000 | 10.500 | 0.000 | 930.000 | 11,500 | 0.000 | 957.000 | 14.200 | | |
| 81 | 12.000 | 941.000 | 14.200 | 12.000 | 1050.000 | 12.500 | 0.000 | 1100.000 | 13.000 | 0.000 | | |
| BT | 1150.000 | 12.500 | 0.000 | 1400.000 | 12,300 | 0.000 | 1470.000 | 15.000 | 0.000 | 1640.000 | (| } |
| вт | 18.000 | 0.000 | 1720.000 | 18,000 | 0.000 | 1730.000 | 20.000 | 0.000 | 2100.000 | 20.000 | | |
| <u> </u> | 0.000 | 2170.000 | 25.000 | -0.000 | -0.000 | -0.000 | -0,000 | -0.000 | -0.000 | -0.000 | | |
| GR | 25.000 | 0.000 | 20.000 | 60.000 | 15.000 | 90.000 | 10.000 | 200.000 | 8.800 | 580.000 | (| |
| GR | 9.500 | 670.000 | 10,500 | 730,000 | 10.500 | 840.000 | 11.500 | 930.000 | 11.700 | 957.000 | | |
| GR | 12.000 | 959.400 | 6.400 | 959.500 | 2.100 | 986.000 | 2.400 | 1000.000 | 12.000 | 1000.010 | ý | e . |
| (GR | 11.900 | 1001.000 | 2.400 | 1001.010 | 2,600 | 1015.000 | 4.100 | 1038.000 | 6.000 | 1040.000 | (| |
| GR | 12.000 | 1041.000 | 12.500 | 1050.000 | 13.000 | 1100.000 | 12.500 | 1150.000 | 12.300 | 1400.000 | | l |
| <u> </u> | 15.000 | 1470.000 | 18.000 | 1640.000 | 18.000 | 1720.000 | 20.000 | 1730.000 | 20,000 | 2100.000 | | |
| ' GR | 25.000 | 2170.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | (| |
| | A SAME AND A SAME AS A SAME A SAME AS A SAME | NAME OF THE PROPERTY OF THE PR | Probamana di barana di dilipone, mana arrappe, apagoy antana y mana di mana di mana di mana di mana di mana di | ************************************** | Z . V . VONDEMN CARAM NEXT COLOR | | WHE WANTED TO THE WATER TO THE | 7/X2/X4 | | | | |
| | | | | | | | | | | | (| |
| <u> X1</u> | 1.885 | ~0.000 | -0.000 | -0.000 | 1.000 | 1.000 | 1.000 | -0.000 | -0.000 | -0.000 | | İ |
| ET | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | 9.100 | 113.000 | 1113.000 | | |
| | | | | | | | | | | | <u> </u> | |
| V1 | 1.895 | 30.000 | 976.000 | 1031.000 | 60 000 | 40 000 | <u> </u> | -0.000 | -0 000 | -0 AAA | , | |
| GR | | | | | 60.000 15.000 | 60.000 | 60.000 | -0.000 | -0.000 | -0.000 | | |
| GR GR | 25.000 9.800 | 0.000 240.000 | 20.000 | 90.000 | • | 110.000 | 11.000 | 190.000 | 10.000 | 210.000 | t | |
| GR | 8.800 | 590.000 | 9.800 9.300 | 380.000 640.000 | 9.500 9.500 | 430.000 680.000 | 8.500 | 490.000 700.000 | 9,000 | 545.000 920.000 | | |
| GR | 11.000 | 976.000 | 4.500 | 977.000 | 2.500 | 980.000 | 10.000 2.000 | 1000.000 | 10.500 2.500 | 1020.000 | | |
| GR | 4.500 | 1025.000 | 10.000 | 1030.000 | 12.000 | 1031.000 | 13.000 | 1080.000 | 11.000 | 1270.000 | ······································ | |
| GR | 15.000 | 1420.000 | 18.000 | 1580.000 | 20.000 | 1650.000 | 20.000 | 2040.000 | 25.000 | 2080.000 | | |
| NC | -0.000 | -0.000 | -0.000 | • 100 | • 300 | -0.000 | -0.000 | - 0 • 0 0 0 | -0 • 000 | -0.000 | ************************************** | |
| NH NH | 5.000 | .050 | 705.000 | •025 | 860.000 | • 050 | 980.000 | •035 | 1060.000 | .050 | (| |
| NH | 1480.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | | |
| ET | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | 9.100 | 114.000 | 1114.000 | | 1 |
| | _ * × × × . | | | | | | | - + 3 0 0 | 2 m . 1 0 0 0 | | (| |
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| GR | 11.300 | 1230.000 | 11.300 | 1280.000 | 13.500 | 1330.000 | 18.000 | 1410.000 | 20.000 | 1480.000 | | |
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| X1 | 2.141 | 22.000 | 960.000 | 1030.000 | 420.000 | 420.000 | 420.000 | -0.000 | -0.000 | -0.000 | · |
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| SB | -0.000 | 1.560 | 2.600 | -0.000 | 63,000 | -0.000 | 400.000 | .793 | 7.700 | 7.700 | 1.000-000-000-000-000-00-00-00-00-00-00-0 |
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| BT | 951.800 | 18.500 | 0.000 | 953.000 | 23.400 | 0.000 | 965.000 | 23,600 | 0.000 | 965.400 | |
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| X5 | 4.000 | 37.750 | 40.250 | 41.700 | 45.450 | -0.000 | -0.000 | -0.000 | -0.000 | -0.000 | |
| GR | 58.500 | 832.000 | 36.800 | 890.000 | 35.000 | 897.000 | 31.500 | 911.000 | 29.400 | 919.000 | |
| GR | 28.000 | 940.000 | 28.000 | 971.000 | 25.100 | 1000.000 | 29.600 | 1022.000 | 30.800 | 1029.000 | (|
| GR | 33.400 | 1039.000 | 35.000 | 1040.000 | 40.100 | 1046.000 | 42.500 | 1075.000 | 45.000 | 1085.000 | |
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| GR | 55.000 | 390.000 | 52.000 | 420.000 | 50.000 | 450.000 | 48.500 | 470.000 | 48.000 | 525.000 | 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 |
| GR CR | 45.200 | 575.000 | 46.600 | 645.000 | 46.000 | 710.000 | 48.000 | 785.000 | 45.000 | 860.000 | |
| GR | 44.600 | 875.000 | 43.500 | 940.000 | 40.000 | 965.000 | 38.500 | 970.000 | 38.000 | 1000.000 | |
| <u>GR</u> | 38,500 55,000 | 1030.000 | 40.000 | 1035.000 | 41.500 | 1050.000 | 45,000 | 1100.000 | 50.000 | 1105.000 | |
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| X1 | 3,475 | 13.000 | 975.000 | 1050,000 | 640.000 | 680,000 | 660 000 | -0.000 | A A | A | (|
| GP | 55.000 | 840.000 | 52.500 | 865.000 | 50.000 | 890.000 | 660.000 | -0.000 | -0.000 | -0.000 | |
| GR | 49.000 | 975.000 | 45.000 | 980,000 | 41.000 | 985.000 | 49.000 41.000 | 920.000 | 49.500 | 945.000 | , |
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| | THE COLUMN ASSESSMENT OF THE COLUMN ASSESSMENT | AMILE COMPANY AND AND AND AND AND AND AND AND AND AND | | 2012H72U127H77 | | | | OPPO THE THE REAL PROPERTY OF THE STATE OF T | о до применения на применения на применения на применения на применения на применения на применения на примене На применения на применени | allere hall (1) (1) (1) (1) (1) (1) (1) (1) (1) (1) | and additional to the second of the second o |
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HEC2 RELEASE DATED NOV 76 UPDATED AUG1977

FREDR CORR - 01.02

MODIFICATION - 50,51,52,53

NOTE- ASTERISK (*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

PEOUONNOCK RIVER

BACKWATER

SUMMARY PRINTOUT

| (| SECNO | CWSEL | Q | DIFEG | DIFWSX | OIFWSP | VCH | TOPWID | EG | QWEIR | н۷ | HL | OL OS S |
|---------------|-------|-------|----------|-------|--------|--------------|------|--------|------|-------|-------|-------|---------|
| | .057 | 3.60 | 2630.00 | 0.00 | 0.00 | 0.00 | •14 | 651.65 | 3.60 | 0.00 | .00 | 0.00 | 0.00 |
| $-\Lambda$ | .057 | 3.60 | 6700.00 | • 00 | 0.00 | 0.00 | .36 | 651.65 | 3.60 | 0.00 | • 00 | 0.00 | 0.00 |
| A | .057 | 3.60 | 9560.00 | • 00 | 0.00 | 0.00 | • 52 | 651.65 | 3.60 | 0.00 | •00 | 0.00 | 0.00 |
| | •057 | 3.60 | 21240.00 | .02 | 0.00 | 0.00 | 1.15 | 651.65 | 3,62 | 0.00 | | 0.00 | 0.00 |
| | .116 | 3.60 | 2630.00 | 0.00 | 00 | 0.00 | •43 | 342.46 | 3.60 | 0.00 | • 0 0 | • 00 | • 00 |
| | •116 | 3.59 | 6700.00 | • 01 | 01 | 00 | 1.08 | 342.46 | 3.61 | 0.00 | • 02 | • 00 | •01 |
| | •116 | 3.59 | 9560.00 | • 02 | 01 | 01 | 1.55 | 342.45 | 3,63 | 0.00 | • 04 | • 00 | .02 |
| | .116 | 3,54 | 21240.00 | •12 | 06 | 05 | 3,45 | 342.36 | 3.72 | 0.00 | • 18 | •01 | .10 |
| | .131 | 3.60 | 2630.00 | 0.00 | • 00 | 0.00 | • 43 | 342.46 | 3.60 | 0.00 | • 00 | • 00 | • 00 |
| | .131 | 3.60 | 6700.00 | .01 | • 00 | ()() | 1.08 | 342.45 | 3.61 | 0.00 | • 02 | • 00 | • 00 |
| | .131 | 3.59 | 9560.00 | • 03 | • 00 | 00 | 1.55 | 342.44 | 3.63 | 0.00 | • 04 | •00 | •00 |
| | •131 | 3.56 | 21240.00 | • 14 | • 02 | 03 | 3,45 | 342.37 | 3,74 | 0.00 | •18 | •02 | • 00 |
| | .257 | 3.60 | 2630.00 | 0.00 | • 00 | 0.00 | .36 | 327.21 | 3.60 | 0.00 | • 00 | | • 0.0 |
| ~~ | .257 | 3.61 | 6700.00 | •02 | • 01 | •01 | •91 | 327.29 | 3.62 | 0.00 | •01 | .01 | •00 |
| \mathcal{H} | .257 | 3.61 | 9560.00 | .04 | .02 | .01 | 1.29 | 327.38 | 3.64 | 0.00 | .03 | .01 | .00 |
| | .257 | | 21240.00 | •20 | •12 | •06 | 2.87 | 327.75 | 3.80 | 0.00 | •13 | .05 | .01 |
| | • 390 | 3.60 | 2630.00 | 0.00 | 00 | 0.00 | • 70 | 338.91 | 3.61 | 0.00 | •01 | •00 | •00 |
| | 390 | 3.60 | 6700.00 | .04 | 00 | • 00 | 1.79 | 338.95 | 3.64 | 0.00 | | | |
| | .390 | 3.61 | 9560.00 | .08 | 01 | • 00 | 2.55 | 338.93 | 3.69 | 0.00 | • 0 8 | .01 | •03 |
| | .390 | | 21240.00 | . 43 | 04 | .03 | 5,66 | 339.10 | 4.04 | 0.00 | • 40 | • 0 7 | •17 |
| | •437 | 3.61 | 2630.00 | 0.00 | • 01 | 0.00 | • 28 | 400.81 | 3.61 | 0.00 | .00 | • 00 | • 00 |
| | .437 | 3.64 | 6700.00 | .04 | •04 | •03 | •72 | 400.82 | 3.65 | 0.00 | •01 | • 00 | •00 |
| | 437 | 3.68 | 9560.00 | .09 | . 08 | .04 | 1.02 | 400.83 | 3.70 | 0.00 | | | |
| Come . | .437 | | 21240.00 | • 48 | • 37 | • 32 | 2.24 | 400.91 | 4.08 | 0.00 | .08 | •01 | •03 |
| | .481 | 3.61 | 2630.00 | 0.00 | 00 | 0.00 | •59 | 342.35 | 3.61 | 0.00 | • 01 | • 00 | •00 |
| | .481 | 3.63 | 6700.00 | •06 | - 01 | .03 | 1.50 | 342.35 | 3.67 | 0.00 | .04 | • 00 | .02 |
| | .481 | 3.67 | 9560.00 | .13 | 01 | • 03 | 2.14 | 342.35 | 3.74 | 0.00 | .07 | • 00 | .04 |
| / | .481 | | 21240.00 | .67 | - 06 | | 4.66 | 343.02 | 4.28 | 0.00 | .34 | .01 | .18 |
| | .498 | 3.61 | 2630.00 | 0.00 | •00 | 0.00 | • 60 | 342.35 | 3.61 | 0.00 | .01 | • 00 | • 0 0 |
| | .498 | 3.64 | 6700.00 | •06 | .00 | .03 | 1.52 | 342.35 | 3.67 | 0.00 | • 04 | • 00 | •00 |
| | 498 | 3.67 | 9560.00 | .14 | .01 | .04 | 2.16 | 342.35 | 3.75 | 0.00 | .07 | .01 | .00 |
| | .498 | | 21240.00 | .70 | •03 | . 29 | 4.73 | 343.15 | 4.32 | 0.00 | • 35 | •03 | .01 |

| SECNO | CWSFL | Q | DIFEG | DIFWSX | DIFWSP | VCH | TOPWID | E G | QWEIR | HV | HL | 01.088 |
|----------------|-------|----------------|------------|-------------|--------|-------|--------|--------|---------|-------|----------|--|
| .573 | 3.61 | 2630.00 | 0.00 | • 00 | 0,00 | .58 | 232.64 | 3.61 | 0.00 | .01 | •00 | •00 |
| .573 | 3.65 | 6700.00 | .07 | .01 | • 04 | 1.47 | 232.74 | 3.68 | 0.00 | .03 | • 01 | •00 |
| 573 | 3.70 | 9560,00 | .15 | .02 | .05 | 2.09 | 232.85 | 3.77 | 0.00 | | | • 00 |
| •573 | 4.08 | 21240.00 | .79 | •11 | • 38 | 4.56 | 233.65 | 4.41 | 0.00 | •32 | • 08 | .01 |
| • 701 | 3.61 | 2630.00 | 0.00 | .00 | 0.00 | .89 | 158.26 | 3.62 | 0.00 | •01 | • 00 | • 00 |
| | 3.65 | 6700.00 | .11 | .00 | • 04 | 2.26 | 158.26 | 3.73 | 0.00 | .08 | -02 | .03 |
| •701 | 3.71 | 9560.00 | . 25 | •01 | • 05 | 3.22 | 158.27 | 3.87 | 0.00 | •16 | •04 | •06 |
| • 701 | 4.12 | 21240.00 | 1.26 | .03 | . 41 | 7.00 | 158.28 | 4.88 | 0.00 | . 76 | •16 | |
| .711 | 3.61 | 2630.00 | 0.00 | 00 | 0.00 | 1.10 | 158.26 | 3.63 | 0.00 | • 02 | .00 | •00 |
| .711 | 3.65 | 6700.00 | •15 | 00 | • 04 | 2.81 | 158.26 | 3.77 | 0.00 | •12 | • 01 | • 0 3 |
| .711 | 3.70 | 9560.00 | • 3.2 | <u>~•01</u> | • 05 | 4.01 | 158.27 | 3.95 | 0.00 | .25 | . 02 | .06 |
| .711 | 4.07 | 21240.00 | 1.68 | 04 | •37 | 8.91 | 158.28 | 5.31 | 0.00 | 1.23 | .10 | • 33 |
| | 3.63 | 2630.00 | 0.00 | • 02 | 0.00 | •63 | 236.41 | 3.63 | 0.00 | .01 | .00 | •00 |
| .834 | 3.79 | 6700.00 | .19 | .14 | .16 | 1.60 | 237.38 | 3.83 | 0.00 | • 04 | .03 | • 02 |
| .834 | 3.98 | 9560.00 | . 42 | •28 | •19 | 2.26 | 238,56 | 4.06 | 0.00 | • 08 | •06 | • 05 |
| .834 | 5,48 | 21240.00 | 2.18 | 1.41 | 1.50 | 4.62 | 248.00 | 5.82 | 0.00 | .33 | • 24 | •27 |
| .952 | 3.63 | 2630.00 | 0.00 | •00 | 0.00 | •76 | 237.53 | 3,64 | 0.00 | | | •00 |
| •952 | 3,80 | 6700.00 | .21 | .01 | •17 | 1.92 | 238.02 | 3 + 85 | 0.00 | • 06 | • 02 | .01 |
| • 952 | 4.00 | 9560.00 | .47 | .02 | .20 | 2.70 | 238.64 | 4.11 | 0.00 | .11 | .04 | .02 |
| .952 | 5.58 | 21240.00 | 2.39 | •09 | 1.58 | 5.40 | 272.32 | 6.03 | 0.00 | • 45 | •15 | • 06 |
| .962 | 3.63 | 2630.00 | 0.00 | • 00 | 0.00 | • 76 | 237.51 | 3.64 | 0.00 | .01 | •00 | •00 |
| . 962 | 3.80 | 6700.00 | | .00 | | 1.92 | 238.03 | 3 • 86 | 0.00 | | | |
| •962 | 4.01 | 9560.00 | 4 8 | •01 | •21 | 2.70 | 238.67 | 4.12 | 0.00 | •11 | .01 | • 00 |
| .962 | 5.62 | 21240.00 | 2.43 | • 04 | 1.61 | 5.38 | 272.53 | 6.07 | 0.00 | . 45 | .04 | .00 |
| 1.096 | 3.64 | 2630.00 | 0.00 | • 00 | 0,00 | .77 | 249.90 | 3.65 | 0.00 | •01 | • 01 | •00 |
| 1.096 | 3.83 | 6700.00 | • 25 | .03 | • 20 | 1.93 | 250.66 | 3.89 | 0.00 | •06 | • 03 | •00 |
| 1.096 | 4.07 | 9560.00 | .54 | .06 | . 24 | 2.71 | 251.52 | 4.18 | 0.00 | | | |
| 1.096 | 5.85 | 21240.00 | 2.64 | • 23 | 1.78 | 5.34 | 273.24 | 6.29 | 0.00 | . 44 | • 22. | •00 |
| 1.250 | 3.64 | 2630.00 | 0.00 | • 00 | 0.00 | 1.21 | 250.48 | 3.66 | 0.00 | •02 | •01 | •00 |
| 1.250 | 3,83 | <u>6700.00</u> | • 32 | • 00 | • 20 | 3.01 | 251.11 | 3.98 | 0.00 | •] 4 | •06 | .02 |
| 7 1.250 | 4.07 | 9560.00 | •69 | • 00 | . 24 | 4.19 | 251.92 | 4.35 | 0.00 | • 27 | •11 | • 05 |
| 1.250 | 5.87 | 21240.00 | 3,14 | • 02 | 1.79 | | 256.99 | 6 8.0 | | | | омномическу уческого под мерен на предоступноступноступноступноступноступноступноступноступноступноступноступн |
| 1.319 | 3.48 | 2630.00 | 0.00 | 15 | 0.00 | 4,96 | 92.87 | 3.87 | 0.00 | •38 | • 03 | .18 |
| 1.319 | 3.16 | 6700.00 | 2.08 | - • 68 | 33 | 13.40 | 91.23 | 5.94 | 0.00 | 2.79 | . 17 | 1.32 |
| 1,319 | 4.76 | 9560.00 | 4.22 | <u>, 69</u> | 1.060 | 14.64 | 99,27 | 8.09 | 0.00 | 3.33 | .29 | 1.53 |
| 1.319 | 9.39 | 21240.00 | 10.88 | 3.52 | 4.62 | 18.58 | 108.50 | 14.75 | 0.00 | 5.36 | •63 | 2.21 |
| 1.329 | 3.54 | 2630.00 | 0.00 | .05 | 0.00 | 4.91 | 93.18 | 3.91 | 0.00 | .37 | • 0 4 | • 00 |
| 1.329 | 5.02 | 6700.00 | 2.62 | 1.86 | 1.48 | 9.87 | 100.50 | 6.53 | 0.00 | 1.51 | . 20 | .38 |
| 1.329 | 6.79 | 9560.00 | 4.83 | 2.03 | 1.77 | 11.20 | 108.50 | 8.74 | 0.00 | 1.95 | • 23 | •41 |
| 1.329 | 15.72 | 21240.00 | 13.58 | 6,34 | 8,94 | 10,96 | 332.93 | 17.49 | 2602.45 | 1.77 | 2.74 | 0.00 |
| 1,349 | 3.65 | 2630.00 | 0.00 | .12 | 0.00 | 6.11 | 68.23 | 4.23 | 0.00 | | | .16 |
| 1.349 | 5.39 | 6700.00 | 3.40 | . 38 | 1.74 | 12.03 | 75.51 | 7.64 | 0.00 | 2.25 | •52 | • 59 |
| 1.349 | 7.20 | 9560.00 | 5.90 | . 41 | 1.81 | 13.74 | 77.86 | 10.13 | 0.00 | 2.93 | <u> </u> | |
| 1.349 | 15.63 | 21240.00 | 14.92 | 09 | 8.43 | 15.05 | 125.05 | 19.15 | 0.00 | 3.52 | •26 | 1.40 |

| SECNO | CWSEL | QQ | DIFEG. | DIFWSX | DIEWSP | VCH | TOPWID | EG | OWEIR | H.V | H-L | | |
|---------|-------|----------|--------|--------|--------|---------|---------|--------|---|---|--|-------|---|
| 1.490 | 4.75 | 2630.00 | 0.00 | 1.10 | 0.00 | 3.41 | 142.94 | 4.93 | 0.00 | 1.8 | | | |
| T 1.490 | 8.43 | 6700.00 | 3.90 | 3.04 | 3.68 | 5.04 | 158.88 | 8.83 | 0.00 | •39 | 1.01 | •19 | |
| 1,490 | 10.85 | 9560.00 | 6.37 | 3.65 | 2.41 | 5,45 | 376.93 | 11.30_ | 0.4.0.0 | .45 | .92 | | #/2005/m-s/s |
| 1.490 | 19.57 | 21240.00 | 14.71 | 3.94 | 8.72 | 2.78 | 1256.35 | 19.64 | 0.00 | •07 | •15 | •34 | |
| 1.583 | 5.14 | 2375.00 | 0.00 | •39 | 0.00 | 0.00 | 45.43 | 6.65 | 0.00 | 1.51 | •66 | 1.06 | |
| 1.583 | 8.65 | 6035.00 | 5.22 | .21 | 3.51 | 0.00 | 55.95 | 11.87 | 0.00 | 3 . 22 | . 78 | 2.26 | |
| 1.583 | 12.20 | 8615.00 | 6.16 | 1.35 | 3.55 | 0.00 | 1156.80 | 12.81 | 0.00 | .62 | .61 | •13 | |
| 1.583 | 19.67 | 19140.00 | 13.06_ | .10 | 7.47 | 0.00 | 1566.90 | 19.71 | 0.00 | | ······································ | | |
| 1.590 | 6.28 | 23.75.00 | 0.00 | 1.14 | 0.00 | 7.09 | 46.04 | 7.06 | 0.00 | | .19 | | |
| 1.590 | 10.54 | 6035.00 | 5 • 48 | 1.89 | 4.26 | 11.36 | 53.43 | 12.54 | 0.00 | 2.00 | • 30 | •37 | |
| 1.590 | 13.26 | 8615.00 | 7.30 | 1.06_ | 2 • 72 | 9,75 | 1746.51 | 14.36 | 0.00 | 1.10 | | . 24 | |
| 1.590 | 19.67 | 19140.00 | 12.67 | • 00 | 6.41 | 3.96 | 2199.63 | 19.73 | 0.00 | •06 | .01 | •.01 | |
| 1.600 | 6.38 | 2375.00 | 0.00 | .10 | 0.00 | 6.99 | 46.04 | 7.14 | 0.00 | . 76 | • 0 7 | •01 | *************************************** |
| 1.600 | 10.54 | 6035.00 | 5.40 | 00 | 4.16 | 11.36 | 52.84 | 12.54 | 1959.98 | 2.00 | 0.00 | 0.00 | |
| 1.600 | 13.60 | 8615.00 | 7.22 | .35 | 3.07 | 8.52 | 1832.82 | 14.36 | 7052.10 | .76 | 0.00 | 0.00 | |
| 1.600 | 19.75 | 19140.00 | 12.67 | .08 | 6.15 | 3.90 | 2202.15 | 19.81 | 18176.59 | .06 | .08 | 0.00 | |
| 1.604 | 6.85 | 2375.00 | 0.00 | .47 | 0.00 | 5.16 | 65.57 | 7.27 | 0.00 | HE MANUFACTOR OF THE PROPERTY | | 10 | HWOIGHWY22 |
| 1.604 | 12.31 | 6035.00 | 5.71 | 1.77 | 5.46 | 6.67 | 1608.39 | 12.97 | 0.00 | •66 | • 03 | • 40 | |
| 1.604 | 14.19 | 8615.00 | 7.24 | • 59 | 1.88 | 5.48 | 1830.64 | 14.51 | 0.00 | .31 | | .13 | |
| 1.604 | 19.75 | 19140.00 | 12.56 | 00 | 5.56 | 3.72 | 2063.81 | 19.82 | 0.00 | •07 | • 00 | •01 | |
| 1.714 | 7.30 | 2375.00 | 0.00 | . 45 | 0.00 | 10.30 | 61.93 | 8.95 | 0.00 | 1.65 | 1.31 | .37 | |
| 1.714 | 13.16 | 6035.00 | 4.82 | . 85 | 5.85 | 7.18 | 1001.50 | 13.77 | 0.0.0. | | | | MANAGER |
| 1.714 | 14.71 | 8615.00 | 5,98 | •51 | 1.55 | 5 • 2 4 | 1236.33 | 14.93 | 0.00 | • 22 | • 42 | • 0 1 | |
| 1.714 | 19.86 | 19140.00 | 10,97 | •11 | 5.15 | 2,97 | 1783.47 | 19.92 | 0.00 | •06 | .09 | • 00 | |
| 1.732 | 9.01 | 2375.00 | 0.00 | 1.71 | 0.00 | 4.16 | 74.47 | 9.28 | 0.00 | .27 | .19 | .14 | |
| 1.732 | 13.60 | 6035.00 | 4.63 | • 45 | 4.59 | 5.04 | 1171.32 | 13.91 | 0.00 | • 30 | .10 | •03 | |
| 1.732 | 14.76 | 8615.00 | 5.72 | | 1.16 | 5.04 | 1252.39 | 15.00_ | 0.00 | | | | привиделя |
| 1.732 | 19.86 | 19140.00 | 10.66 | • 00 | 5.11 | 3.60 | 1813.86 | 19.94 | 0.00 | •08 | •01 | •01 | |
| 1.733 | 9.01 | 2375.00 | 0.00 | •00 | 0.00 | 4.16 | 74.47 | 9.28 | 0.00 | .27 | •00 | •00 | |
| 1.733 | 13.60 | 6035.00 | 4.63 | .00 | 4,59 | 5.04 | 1170.95 | 13.91 | 0.00 | .31 | • 00 | • 00 | |
| 1.733 | 14.76 | 8615.00 | 5.72 | •00 | 1.16 | 5.04 | 1252.41 | 15.00 | 0.00 | • 24 | • 00 | •00 | |
| 1.733 | 19.86 | 19140.00 | 10.66 | • 00 | 5 1 0 | 3.61 | 1812.73 | 19.94 | AAA TII TAA AAAA AAAA AAAA AAAAA AAAAA AAAAA AAAA | | <u></u> | .0.0 | -10110000 |
| 1.884 | 10.38 | 2375.00 | 0.00 | 1.36 | 0.00 | 5.87 | 610.90 | 10.70 | 0.00 | | 1.38 | •03 | |
| 1.884 | 14,45 | 6035.00 | 3.78 | •84 | 4.07 | 1.32 | 1353.34 | 14.47 | 0.00 | .03 | • 42 | •14 | |
| 1.884 | 15.46 | 8615.00 | 4.79 | • 70 | 1.01 | 1.49 | 1408.63 | 15.49 | 0.00 | .03 | .38 | .11 | |
| 1.884 | 20.08 | 19140.00 | 9.41 | • 22 | 4.62 | 1.55 | 2042.06 | 20.11 | 0.00 | •03 | .15 | •02 | |
| 1.885 | 10.62 | 2375.00 | 0.00 | .25 | 0.00 | 3.44 | 745.43 | 10.78 | 0.00 | •16 | •00 | • 08 | |
| 1.885 | 14.44 | 6035.00 | 3.71 | 01 | 3.81 | 2,69 | 1353,44 | 14.49 | 0.00 | • 05 | • 00 | .02 | |
| 1.885 | 15.45 | 8615.00 | 4.73 | 01 | 1.01 | 3.00 | 1408.71 | 15.51 | 0.00 | •06 | •00 | •02 | |
| 1.885 | 20.08 | 19140.00 | 9,34 | 00 | 4.63 | 2.97 | 2042.07 | 20.12 | 0.00 | | • 00 | .01 | |
| 1.895 | 10,63 | 2375.00 | 0.00 | | 0.00 | <u></u> | 791.24 | 10.89 | 0.00 | .26 | | | мпетела |
| 1.895 | 14.45 | 6035.00 | 3.62 | .01 | 3.82 | 3.19 | 1278.50 | 14.51 | 0.00 | •06 | •01 | •01 | |
| 1.895 | 15.46 | 8615.00 | 4.64 | .01 | 1.01 | 3,55 | 1336.88 | 15.53 | 0.00 | .07 | .01 | .01 | |
| 1.895 | 20.08 | 19140.00 | 9 • 25 | •01 | 4.62 | 3.51 | 1952.20 | 20.13 | 0.00 | •05 | .01 | .01 | |

| | SECNO | CWSEL | Q | DIFEG | DIFWSX | DIFWSP | VCH | TOPWID | <u> FG</u> | OWEIR | н۷ | HL | <u>OLOSS</u> |
|--|-------|-------|----------|-------|--------------|--------|-------|---------|------------|----------|------------|--|--------------|
| A 4 | 1.960 | 10.96 | 2375.00 | 0.00 | .33 | 0.00 | 4.41 | 780.64 | 11.21 | 0.00 | .25 | . 32 | •00 |
| M | 1.960 | 14.54 | 6035.00 | 3.37 | •09 | 3.57 | 2.39 | 1106.37 | 14.58 | 0.00 | • 04 | •07 | •00 |
| · | 1.960 | 15,55 | 8615.00 | 4.39 | .09 | 1.02 | 2.62 | 1137.44 | 15.60 | QQ. | | | |
| | 1.960 | 20.13 | 19140.00 | 8.97 | • 05 | 4.57 | 2.67 | 1788.31 | 20.18 | 0.00 | • 05 | • 05 | •00 |
| | 1.979 | 11.02 | 2375.00 | 0.00 | •05 | 0.00 | 5.14 | 655.08 | 11.40 | 0.00 | •39 | •10 | •10 |
| | 1.979 | 14.52 | 6035.00 | 3.30 | 01 | 3.51 | 4.79 | 1143.68 | 14.70 | 0.00 | .18 | •03 | •10 |
| | 1.979 | 15.54 | 8615.00 | 4.33 | 01 | 1.02 | 5.33 | 1184.73 | 15.73 | 0.00 | • 20 | •03 | •10 |
| | 1.979 | 20.12 | 19140.00 | 8.85 | =.01 | 4.58 | 5.30 | 1340.00 | 20.26 | 0.00 | | | 06 |
| | 1.980 | 10.99 | 2375,00 | 0.00 | 02 | 0.00 | 5,69 | 590.09 | 11.46 | 0.00 | . 46 | • 00 | •05 |
| | 1.980 | 14.67 | 6035.00 | 3.29 | •15 | 3.68 | 3.77 | 1152.09 | 14.75 | 0.00 | •07 | .00 | • 04 |
| | 1.980 | 15.73 | 8615.00 | 4.33 | •19 | 1.06 | 3.31 | 1189.97 | 15,79 | 0.00 | •06 | • 00 | .05 |
| | 1.980 | 20.23 | 19140.00 | 8.83 | •11 | 4.50 | 3.15 | 1340.00 | 20.29 | 0.00 | •06 | • 00 | •03 |
| THE RESERVE OF THE PERSON OF T | 2.057 | 11.53 | 2375.00 | 0.00 | •53 | 0.00 | 4.27 | 109.74 | 11.81 | 0.00 | .28 | • 28 | • 07 |
| | 2.057 | 14.79 | 6035.00 | 3.64 | .12 | 3.26 | 7.03 | 759.93 | 15.45 | 0.00 | .66 | . 29 | .41 |
| | 2.057 | 15.84 | 8615.00 | 4.83 | .11 | 1.05 | 8.25 | 813.10 | 16.64 | 0.00 | •81 | • 33 | • 52 |
| | 2.057 | 20.27 | 19140.00 | 9.08 | • 04 | 4,44 | 8.85 | 882.30 | 20.89 | 0.00 | .61 | .21 | 39 |
| Walter Walter | 2.058 | 11.53 | 2375.00 | 0.00 | .01 | 0.00 | 4.25 | 109.96 | 11.81 | 0.00 | •28 | •00 | •00 |
| | 2.058 | 15.00 | 6035.00 | 3.70 | • 21 | 3.47 | 6.39 | 799.67 | 15.51 | 0.00 | •51 | •00 | •06 |
| | 2.058 | 16.20 | 8615.00 | 4.94 | • 36 | 1.20 | 7.14 | 818.87 | 16,75 | 0.00 | .55 | .00 | .10 |
| | 2.058 | 20.48 | 19140.00 | 9.13 | .21 | 4.28 | 7.93 | 884.19 | 20.95 | 0.00 | •47 | •00 | •06 |
| | 2.063 | 11.78 | 2375.00 | 0.00 | • 25 | 0.00 | 2.52 | 204.49 | 11.88 | 0.00 | .10 | .01 | •05 |
| -\ | 2.063 | 15.52 | 6035.00 | 3.76 | . 52 | 3.74 | 3.20 | 602,53 | 15.64 | 0.00 | .12 | •01 | .12 |
| IV | 2.063 | 16.74 | 8615.00 | 5.01 | •54 | 1.22 | 3.65 | 678.98 | 16.88 | 0.00 | .15 | .01 | •12 |
| | 2.063 | 20.87 | 19140.00 | 9.17 | • 39 | 4.14 | 4.33 | 827.46 | 21.05 | 0.00 | .17 | •01 | .09 |
| | 2.141 | 11.83 | 2375.00 | 0.00 | • 05 | 0.00 | 7.73 | 116.36 | 12.71 | 0.00 | .88 | • 20 | 6.2 |
| | 2.141 | 15.62 | 6035.00 | 3.17 | •10 | 3.79 | 5.30 | 476.47 | 15.88 | 0.00 | • 26 | •13 | •63 •11 |
| | 2.141 | 16.85 | 8615.00 | 4,41 | •11 | 1,23 | 5.53 | 542.75 | 17.12 | 0.00 | .27 | .14 | •10 |
| | 2.141 | 20.97 | 19140.00 | 8.51 | . 10 | 4.12 | 5.60 | 748.69 | 21.22 | 0.00 | •26 | •11 | .07 |
| | 2.150 | 11.98 | 2375.00 | 0.00 | .15 | 0.00 | 8,93 | 62.67 | 13.21 | 0.00 | 1.24 | 22 | 20 |
| | 2.150 | 15,46 | 6035.00 | 3.65 | 16 | 3.48 | 10.31 | 325.05 | 16.86 | 0.00 | 1.40 | •22 •07 | •28 •91 |
| | 2.150 | 16.73 | 8615.00 | 4.67 | 12 | 1.27 | 10.18 | 436.40 | 17.89 | 0.00 | 1.16 | .06 | •71 |
| | 2.150 | 20,93 | 19140.00 | 8 3 1 | ∞. 04 | 4.20 | | 645.77 | 21,53 | 0.00 | | .03 | 27 |
| | 2.157 | 15.05 | 2375.00 | 0.00 | 3.08 | 0.00 | 7.89 | 282.56 | 15.80 | 0.00 | .75 | • 3? | 2.6 |
| | 2.157 | 16.28 | 6035.00 | 1.71 | .82 | 1.23 | 7.61 | 394.80 | 17.51 | 0.00 | 1.23 | •23 | .30 .10 |
| | 2.157 | 17.36 | 8615.00 | 2.31 | •63 | 1.08 | 8.48 | 459.42 | 18.11 | 5627.95 | • 75 | • 23 | 0.00 |
| | 2.157 | 21.58 | 19140.00 | 6.24 | • 64 | 4.21 | 7.43 | 652.99 | 22.04 | 16279.74 | • 46 | •51 | 0.00 |
| | 2.161 | 15.81 | 2375.00 | 0.00 | 76 | 0.00 | 4.50 | 79.06 | 16.12 | 0 • 0 0 | | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~ | 2 L |
| | 2.161 | 17.87 | 6035.00 | 2.02 | 1.59 | 2.06 | 4.85 | 550.95 | 18.14 | 0.00 | •31 •27 | •06 •05 | •26 •58 |
| | 2.161 | 17.40 | 8615.00 | 2.10 | •03 | 47 | 8.33 | 534.18 | 18.22 | 0.00 | .82 | • 05 | •06 |
| | 2.161 | 21.69 | 19140.00 | 5.97 | • 12 | 4.29 | 5.18 | 624.16 | 22.09 | 0.00 | •40 | .02 | •04 |
| | 2.265 | 16.75 | 2375.00 | 0.00 | • 94 | 0.00 | 4.35 | 659,57 | 16.94 | 0.00 | 10 | | |
| | 2.265 | 18.62 | 6035.00 | 1.84 | .75 | 1.87 | 4.64 | 685.98 | 18.79 | 0.00 | 19 | | 01 |
| | 2.265 | 19.27 | 8615.00 | 2.54 | 1.87 | .65 | 5.36 | 695.05 | 19.48 | 0.00 | •17 •22 | •63 | •01 |
| | 2.265 | | 19140.00 | 5.67 | .64 | 3.07 | 5.85 | 710.37 | 22.61 | 0.00 | •28 | 1.20 .50 | .06 |

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| SECNO | CWSEL | | DIFEG | DIFWSX | OTEWSP | VCH | TOPWIO | E.G | OWEIR | HV | HL | 0L0\$S |
|------------------|--|--|--|--|--|--|------------------|--|--|--|---|--|
| * 2.788 | 37.75 | 2375.00 | 0.00 | 21.00 | 0.00 | 1.83 | 166 77 | 27 00 | 0.00 | 0.5 | e c | 0.1 |
| * 7 2.788 | 40.25 | 6035.00 | 2.65 | 21.63 | 2.50 | 3.58 | 155.77 167.03 | 37.80 40.45 | 0.00 | • .0.5 • 2.0 | .55 1.15 | •01 |
| * 788 | 41.70 | 8615.00 | 4.21 | 22,43 | 1.45 | 4.49 | 188.43 | 42.01 | 0.00 | .31 | 1.15 | • 01 |
| */ 2.788 | 45.45 | 19140.00 | 8.49 | 23.12 | 3.75 | 7.46 | 218.57 | 46.29 | 0.00 | .84 | 2.08 | •17 |
| · | | | | | | | | | | | N. 10 11 11 11 11 11 11 11 11 11 11 11 11 | |
| 3.096 | 37.87 | 2375.00 | 0.00 | •12 | 0.00 | 5.36 | 104.88 | 38.32 | 0.00 | • 45 | •36 | •16 |
| 3.096 | 40.71 | 6035.00 | 3.15 | . 46 | 2.84 | 7.28 | 305.80 | 41.47 | 0.00 | . 75 | | .22 |
| 3.096 | 42.36 | 8615.00 | 4.75 | • 66 | 1.65 | 7.42 | 390.78 | 43.07 | 0.00 | •71 | •90 | .16 |
| 3,096 | 46.82 | 19140.00 | 9.15 | 1.37 | 4.46 | 7.84 | 487.77 | 4.7.4.7 | 0.00 | | 1.13 | • 0.4 |
| 3.351 | 41.73 | 2375.00 | 0.00 | 3.86 | 0.00 | 9.17 | 100.61 | 43.04 | 0.00 | 1.31 | 4.46 | . 26 |
| * 7 3.351 | 44.12 | 6035.00 | 3.07 | 3.41 | 2.39 | 11.46 | 184.25 | 46.10 | 0.00 | 1.98 | 3.98 | .37 |
| * 3.351 | 45.53 | 8615.00 | 4.40 | 3.17 | 1.41 | 11.62 | 276.32 | 47.44 | 0.00 | 1.91 | 3.03 | .36 |
| * 3.351 | 48.40 | 19140.00 | 7.21 | 1.57 | 2.87 | 12.90 | 622.28 | 50.25 | 0.00 | 1.85 | 2.02 | •36 |
| . 54551 | 10010 | 1/1/01/00 | · •,- | *** | | 24,470 | 022420 | J V 4 L. J | | 1,00 | 2.002 | • 50 |
| 3.475 | 46.68 | 2375.00 | 0.00 | 4.95 | 0.00 | 10.93 | 46.56 | 48.53 | 0.00 | 1.85 | 5.28 | • 22 |
| * 3,475 | 50.47 | 6035.00 | 4.00 | 6.35 | 3.79 | 11.83 | 165.65 | 52.54 | 0.00 | 2.06 | 3,95 | 03 |
| * 3.475 | 51.78 | 8615.00 | 5.52 | 6.25 | 1.31 | 12.84 | 181.34 | 54.05 | 0.00 | 2.27 | 3.24 | •14 |
| * 3.475 | 55.14 | 19140.00 | 9.84 | 6.74 | 3.36 | 16.23 | 220.00 | 58.37 | 0.00 | 3.24 | 2.73 | . 55 |
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| | manunan and a second a second and | | | | AND AND A SECOND AND AND AND AND AND AND AND AND AND A | | responsibility for material primary and the second of the | NT 200 TO 10 decide hill beliefeler 4° Albert et distances reconstruct consequent securioris | | en en en en en en en en en en en en en e | oodis 1 aantala kassaan alkaasan sakkasan lakkasan lakkasan sa kassa sa kassa sa kassa sa kassa sa kassa sa ka |
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| | | nad Add All Carlo Bell amount Charloster or hand discovered bell and an activative charloster of the activative and the second activative charloster of the activ | alamatan Palatan and Andrews Andrews Towns and Andrews | ann o gaile an tha ann an an an an an an an an an an an a | | andronous authorises de l'Administrative de l' | | | ANGENERAL PARTIES ANGEL | THE CHIEF CONTROL OF THE CHIEF | d Mariolda A. M. I. ad II No. Marionomora il masse e manusconomorar e e e manusconomo e e e e e e e e e e e e e | er og forstatten skriver i statten. Det kjerre forstaten konstatten konstationer kantiliser forstatten kantiliser forstatten konstatten konstat |
| | | | | | | Bernandundungstrader i Samuel i Bernandungstrader i Samuel i Samue | | | - A CONTROL OF THE STATE OF THE | таптитетический под температуру на принцента на принцента на принцента на принцента на принцента на принцента н | Filedolick AEL all Mark in income above, a management of a pronounce of | |
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PEQUONNOCK RIVER

SUMMARY PRINTOUT

BACKWATER

| | SECNO | CWSEL | FLTRD | ELLC | XLCH | ELMIN | K*CHSL | OL OB | QCH | QRO8 | ALPHA | SSTA | ENDST |
|--|--|---|--|---|--|-------------------|--------|---------|----------|--------------|--------|--|--------------------|
| | .057 | 3,60 | 0.00 | 0.00 | 0.00 | -35.00 | 0.00 | 0.00 | 2630.00 | 0.00 | 1.00 | 618.30 | 1269.95 |
| Δ_ | .057 | 3.60 | 0.00 | 0.00 | 0.00 | -35.00 | 0.00 | 0.00 | 6700.00 | 0.00 | 1.00 | 618.30 | 1269.95 |
| 4 | .057 | 3.60 | 0.00 | 0.00 | 0.00 | -35.00 | 0.00 | 0.00 | 9560.00 | 0.00 | 1.00 | 618.30 | 1269.95 |
| \ | .057 | 3.60 | 0.00 | 0.00 | 0.00 | -35.00 | 0.00 | 0.00 | 21240.00 | 0.00 | 1.00 | 618.30 | 1269.95 |
| | •116 | 3.60 | 0.00 | 0.00 | 310.00 | -27.90 | 22.90 | 0.00 | 2630.00 | 0.00 | 1.00 | 824.82 | 1243.25 |
| • | | | | | 310.00 | -27.90 | 22.90 | 0.00 | 6700.00 | 0.00 | 1.00 | 824.82 | 1243.25 |
| | .116 | 3.59 | 0.00 | 0.00 | 310.00 | -27.90 -27.90 | 22.90 | 0.00 | 9560.00 | 0.00 | 1.00 | 824.82 | 1243.25 |
| | .116 .116 | 3.59 3.54 | 0.00 | 0.00 | 310.00 | -27.90 | 22.90 | 0.00 | 21240.00 | 0.00 | 1.00 | 824.82 | 1243.25 |
| | DECAMBLE COMPANIES CONTRACTOR CON | THE RESIDENCE OF THE PROPERTY | Manager and a second a second and mumica/Shares Solvers | THE COLUMN THE PROPERTY OF THE COLUMN THE CO | | | | 2/2/ 00 | A A A | 1.00 | 824.82 | 1243.25 |
| | .131 | 3.60 | 13.60 | 11.90 | 70.00 | -27.90 | 0.00 | 0.00 | 2630.00 | 0.00 | | 824.82 | 1243.25 |
| | .131 | 3.60 | 13.60 | 11,90 | 70.00 | -27.90 | 0.00 | 0.00 | 6700.00 | 0.00 | 1.00 | | 1243.25 |
| | .131 | 3.59 | 13.60 | 11.90 | 70.00 | -27.90 | 0.00 | 0.00 | 9560.00 | 0.00 | 1.00 | 824.82 | |
| | .131 | 3.56 | 13.60 | 11.90 | 70.00 | -27.90 | 0.00 | 0.00 | 21240.00 | 0.00 | 1.00 | 824.82 | 1243.25 |
| | .257 | 3.60 | 0.00 | 0.00 | 680.00 | -25.00 | 4.26 | 0.00 | 2630,00 | 0.00 | 1.00 | MININE AND AND AND AND AND AND AND AND AND AND | |
| <u> </u> | .257 | 3.61 | 0.00 | 0.00 | 680.00 | -25.00 | 4.26 | 0.00 | 6700.00 | 0.00 | 1.00 | 842.78 | 1170.06 |
| $\vdash \prec$ | 257 | 3.61 | 0.00 | 0.00 | 680.00 | -25.00 | 4.26 | 0.00 | 9560.00 | 0.00 | 1.00 | 842.75 | 1170.13 |
| | • 257 | 3.67 | 0.00 | 0.00 | 680.00 | -25.00 | 4.26 | 0.00 | 21240.00 | 0.00 | 1.00 | 842.66 | 1170.40 |
| | | | A A-A | A A A | 300 00 | | 1 20 | 773.00 | 1580.87 | 276.13 | 1.07 | 784.08 | 1178.54 |
| | • 390 | 3.60 | 0.00 | 0.00 | 720.00 | -24.00 | 1.39 | 1970.31 | 4025.90 | 703.79 | 1.07 | 784.08 | 1178.58 |
| | .390 | 3.60 | 0.00 | 0.00 | 720.00 | -24.00 | 1.39 | | | 1003.99 | 1.07 | 784.08 | 1178.56 |
| | .390 | 3.61 | 0.00 | 0.00 | 720.00 | -24.00 | 1.39 | 2810.68 | 5745.32 | | 1.07 | | 1178.72 |
| | .390 | 3.63 | 0.00 | 0.00 | 720.00 | -24.00 | 1.39 | 6257.23 | 12747.96 | 2234.81 | 1.0/ | 107100 | |
| | •437 | 3.61 | 0.00 | 0.00 | 200.00 | -23.00 | 5.00 | 0.00 | 2630.00 | 0.00 | 1.00 | 799.70 | 1200.51 |
| | .437 | 3.64 | 0.00 | 0.00 | 200.00 | -23.00 | 5.00 | 0.00 | 6700.00 | 0.00 | 1.00 | 799.70 | 1200.52 |
| | .437 | 3.68 | 0.00 | 0.00 | 200.00 | -23.00 | 5.00 | 0.00 | 9560.00 | 0.00 | 1.00 | 799.69 | 1.200.53 |
| | .437 | 4.01 | 0.00 | 0.00 | 200.00 | -23.00 | 5.00 | 0.00 | 21240.00 | 0.00 | 1.00 | 799.67 | 1200.57 |
| | • 481 | 2 61 | 0.00 | 0.00 | 240.00 | -20.80 | 9.17 | 0.00 | 2630.00 | 0.00 | 1.00 | 796.03 | 1202.17 |
| | | 3.61 | | | 240.00 | -20.80 | 9.17 | 0.00 | 6700.00 | 0.00 | 1.00 | 796.03 | 1202.17 |
| | • 481 | 3.63 | 0.00 | 0.00 | | | 9.17 | 0.00 | 9560.00 | 0.00 | 1.00 | 796.03 | 1202.17 |
| | .481 .481 | 3.67 3.94 | 0.00 | 0.00 <u>0.00</u> | 240.00 240.00 | -20.80 -20.80 | 9.17 | 0.00 | • | 0.00 | 1.00 | 796.02 | |
| | | | | | | | | | 0.400.00 | 0.00 | 1 00 | 796.03 | 1202.17 |
| | •498 | 3,61 | 9,00 | 15.00 | 80.00 | -20.80 | 0.00 | 0.00 | 2630.00 | 0.00 | 1.00 | | 1202.17 |
| | •498 | 3.64 | . 9.00 | 15.00 | 80.00 | -20.80 | 0.00 | 0.00 | 6700.00 | 0.00 | 1.00 | 796.03 | |
| | •498 | 3.67 | 9.00 | 15.00 | 80.00 | -20.80 | 0.00 | 0.00 | 9560.00 | 0,00 | 1.00 | 796.03 796.02 | 1202.17 1202.17 |
| | .498 | 3.97 | 9.00 | 15.00 | 80.00 | -20.80 | 0.00 | 0.00 | 21240.00 | 0.00 | 1 • UV | 1700VC | |
| | •573 | 3.61 | 0.00 | 0.00 | 410.00 | -20.00 | 1.95 | 0.00 | 2630.00 | 0.00 | 1.00 | 884.58 | 1117.22 |
| | .573 | 3.65 | 0.00 | 0.00 | 410.00 | -20.00 | 1.95 | 0.00 | 6700.00 | 0.00 | 1.00 | 884.57 | 1117.31 |
| | •573 | 3.70 | 0.00 | 0.00 | 410.00 | -20.00 | 1.95 | 0.00 | 9560.00 | 0.00 | 1.00 | 884.56 | 1117.41 |
| THE STATE OF THE S | .573 | 4.08 | 0.00 | 0.00 | 410.00 | -20.00 | 1,95 | 0.00 | 21240.00 | 0.00 | 1.00 | 884.52 | 1118.16 |
| | .701 | 3.61 | 0.00 | 0.00 | 670.00 | -19.20 | 1,19 | 0.00 | 2630.00 | 0.00 | 1.00 | 851.04 | 1031.08 |
| | | | 0.00 | 0.00 | 670.00 | -19.20 | 1.19 | 0.00 | 6700.00 | 0.00 | 1.00 | 851.04 | 1031.08 |
| | • 701 | 3.65 | | | 670.00 | -19.20 -19.20 | 1.19 | 0.00 | 9560.00 | 0.00 | 1.00 | 851.04 | 1031.08 |
| | .701 .701 | 3.71 4.12 | 0.00 | 0.00 | 670.00 | -19.20 | 1.19 | 0.00 | 21240.00 | 0.00 | 1.00 | 851.04 | 1031.08 |
| | | | ,,,,,,, | | | | 0.00 | 0.00 | 2620 00 | 0.00 | 1.00 | 851.04 | 1031.08 |
| | .711 | 3.61 | 14.50 | 9.10 | 70.00 | -19.20 | 0.00 | 0.00 | 2630.00 | 0.00 | 1.00 | 851.04 | 1031.08 |
| | . 711 | 3.65 | 14.50 | 9.10 | 70.00 | -19.20 | 0.00 | 0.00 | 6700.00 | | 1.00 | 851.04 | 1031.08 |
| | •711 | 3.70 | 14.50 | 9.10 | 70.00 | -19.20 | 0.00 | 0.00 | 9560.00 | 0.00 | | 851.04 | 1031.08 |
| | .711 | 4.07 | 14.50 | 9.10 | 70.00 | -19.20 | 0.00 | 0.00 | 21240.00 | 0.00 | 1.00 | 071104 | 100100 |

| | SECNO | CWSEL | FLTRD | ELLC | XLCH | ELMIN_ | K*CH\$L | QLOB | QCH | QRQ8 | AL PHA | SSTA | ENDST | |
|--|-------|-------|-------|-------|---------|------------------|---------|--------|-----------|-------------------------|--------|----------|--------------|--|
| | 834 | 3.63 | 0.00 | 0.00 | 660.00 | -19.00 | •30 | 0.00 | 2630.00 | 0.00 | 1.00 | 875.96 | 1112.37 | |
| Tomas . | .834 | 3.79 | 0.00 | 0.00 | 660.00 | -19.00 | • 30 | 0.00 | 6700.00 | 0.00 | 1.00 | 875.72 | 1113.10 | |
| _/ | .834 | 3,98 | 0.00 | 0.00 | 660.00 | -19.00 | | 0.0.0 | 9560 • 00 | 0.00 | 1.00 | 8.75 4.3 | | Second Se |
| and a summa | .834 | 5.48 | 0.00 | 0.00 | 660.00 | -19.00 | • 30 | 0.00 | 21240.00 | 0.00 | 1.00 | 873.10 | 1121.10 | |
| | •952 | 3.63 | 0.00 | 0.00 | 630.00 | -18.60 | .63 | 0.00 | 2630.00 | 0.00 | 1.00 | 860.84 | 1140.03 | |
| | .952 | 3.80 | 0.00 | 0.00 | 630.00 | -18.60 | 63 | 0.00 | 6700.00 | 0.00 | 1.00 | 860.83 | 1140.45 | |
| | .952 | 4.00 | 0.00 | 0.00 | 630.00 | -18.60 | .63 | 0.00 | 9560.00 | 0.00 | 1.00 | 860.81 | 1140.98 | |
| est transference and an extension of the second of the second of the second of the second of the second of the | 952 | 5,58 | 0.00 | 0.00 | 630.00 | -18.60 | 63 | 0.0 | 21240.00 | | 1.00 | 860.68 | | agaspadyundsyavilgs-eritysig |
| | .962 | 3.63 | 16.50 | 17.00 | 60.00 | -18.60 | 0.00 | 0.00 | 2630.00 | 0.00 | 1.00 | 860 • 84 | 1140.02 | |
| | •962 | 3.80 | 16.50 | 17.00 | 60.00 | -18.60 | 0.00 | 0.00 | 6700.00 | 0.00 | 1.00 | 860.83 | 1140.46 | |
| | .962 | 4.01 | 16.50 | 17.00 | 60.00 | -18.60 | 0.00 | 0.00 | 9560.00 | 0.00 | 1.00 | 860.81 | 1141.01 | |
| | •962 | 5.62 | 16.50 | 17.00 | 60.00 | -18.60 | 0.00 | 0.00 | 21240.00 | 0.00 | 1.00 | 860.68 | 1179.50 | |
| | 1.096 | 3.64 | 0.00 | 0.00 | 660.00 | -13.30 | 8.03 | 0.00 | 2630.00 | 0.00 | 1.00 | 876.70 | 1126.60 | |
| | 1.096 | 3.83 | 0.00 | 0.00 | 660.00 | -13.30 | 8.03 | 0.00 | 6700.00 | 0.00 | 1.00 | 876.45 | | |
| | 1.096 | 4.07 | 0.00 | 0.00 | 660.00 | -13.30 | 8.03 | 0.00 | 9560.00 | 0.00 | 1.00 | 876.16 | 1127.68 | |
| - | 1.096 | 5.85 | 0.00 | 0.00 | 660.00 | -13.30 | 8.03 | 1.28 | 21237.92 | .80 | 1.00 | 861.46 | 1134.70 | |
| | 1.250 | 3.64 | 0.00 | 0.00 | 1000.00 | -7.10 | 6.20 | 0.00 | 2630.00 | 0.00 | 1.00 | | 1122.74 | erroma are Mandre d'Arrichada e errom |
| | 1.250 | 3.83 | 0.00 | 0.00 | 1000.00 | -7.10 | 6.20 | 0.00 | 6700.00 | 0.00 | 1.00 | 871.94 | 1123.06 | |
| 1 7 | 1.250 | 4.07 | 0.00 | 0.00 | 1000.00 | ~7.10 | 6.20 | 0.00 | 9560.00 | 0.00 | 1.00 | | 1123,46 | |
| | 1.250 | 5.87 | 0.00 | 0.00 | 1000.00 | -7.10 | 6.20 | 0.00 | 21240.00 | 0.00 | 1.00 | 869.74 | 1126.73 | |
| | 1.319 | 3.48 | 0.00 | 0.00 | 390.00 | -4.50 | 6.67 | 0.00 | 2630.00 | 0.00 | 1.00 | 922.04 | 1019.37 | |
| <u> </u> | 1.319 | 3,16 | 0.00 | 0.00 | 390.00 | -4.50 | 6.67 | 0.0.0. | 6700.00 | | | 922.99 | 1.0.1.8. 6.9 | Marian de Caración |
| • | 1.319 | 4.76 | 0.00 | 0.00 | 390.00 | -4.50 | 6.67 | 0.00 | 9560.00 | 0.00 | 1.00 | 918.30 | 1022.00 | |
| k . | 1.319 | 9.39 | 0.00 | 0.00 | 390.00 | -4.50 | 6.67 | 0.00 | 21240.00 | 0.00 | 1.00 | 917.50 | 1026.00 | |
| | 1.329 | 3.54 | 15.30 | 9.50 | 50.00 | -4.50 | 0.00 | 0.00 | 2630.00 | 0.00 | 1.00 | 921.85 | 1019.49 | |
| | 1.329 | 5.02 | 15.30 | 9.50 | 50.00 | -4.50 | 0.00 | 0.00 | 6700.00 | 0.00 | 1.00 | 917.60 | 1022.53 | |
| | 1.329 | 6.79 | 15.30 | 9,50 | 50.00 | -4.50 | 0.00 | 0.00 | 9560.00 | | 1.00 | 917.50 | 1026.00 | LANGUA TIMOTETTI IN THE STATE OF THE STATE O |
| | 1.329 | 15.72 | 15.30 | 9.50 | 50.00 | -4.50 | 0.00 | 0.00 | 20067.16 | 1172.84 | 1.25 | 917.50 | 1300.41 | |
| | 1.349 | 3.65 | 0.00 | 0.00 | 130.00 | -4.40 | .77 | 0.00 | 2630.00 | 0.00 | 1.00 | 967.26 | 1035.49 | |
| | 1.349 | 5.39 | 0.00 | 0.00 | 130.00 | -4.40 | • 77 | 0.00 | 6700.00 | 0.00 | 1.00 | 964.88 | 1040.39 | |
| Π | 1.349 | 7.20 | 0.00 | 0.00 | 130.00 | -4.40 | •77 | 0.00 | 9560.00 | 0.00 | 1.00 | | 1042.20 | |
| | 1,349 | 15.63 | 0.00 | 0.00 | 130.00 | =4.40 | • 77 | | 21239.19 | <u>81</u> (m. 44-18 mil | 1.00 | 962.00 | 1087.05 | HERMANICAL PARTICIPATION OF THE PERTURNING PARTICIPATION OF TH |
| | 1.490 | 4.75 | 0.00 | 0.00 | 740.00 | -3.50 | 1.22 | 0.00 | 2630,00 | 0,00 | 1.00 | 926.24 | 1069.18 | |
| 7 | 1.490 | 8.43 | 0.00 | 0.00 | 740.00 | -3.50 | 1.22 | 0.00 | 6700.00 | 0.00 | 1.00 | 914.70 | 1073.58 | |
| | 1.490 | 10.85 | 0.00 | 0.00 | 740.00 | -3.50 | 1.22 | . 10 | 9395.29 | 164.62 | 1.10 | 909.15 | 1750.82 | |
| | 1.490 | 19.57 | 0.00 | 0.00 | 740.00 | -3.50 | 1.22 | 22.42 | 8774.10 | 12443.47 | 1.24 | 900.44 | 2156.79 | |
| | 1.583 | 5.14 | 0.00 | 0.00 | 510.00 | -3.00 | •98 | 0.00 | 0.00 | 2375.00 | 1.00 | 979.71 | 1025.14 | TOTAL POSSESSES MITTERS / ATV A |
| | 1.583 | 8.65 | 0.00 | 0.00 | 510.00 | -3.00 | • 98 | 0.00 | 0.00 | 6035.00 | 1.00 | 972.70 | 1028.65 | |
| ٠ | 1.583 | 12.20 | 0.00 | 0.00 | 510.00 | -3.00 | • 98 | 0.00 | 0.00 | 8615.00 | 1.00 | 961.20 | | |
| | 1.583 | 19.67 | 0.00 | 0.00 | 510.00 | -3.00 | • 98 | 0.00 | 0.00 | 19140.00 | 1.00 | 763.20 | 2330.10 | |
| | 1.590 | 6.28 | 0.00 | 0.00 | 60.00 | -2.90 | 1.67 | 0.00 | 2375.00 | 0.00 | 1.00 | 972.04 | 1018.08 | |
| | 1.590 | 10.54 | 0.00 | 0.00 | 60.00 | -2.90 | 1.67 | • 0 0 | 6034.37 | •63 | 1.00 | 971.76 | 1309.89 | |
| : | 1.590 | 13.26 | 0.00 | 0.00 | 60.00 | <u>~2.90</u> | 1.67 | 1.64 | 6399.01 | 2214.35 | 6.64 | | 2841.26 | |
| | 1.590 | 19.67 | 0.00 | 0.00 | 60.00 | -2.90 | 1.67 | 226.66 | 3768.01 | 15145.33 | 2.65 | 749.72 | 2949.35 | |

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| SECNO | CWSFL | FLTRD | FLLC | XLCH | ELMIN | K*CHSL | QLOB | осн | QROB | ALPHA | SSTA | ENDST |
|-------------|-------|--------|---------|--------|------------------------|--------|------------------|--------------------|--------------------|---------------------------------------|------------------|--------------------|
| 1.600 | 6.38 | 10.50 | 10.00 | 50.00 | -2.90 | 0.00 | 0.00 | 2375.00 | 0.00 | 1.00 | 972.04 | 1018.08 |
| 1.600 | 10.54 | 10.50 | 10.00 | 50.00 | -2.90 | 0.00 | 0.00 | 6034.37 | .63 | 1.00 | 972.00 | 1309.62 |
| 1.600 | 13.60 | 10.50 | 10.00 | 50.00 | 2,90 | 0.00 | 0.00 | 5727.91 | 2887.09 | 6.95 | 972.00 | 2860.94 |
| 1.600 | 19.75 | 10.50 | 10.00 | 50.00 | -2.90 | 0.00 | 235.69 | 3732.41 | 15171.90 | 2.63 | 747.36 | 2949.51 |
| 1.604 | 6.85 | 0.00 | 0.00 | 20.00 | -2.80 | 5.00 | 0.00 | 2375.00 | 0.00 | 1.00 | 968.14 | 1033.71 |
| 1.604 | 12.31 | 0.00 | 0.00 | 20.00 | -2.80 | 5.00 | 0.00 | 5787.97 | 247.03 | 2,52 | 962,70 | 2754.12 |
| 1.604 | 14.19 | 0.00 | 0.00 | 20.00 | -2.80 | 5.00 | 0.00 | 5705.77 | 2909.23 | 5.97 | 960.81 | 2842.11 |
| 1.604 | 19.75 | 0.00 | 0.00 | 20.00 | -2.80 | 5.00 | 126.25 | 5832.34 | 13181.41 | 3.28 | 891.21 | 2955.02 |
| 1.714 | 7.30 | 0,00 | 0.00 | 610.00 | 1.60 | 7.21 | 0.00 | 2375.00 | 0.00 | 1.00 | 967.69 | 1029,62 |
| 1.714 | 13.16 | 0.00 | 0.00 | 610.00 | 1.60 | 7.21 | 0.00 | 4598.15 | 1436.85 | 2.77 | 961.84 | 2072.87 |
| 1.714 | 14.71 | 0.00 | 0.00 | 610.00 | 1,60 | 7.21 | 0.00 | 3993.16 | 4621.84 | 2.22 | 960.29 | 2196.63 |
| 1.714 | 19.86 | 0.00 | 0.00 | 610.00 | 1.60 | 7.21 | 28.66 | 3582.19 | 15529.15 | 1.20 | 901.39 | 2684.86 |
| 1.732 | 9.01 | 0.00 | 0.00 | 110.00 | • 30 | -11.82 | 0.00 | 2375.00 | 0.00 | 1.00 | 961.25 | 1036.71 |
| 1.732 | 13.60 | 0.00 | 0.00 | 110.00 | .30 | -11.82 | 9.33 | 4615.60 | 1410.07 | 3.02 | 947.91 | 2163.89 |
| 1.732 | 14.76 | 0.00 | 0.00 | 110.00 | .30 | -11.82 | 25.85 | 5057.72 | 3531.44 | 3.00 | 941.37 | 2193.75 |
| 1.732 | 19.86 | 0.00 | 0.00 | 110.00 | • 30 | -11.82 | 249,77 | 5016.34 | | 1.70 | 868,17 | 2682.04 |
| 1,733 | 9.01 | 11.00 | 11.30 | 1.00 | . 30 | 0.00 | 0.00 | 2375.00 | 0.00 | 1.00 | 961.25 | 1036.71 |
| 1.733 | 13.60 | 11.00 | 11.30 | 1.00 | • 30 | 0.00 | 9.31 | 4618.21 | 1407.49 | 3.02 | 947.92 | 2163.82 |
| 1.733 | 14.76 | 11.00 | 11.30 | 1.00 | • 30 | 0.00 | 25.85 | 5056.97 | 3532.18 | 3.00 | 941.36 | 2193.77 |
| 1.733 | 19.86 | 11.00 | 11.30 | 1.00 | • 30 | 0.00 | 249.48 | 5020.56 | 13869.97 | 1.70 | 868.28 | 2681.01 |
| 1.884 | 10.38 | 8.80 | 1200.00 | 800.00 | 2.10 | 2.25 | 1122.24 | 1252.76 | 0.00 | 1 07 | 101 70 | 10/0 72 |
| 1.884 | 14.45 | 8.80 | 1200.00 | 800.00 | 2.10 | 2.25 | 4893.98 | 408.30 | 732.72 | 1.87 1.03 | 191.79 102.24 | 1040.73 1455.58 |
| 1.884 | 15.46 | 8.80 | 1200.00 | 800.00 | 2.10 | 2.25 | 6581.82 | 581.69 | 1451.49 | 1.01 | 87.26 | 1495.89 |
| 1.884 | 20.08 | 8.80 | 1200.00 | 800.00 | 2.10 | 2.25 | 12343.67 | 1194.45 | 5601.87 | 1.00 | 59.05 | 2101.11 |
| 1.885 | 10.62 | 0.00 | 0.00 | 1.00 | 2.10 | 0.00 | 377.65 | 1997.35 | 0.00 | 2.71 | 186.24 | 1040 77 |
| 1.885 | 14.44 | 0.00 | 0.00 | 1.00 | 2.10 | 0.00 | 3167.33 | 2396.01 | 471.66 | 2.59 | 102.19 | 1040.77 1455.63 |
| 1.885 | 15.45 | 0.00 | 0.00 | 1.00 | 2.10 | 0.00 | 4673.24 | 2921.09 | 1020.66 | 2.28 | 87.25 | 1495.96 |
| 1.885 | 80.08 | 0.00 | 0.00 | 1.00 | 2.10 | 0.00 | 10455.69 | 4006.23 | 4678.08 | 1.59 | 59.04 | |
| 1.895 | 10.63 | 0.00 | 0.00 | 60.00 | 2.00 | -1.67 | 484.77 | 1890.23 | 0.00 | 2 60 | 107 / 2 | 1020 21 |
| / 1.895 | 14.45 | 0.00 | 0.00 | 60.00 | 2.00 | -1.67 | 3487.01 | 1986.12 | 561.87 | 3.69 2.91 | 197.43 120.96 | 1030.31 1399.46 |
| 1.895 | 15.46 | 0.00 | 0.00 | 60.00 | 2.00 | -1.67 | 5097.10 | 2404.87 | 1113.03 | 2.50 | | 1445.00 |
| 1.895 | 20.08 | 0.00 | 0.00 | 60.00 | 2.00 | -1.67 | 11228.27 | 3270.28 | 4641.44 | 1.68 | | 2040.68 |
| 1.960 | 10.96 | 0.00 | 0.00 | 350.00 | 1.60 | -1.14 | 422.80 | 1001 02 | 50 24 | ኃ ኃ ፡ | 222 70 | 1102 22 |
| 1.960 | 14.54 | . 0.00 | 0.00 | 350.00 | 1.60 | -1.14 | 3440.66 | 1901.83 1711.66 | 50.36 882.68 | 2.35 1.45 | 322.78 242.05 | 1192.22 1348.42 |
| 1.960 | 15.55 | 0.00 | 0.00 | 350.00 | 1.60 | -1.14 | 5141.57 | 2093.46 | 1379.97 | 1.43 | 228,91 | 1366,35 |
| 1.960 | 20.13 | 0.00 | 0.00 | 350.00 | 1.60 | -1.14 | 12251.87 | 3107.63 | 3780.49 | 1.15 | 214.29 | 2002.60 |
| 1.979 | 11.02 | 0.00 | 0.00 | 110.00 | 1.30 | -2.73 | 55.93 | 22/Q 20 | 70 70 | • • • • • • • • • • • • • • • • • • • | 2/0 50 | 1200 |
| 1.979 | 14.52 | 0.00 | 0.00 | 110.00 | 1.30 | -2.73 | 1868.45 | 2248.30 2973.28 | 70.78 1193.27 | 2.54 5.12 | 349.52 244.36 | 1300.40 1388.04 |
| 1.979 | 15.54 | 0.00 | 0.00 | 110.00 | 1.30 | -2.73 | 3130.15 | 3591.86 | 1892.99 | 4.54 | 227.84 | 1412.57 |
| 1.979 | 20.12 | 0.00 | 0.00 | 110.00 | 1.30 | -2.73 | 9084.65 | 4846.87 | 5208.48 | 2.82 | 210.00 | 1550.00 |
| 1.980 | 10,99 | 10.00 | 10.00 | 1,00 | 1.30 | 0.00 | 99 74 | 2100 50 | 102 // | | | |
| 1.980 | 14.67 | 10.00 | 10.00 | 1.00 | 1.30 | 0.00 | 82.76 2864.56 | 2188.59 1448.99 | 103.66 | 2,50 | 350.18 | 1299.65 |
| 1.980 | 15.73 | 10.00 | 10.00 | 1.00 | 1.30 | 0.00 | 4595.77 | 1440.99 | 1721.45 2636.83 | 1.94 1.32 | 239.77 | 1391.86 |
| 1.980 | 20.23 | 10.00 | 10.00 | 1.00 | 1.30 | 0.00 | 10952.31 | 2056.44 | 6131.25 | 1.14 | 227.08 210.00 | 1417.05 1550.00 |
| - · · · · - | | . • | | | .= * ~ * | 2 | | → w + ~ w w 1 1 | | * # F I | | *>> \ |

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| SECNO | CWSEL | FLTRD | ELLC | XLCH | ELMIN_ | K*CHSL | QLOB | QCH | QROB | ALPHA | S.S.T.A | ENDST |
|-----------|-------|-------|--------|---------|--------|--------|----------|----------------|-----------|--|----------|---------|
| 2.057 | 11.53 | 11.50 | 10.00 | 400.00 | .10 | -3.00 | .00_ | 2372.58 | 2.42 | 1.02 | 637.08 | 1038.71 |
| 2.057 | 14.79 | 11.50 | 10.00 | 400.00 | .10 | -3.00 | 803.16 | 5161.94 | 69.90 | 3.57 | 282.61 | 1058.41 |
| 2.057 | 15.84 | 11.50 | 10.00_ | 400.00 | .10 | -3.00 | 1955.48 | 6527.39 | 132.13 | 4.41 | 251.62 | |
| 2.057 | 20.27 | 11.50 | 10.00 | 400.00 | .10 | -3.00 | 9464.40 | 9140.09 | 535.52 | 3.97 | 209.18 | 1091.48 |
| 2.058 | 11.53 | 0.00 | 0.00 | 1.00 | .10 | 0.00 | 9.76 | 2362.83 | 2.41 | 1.11 | 636.97 | 1038.72 |
| 2.058 | 15.00 | 0.00 | 0.00 | 1.00 | 10 | 0.00 | 1116.74 | 4848.71 | 69.55 | 4.40 | 260.00 | 1059.67 |
| 2.058 | 16.20 | 0.00 | 0.00 | 1.00 | .10 | 0.00 | 2568.63 | 5916.54 | 129.84 | 4.81 | 248.02 | 1066.89 |
| 2,058 | 20.48 | 0.00 | 0.00 | 1.00 | .10 | 0.00 | 10093.95 | 8555.24 | 490.80 | 3.81 | <u> </u> | 1092.74 |
| 2.063 | 11.78 | 0.00 | 0.00 | 40.00 | 1.80 | 42.50 | 12.81 | 2344.86 | 17.33 | 1.08 | 860.95 | 1065.45 |
| A / 2.063 | 15.52 | 0.00 | 0.00 | 40.00 | 1.80 | 42.50 | 1375.12 | 4423.80 | 236.08 | 1.61 | 500.59 | 1103.11 |
| 2.063 | 16.74 | 0.00 | 0.00 | 40.00 | 1.80 | 42.50 | 2596.64 | 5586.73 | 431.63 | 1.57 | 431.45 | 1110.43 |
| 2.063 | 20.87 | 0.00 | 0.00 | 40.00 | 1.80 | 42.50 | 8985.31 | 8780.29 | 1374.40 | 1.38 | 307.78 | 1135.24 |
| 2.141 | 11.83 | 0.00 | 0.00 | 420.00 | 7.00 | 12.38 | 85.15 | 2244.46 | 45.39 | 1.15 | 935.87 | 1052.23 |
| 2.141 | 15.62 | 0.00 | 0.00 | 420.00 | 7.00 | 12.38 | 463.57 | 2945.59 | 2625.84 | 1.47 | | 1389.04 |
| 2.141 | 16.85 | 0.00 | 0.00 | 420.00 | 7.00 | 12.38 | 699.04 | 3551.00 | 4364.96 | 1.35 | 897.82 | 1440.57 |
| 2.141 | 20.97 | 0.00 | 0.00 | 420.00 | 7.00 | 12.38 | 2692.11 | 5210.07 | 11237.82 | 1.23 | 700.81 | 1449.50 |
| 2.150 | 11.98 | 0.00 | 0.00 | 50.00 | 7.40 | 8,00 | 0.00 | 2375.00 | 0.00 | 1.00 | 968.69 | 1031.36 |
| 2.150 | 15.46 | .0.00 | 0.00 | 50.00 | 7.40 | 8.00 | 7.55 | 5029.51 | 997.94 | 1.63 | 962.74 | 1448.45 |
| 2.150 | 16.73 | 0.00 | 0.00 | 50.00 | 7.40 | 8,00 | 35.65 | 5792.25 | 2787.09 | 1.70 | 958.17 | 1490.03 |
| 2.150 | 20.93 | 0.00 | 0.00 | 50.00 | 7.40 | 8.00 | 567.46 | 7010.17 | 11562.37 | 1.36 | 844.75 | 1490.52 |
| k 2.157 | 15.05 | 13.00 | 14.00 | 35.00 | 7.40 | 0.00 | 0.00 | 1022.85 | 1352.15 | 1.05 | 968.00 | 1432.14 |
| × 2.157 | 16.28 | 13.00 | 14.00 | 35.00 | 7.40 | 0.00 | 0.00 | 995.31 | 5039.68 | 1.001 | 968.00 | 1481.30 |
| 2.157 | 17.36 | 13.00 | 14.00 | 35.00 | 7.40 | 0.00 | 0.00 | 5169.24 | 3445 + 76 | 1.60 | 968.00 | 1490.10 |
| 2.157 | 21.58 | 13.00 | 14,00 | 35.00 | 7.40 | 0.00 | 747.56 | 6530.71 | 11861,72 | 1.32 | 837.61 | 1490,60 |
| 2.161 | 15.81 | 0.00 | 0.00 | 20.00 | 8.00_ | 30.00 | 0.00 | 2375.00 | 0.00 | 1.00 | 960.00 | 1040.00 |
| 2.161 | 17.87 | 0.00 | 0.00 | 20.00 | 8.00 | 30.00 | 15.32 | 3355.33 | 2664.34 | 1.16 | 949.23 | 1500.18 |
| 2.161 | 17.40 | 0.00 | 0.00 | 20.00 | 8.00 | 30.00 | 17.03 | <u>5454.71</u> | 3143.26 | 1.420 | 950.98 | 1500.13 |
| 2.161 | 21.69 | 0.00 | 0.00 | 20.00 | 8.00 | 30.00 | 591.58 | 5168.13 | 13380.28 | 1.04 | 876.46 | 1500.62 |
| 2.265 | 16.75 | 0.00 | 0.00 | 560.00 | 10.00 | 3.57 | 19.88 | 1474.58 | 880.53 | 2.11 | 940.51 | |
| 2.265 | 18.62 | 0.00 | 0.00 | 560.00 | 10.00 | 3.57 | 123.37 | 2059.99 | 3851.64 | 1.46 | 914.31 | 1600.29 |
| 2.265 | 19.27 | 0.00 | 0.00 | 560.00 | 10.00 | 3.57 | 208.91 | 2569.56 | 5836.53 | 1.35 | 905.32 | 1600.36 |
| 2.265 | 22.33 | 0.00 | 0.00 | 560.00 | 10.00 | 3.57 | 858.22 | 3809.38 | 14472.40 | maanamaan energyy-käär – 25. Proposition in 1979 van 1979 van 1979 van 1979 van 1979 van 1979 van 1979 van 197 | | 1600.70 |
| 2.788 | 37.75 | 0.00 | 0.00 | 2530.00 | 25.10 | 5.97 | .12 | 2374.88 | 0.00 | 1.00 | | 1043.24 |
| 2.788 | 40.25 | 0.00 | 0.00 | 2530.00 | 25.10 | 5.97 | 6.14 | 6028.84 | • 02 | 1.02 | 880.78 | |
| 2.788 | 41.70 | 0.00 | 0.00 | 2530.00 | 25.10 | 5.97 | 18.06 | 8585.46 | 11.47 | 1.04 | 876.90 | 1065.33 |
| 2.788 | 45.45 | 0.00 | 0.00 | 2530.00 | 25.10 | 5.97 | 114.28 | 18625.31 | 400.41 | 1.11 | 866.88 | 1085.45 |
| 3.096 | 37.87 | 0.00 | 0.00 | 1630.00 | 32.30 | 4 • 42 | 0.00 | 2375•00 | 0.00 | 1.00 | 945.67 | |
| 3.096 | 40.71 | 0.00 | 0.00 | 1630.00 | 32.30 | 4.42 | 549.41 | 5477.93 | 7.67 | 1.33 | 754.91 | 1060.71 |
| 3.096 | 42.36 | 0.00 | 0.00 | 1630.00 | 32.30 | 4.42 | 1651.94 | 6932.66 | 30.40 | 1.49 | 635.17 | 1062.36 |
| 3.096 | 46.82 | 0.00 | 0.00 | 1630.00 | 32.30 | 4.42 | 7829.04 | 11171.57 | 139.39 | 1.48 | 579.05 | 1066.82 |
| 3.351 | 41.73 | 0.00 | 0.00 | 1310.00 | 38.00 | 4,35 | 0.00 | 2374.72 | . 28 | 1.00 | | 1053.26 |
| 3.351 | 44.12 | 0.00 | 0.00 | 1310.00 | 38.00 | 4.35 | 18.63 | 5854.42 | 161.95 | 1.14 | 903.22 | |
| 3.351 | 45.53 | 0.00 | 0.00 | 1310.00 | 38.00 | 4.35 | 411.67 | 7740.66 | 462.67 | 1.33 | | 1100.53 |
| 3.351 | 48.40 | 0.00 | 0.00 | 1310.00 | 38.00 | 4.35 | 4932.88 | 12655.25 | 1551.88 | 1.63 | 481.12 | 1103.40 |

| 2 | / 7 E | | 0.00 | 0.00 | | (1.00 | 4 C.C | 0.00 | 0075 00 | | , | A 77 - A A | |
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| | <u>.475</u> .475 | 46.68 50.47 | 0.00 | 0.00 | 660.00 660.00 | 41.00 41.00 | 4.55 4.55 | 0.00 324.08 | 2375.00 5710.67 | 0.00 | 1.00 | | 1024.46 |
| | • 475 | 51.78 | 0.00 | 0.00 | 660.00 | 41.00 | 4.55 | 1149.90 | 7457.11 | .24 7.98 | 1.23 1.28 | 885.29 | |
| | •475 | 55.14 | 0.00 | 0.00 | 660.00 | 41.00 | 4.55 | | 13520.64 | | | | 1053.56 |
| | • 7 () | 25.14 | 0.00 | 0.00 | 000.00 | 41.00 | 4.00 | 2405.01 | 13920.04 | 135.75 | 1.25 | 840.00 | 1060.00 |
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| SUMMARY | OF ERRO | RS | | | | | | 00776_00706F708_1007000E301306E303011 | | | | | |
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| <u>የ</u> ል፤፤ቸ የ ጠእነ | CCCNOS | 1 500 | 0005115- 2 | COTTTCAL | OCOTH A | CHUCK | | | | | | | |
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| AUTION | | | | | | | TO PROCEED BY THE BOTTOM CONTROL OF CONTROL | normalismos de Mariella como empresa es a portante de Mariella con como esta de Carlos | | | | ca i i suma vanc. once o ca casa conser y casacone de Abacon de Abacon de Abacon de Cita Medica. | отта том температурання потоком и могам могам постоя на могати и могати и могат и могат и могат на могат на мог На применения на могат на могат на могат на могат на могат на могат на могат на могат на могат на могат на мога |
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SECNO CWSEL FLTRD FLIC XLCH FLMIN K*CHSL QLOB QCH QROB ALPHA SSTA ENDST

FHF FOR THE REACH = 030 WITH 18.40 DF THE REACH WITHIN 1.0 FEET ZONE FOR THE REACH = A 6

-1.23

-1.27

-1.08

.47

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-.92

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2.87

3.36

3.19

-5.02

-4.76

-2.31

-1.59

-2.52

-3.95

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WEIGHTED AVG FOR REACH -2.82

| INC | ቸጠፕል! | AVC C | LCUATION | i nata | 1 ታ ግግ ኮ | | AFRACI |
|----------|------------------------|--------|----------------|--------------|-----------------|------------|-------------------|
| NO. | <u>TOTAL</u> LENGTH | 10 [| LEVATION)[| DIFF. | WID. AVG. | FHF | PERCENT WITHIN |
| 11.78 | WENGIN | 7 A F | . J L | U L I T | AVO | 1 111 | M T 1 LI T IA |
| | 0. | | | | \$ E | С. | .057 |
| 1 | 100. | 3.60 | 3.60 | 0.00 | 0.00 | 005 | 100. |
| 2 | 200. | 3.60 | 3.59 | •01 | •01 | 005 | 100. |
| | 300. | 3.60 | 3.59 | •01 | .01 | 005 | 100. |
| | 310. 380. | | | | SE | | •116 |
| | 400. | 3.60 | 3.59 | Λ1 | | C. | .131 |
| 7 Fi | 500 | 3.60 | 3.59 | •01 •01 | •01 •01 | 005 | 100. |
| 6 | 600. | 3.60 | 3.60 | | | 005 | 100. |
| • • | 700 | 3.60 | 3.60 | 0.00 | .01 | 005 | 100. |
| A S | 800. | 3.60 | 3.60 | 0.00 | .01 | 005 005 | 100. |
| Q | 900. | 3.60 | 3.61 | | | | 100. |
| 10 | 1000. | 3.60 | | 01 | • 00 | 005 | 100. |
| 10 | 1060. | 5 • 60 | -3.61 | 01 | •00 | 005 | 100. |
| 11 | 1100. | 3.60 | 3.61 | _ 01 | SE 20 | | .257 |
| 12 | 1200. | 3.60 | 3.61 | 01 01 | • 00 | 005 | 100. |
| 13 | 1300. | 3.60 | 3.61 | | 0.00 | 005 | 100. |
| 14 | | 3.60 | | 01 | 00 | 005 | 100. |
| 15 | 1400. 1500. | | 3.61 | 01 | 00 | 005 | 100. |
| 16 | | 3.60 | 3.61 | 01 | 00 | 005 | 100. |
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| 17 | 1700. 1780. | 3.60 | 3.61 | 01 | 00 SE | 0.05 | 100. |
| 18 | 1800. | 3.60 | 3.61 | 01 | | 005 | .390 100. |
| 19 | 1900. | 3.60 | 3.63 | 03 | 00 | 005 | 100. |
| | 1980. | 3600 | 3,03 | ••• | SE | | •437 |
| 20 | 2000. | 3.61 | 3.67 | 06 | 01 | 005 | 100. |
| 21 | 2100. | 3.61 | 3.68 | 07 | 01 | 005 | 100. |
| 2.2 | 2200. | 3.61 | 3.67 | 06 | 01 | 005 | 100. |
| | 2220. | | | | SE | | .481 |
| 23 | 2300. | 3.61 | 3.67 | 06 | 01 | 005 | 100. |
| . 20 | 2300. | 3401 | 3,01 | - • • • • | SE(| | • 498 |
| 24 | 2400. | 3.61 | 3.68 | 07 | <u>-</u> •02 | 005 | 100. |
| 2.5 | 2500. | 3.61 | 3.68 | ~. 07 | 02 | 005 | 100. |
| 26 | 2600 | 3.61 | 3.69 | 08 | -•02 -•02 | 005 | 100. |
| 27 | 2700. | 3.61 | 3.69 | 08 | 02 | 005 | 100. |
| | 2710. | | | - | SE(| | . 573 |
| 28 | 2800. | 3.61 | 3,70 | 09 | 03 | 005 | 100. |
| 29 | 2900. | 3.61 | 3.70 | 09 | 03 | 005 | 100. |
| 30 | 3000. | 3.61 | 3.70 | 09 | 03 | 005 | 100. |
| 31 | 3100. | 3.61 | 3.70 | 09 | 03 | 005 | 100. |
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| 33 | 3300. | 3.61 | 3.70 | 09 | 04 | 005 | 100. |
| | 3380. | | | | SEC | | •701 |
| 34 | <u> 3400.</u> | 3.61 | 3.70 | 09 | 04 | 005 | 100. |
| | 3450. | | | | SEC | | •711 |
| 35 | 3500. | 3.61 | 3.71 | 10 | 04 | 005 | 100. |
| 36 | 3600. | 3.61 | 3.74 | 13 | 04 | 005 | 100. |
| 37 | 3700. | 3.61 | 3.78 | 17 | 05 | 005 | 100. |
| 3.8 | 3800. | 3.62 | 3.83 | 21 | 05 | 005 | 100. |
| 39 | 3900. | 3.62 | 3.87 | 25 | ~.05 | 005 | 100. |
| 40 | 4000. | 3.62 | 3.91 | ··· 29 | 06 | 005 | 100. |
| 41 | 4100. | 3.63 | 3.95 | 32 | 07 | 005 | 100. |
| | 4110. | | | <u> </u> | SEC | | .834 |
| 42 | 4200. | 3.63 | 3.98 | 35 | ~.07 | 005 | 100. |
| 43 | 4300. | 3.63 | 3.98 | 35 | 08 | | |
| 44 | | | | | | 005 | 100. |
| 45 | 4400. | 3.63 | 3.99 | = ± 36 | 09 | 005 | 100. |
| 42 | 4500. | 3.63 | 3.99 | 3 6 | 09 | 005 | 100. |

| 46 | 4600. | 3.63 | 3.99 | ~. 36 | 10 | 005 | 100. | | |
|--|-------------------------|-----------------------------|--|--|--|---------------------------------------|-----------------------|---|--|
| 47 | 4700. | 3.63 | 4.00 | 37 | 10 | 005 | 100. | | |
| | 4740. | | | | SEC | | • 952 | | |
| 4.8 | 4800. | 3.63 | 4.00 | 37 | 11 | 005 | 100. | | |
| 49 | 4800. 4900. | 3.63 | 4 O1 | 38 | SEC. | 005 | .962 | | - |
| 50 | 5000. | 3.63 | 4.01 4.02 | 3 9 | - 12 | 005 | 100. | | Printed of Printed Control of the State of t |
| 5 <u>1</u> | 5100. | 3.63 | 4.03 | 40 | -+ 12 13 | 005 | 100. | | |
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| 54 | 5400. | 3.64 | 4.06 | 42 | 14 | 005 | 100. | | |
| | 5460. | | | TO SHAPE IN THE SECOND STATE OF THE SECOND STA | SEC | | 1.096 | | |
| 55 | 5500. | 3.64 | 4.07 | 43 | 15 | 005 | 100. | | The state of the s |
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| 58 | 5800. | 3.64 | 4.07 | 43 | 16 | 005 | 100. | | |
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| 61 | 6100. | 3.64 | 4.07 | 43 | | 005 | 100. | | |
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| 64 | 6400. | 3.64 | 4.07 | 43 | | 005 | 100. | | |
| , E | 6460. | 2 / 2 | , | | SEC. | | 1.250 | | |
| 65 | 6500. | 3,63 | 4.11 | - 48 | | 005 | 100 | | |
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| <u>68</u> | 6700. 6800. | 3.56 3.52 | 4.41 | -,85 | | 005 | 99. | | |
| 0.0 | 6850. | 3.26 | 4.59 | -1.07 | 22 SEC. | 005 | 97. | | |
| 69 | 6900. | 3.52 | 5.73 | -2.21 | | 005 | 1.319 | | |
| U 7 | 6900. | J Q J C | 7413 | - € • C T | SEC. | | 96. 1.329 | | |
| 70 | 7000. | 3.58 | 6.95 | -3.37 | | 005 | 94. | | |
| . 0 | 7030. | J + JU | | J • J ; | SEC. | | 1.349 | | |
| 71 | 7100. | 3. 69 | 7.32 | =3.63 | | 005 | 93. | | |
| 72 | 7200 | 3.83 | 7.79 | -3.96 | | 005 | 93. | | |
| 73 | 7300. | 3.98 | 8.28 | -4.30 | | 005 | 92. | | |
| 74 | 7400. | 4.13 | 8.78 | -4.65 | | 005 | 85. | | |
| 75 | 7500. | 4.28 | 9.27 | -4.99 | | 005 | 64. | | Secretary and the secretary secretary and a secretary se |
| 76 | 7600. | 4.43 | 9.76 | -5.33 | | 005 | 43, | | |
| 77 | 7700. | 4.57 | 10.26 | -5.69 | | 005 | 40. | | |
| | 7770. | | | | SEC. | | 1.490 | | |
| 78 | 7800. | 4.71 | 10.71 | -6.00 | | 010 | 37. | | |
| 79 | 7900. | 4.81 | 11.06 | -6.25 | | 010 | 34. | | VATERIORI CONTROL CONT |
| 80 | 8000. | 4.89 | 11.32 | -6.43 | | 010 | 23. | | |
| 81 | 8100. | 4.97 | 11.59 | -6.62 | | 010 | 5 • | | |
| 82 | 8200. | 5.04 | 11.85 | -6.81 | | 010 | 4 • | | |
| | 8280. | | | | SEC. | | 1.583 | | |
| 83 | 8300. | 5.30 | 12.27 | -6.97 | | 010 | 4. | | |
| 200 (CC 100) (C | 8340. | | ************************************** | | SEC. | | 1.590 | | |
| | 8390. | | | | SEC. | | 1.600 | | |
| ====== | | * = 2 2 2 2 2 2 | | | | 2 2 2 2 2 | 222222222222 | | |
| | | | | ATION DIF | | | | | |
| | | | | EN BASE F 20 | 12.0 | | | | |
| JE TCHT | TED AVG FOR | S BEYON | | ∠ L - • 54 | 2.24 | | | | |
| | <u> </u> | <u> </u> | | | <u> </u> | | | | ************************************** |
| <u> </u> | | 1 = 010 | WITH | 4. [NF T | HE REACH WIT | HTN | .5 FFFT | | |
| | IR REACH | 100 1711 | | <u> </u> | THE PARTY OF THE P | · · · · · · · · · · · · · · · · · · · | - 1 | | |
| FHF FN | IR REACH | | 2 | | | | ********** | | |
| FHF FO ZONE F | OR THE REA | ACH = A | | | | | | | |
| FHF FO ZONE F | OR THE REA | ACH = A | | 2222222 | | | | | |
| FHF FO ZONE F | OR THE REA | ACH = A | | -7.16 | | 070 | 100. | | |
| FHF FO | OR THE REA | ACH = A | | | -7.16 | 070 | | | officers of the State of the St |
| FHF FO | FOR THE REASERS | ACH = A | | | -7.16 SEC. | 070 | 100. 1.604 100. | | ************************************** |
| FHF FO ZONE F | 8400. 8410. | ACH = A EBBEEBB 6.07 | 13.23 | -7.16 | -7.16 SEC. | 070 | 1.604 | | |
| FHF FO ZONE F ###### 84 | 8400. 8410. 8500. | ACH = A EBBEEBBB 6.07 | 13.23 | -7.16 -7.31 | -7.16 SEC. -7.24 -7.27 | 070 070 | 1.604 100. | | |

| 89 | 8900. | 7.18 7.25 | 14.56 14.65 | -7.38 -7.40 | -7.33 -7.34 | 075 075 | 100. 100. | | | | | | | (| |
|---|--|--|--|---|---|--|---|--|--|--|--|--|--|--|------------------|
| 90 | 9020. | | | | SE | | 1.714 | | | | | | | | |
| 91 | 9100. 9130. | 7,92 | 14.72 | -6.80 | -7.27 SE | | 1.732 | | | | | • | | 1 | |
| | 9130. | | and the second s | | SF | C | 1.733 | att gergement en lei 2000 person en en en 2000 generalen en en en 1000 person en en el 2000 person en en 2000 | | na saara 2007, sayaan ka . maanaa ah ta'aa ah maanaa ah ah ah 2007, paraman ah ah ah 2007. | CONTROL OF THE PROPERTY OF THE STATE OF THE | And the second s | recovers a Mildeletz transport of the Control of th | | |
| 22222 | E222223 | | : | VATION DIFF | ERENCE | E = = = = = = = = = = = = = = = = = = = | | - Annual Control of the Control of t | | | | | | ` | |
| | , | | BETW | EEN BASE FL | LOOD AND | | | | | | | | | | |
| | ED AVG FO | | | 2 <u>2 [</u> -1 • 8 7 | 0.2[5.50 | | | | | uperamente está de la compete persona e en la compete de la compete de la compete de la compete de la compete | ppp parametris suit in the superior sup | AdvailがPPC essestAll eronousをEALをESALvectoressAlleron | | restrict Main reasons erest Mainten areas considered Side (Consideration) | |
| FHF FC | R REACH | 2 = 075 | WITH : | 100.[DF TH | HE REACH W | ITHIN 2 | 2.0 FEET | | - 1111 | | , 1000 | | | | |
| ZONE E | OR THE RI | FACH = Al | . <u>5</u> | 2222222222 | 22222222 | 222222 | ********** | | | | | | | | . |
| | | | 44 70 | E 04 | -5,94 | 060 | 100. | | | | | | | | |
| 92 93 | 9200. 9300. | 8 • 84 9 • 22 | 14.78 14.86 | -5.94 -5.64 | -5.79 | 060 | 99. S 200 process - 200 pro | Statement of Mahamatan and Statement of Stat | enteren sekt 1880-til et enteren och sekt til til ett enteren sekt til til til ett enteren sekt til til til ti | a minimizer the second | AND THE RESIDENCE OF THE PROPERTY OF THE PROPE | Communication of the second se | mandel 12 of the transfer of the second constitution of the second control of the second control of the second | egeneral de de l'accesso d'accessos de l'embolica de l'accesso () de embolica () escalable () escalable () | |
| 94 | 9400. | 9.39 | 14.95 | -5.56 | -5.71 | 055 055 | 99 . 99. | \ | | | | ···· | | · · · · · · · · · · · · · · · · · · · | (|
| 95 | 9500 | 9.56 9.73 | 15.04 15.13 | <u>-5.48</u> -5.40 | <u>-5.66</u> -5.60 | <u>055</u> 055 | 99. | | | | | | | | ! |
| 96 97 | 9600. 9700. | 9.13 | 15.21 | -5.31 | -5.56 | 055 | 99. | | | | | | | (| (|
| 98 | 9800. | 10.07 | 15.30 | -5.23 -5.15 | -5.51 -5.46 | 055 055 | 99 . 99 . | | | A SECTION CONTRACTOR OF THE CO | ###################################### | one in the territory of the second of the se | | bosznamony) www.attilmot(() c= −0 km/mkt/c∎ | |
| 99 | 9900. 9931. | 10.24 | 15,39 | AND THE RESIDENCE OF THE PARTY | SE | C • | 1.884 | | | | | | | (| (|
| | 9932. | | | | SE SE | <u>C.</u> | 1.885 1.895 | | | | | | | | |
| | 9992. | | | | | | 10015 | / | | | | | | | ϵ |
| 22552 | ******* | | ELE | VATION DIF | FERENCE | | | | | | | ATTERNAL AND THE STREET AND THE STRE | nggo Allika ang kanganga 1672 kita ang kanga a pakkananana. | | |
| | | AND THE PARTY OF T | ALL DE LA COLONIA DE LA COLONI | FEN BASE E | 0 • 2 C | | | мер под под при при на при на при на при на при на при на при на при на при на при на при на при на при на при На при на | MANEYPOR AT ANNU BET TETERIOR OF PROCESSED LANGUAGE CONTRACTOR AND ANNUAL CONTRACTOR SETTING AND ANNUAL CONTRACTOR AND ANNUAL CONTRA | No. of the state o | - | | | 1 | (|
| MC TOUT | TED AVG F | OR REACH | 1.0€ =5.46 | -1 • 1 <u>0</u> | 4.88 | | | | | | | | | | |
| | | | | | | | _ | \ | | | | | | | |
| 1 | | | 1140 40 11 | 00 f 05 T | HE DEACH N | ITTHTN | 1.0 FFFT | \ | | | | | | | (|
| 70NE | CHO THE D | FACH = A | 11 | 99.[OF T | | | | | _ | | 2% | 5-0 | % | | (|
| 70NE | CHO THE D | FACH = A | 11 | | | | 1.0 FEET | | Combine | 10% | 2% | ٥٥ | % | ner Add Assessment (1985) in Add Assessment (1985) in Add Assessment (1985) in Add Assessment (1985) in Add As | (|
| ZONE | FOR THE R | EACH = A | 11 | | | | 100. | | . Combine | | | | | | (|
| 70NE | CHO THE D | FACH = A | 11 ======= 15.45 15.48 | -4.97 -4.80 | -4.97 -4.89 | 050 050 | 100. | | | | | | | | (|
| 100 101 102 | 10000. 10100. 10200. | 10.48 10.68 10.78 | 11 ======= 15.45 15.48 15.50 | -4.97 -4.80 -4.72 | -4.97 -4.89 -4.83 | 050 050 050 | 100. 100. 100. | | | | | | | within 10 | (() |
| ZONE | 10000. 10100. 10200. 10300. | 10.48 10.68 | 11 ======= 15.45 15.48 | -4.97 -4.80 | -4.97 -4.89 -4.83 -4.79 | 050 050 050 050 | 100. 100. 100. 100. 100. | | | | | | | within 1.0 | (((, |
| 100 101 102 | 10000. 10100. 10200. 10300. 10342. 10400. | 10.48 10.68 10.78 | 11 ======= 15.45 15.48 15.50 | -4.97 -4.80 -4.72 | -4.97 -4.89 -4.83 -4.79 SF | 050 050 050 050 050 | 100. 100. 100. 100. 100. 1.960 100. | | | | | | | within 1.0 | ((. |
| 100 101 102 103 | 10000. 10100. 10200. 10342. 10400. 10452. | 10.48 10.68 10.78 10.87 | 11 15.45 15.48 15.50 15.53 | -4.97 -4.80 -4.72 -4.66 | -4.97 -4.89 -4.83 -4.79 SE -4.75 | 050 050 050 050 050 050 | 100. 100. 100. 100. 100. 1.960 100. 1.979 1.980 | | Combine FHF feet for Zor | | | | | within 1:0 | ((· |
| 100 101 102 103 | 10000. 10100. 10200. 10300. 10342. 10400. | 10.48 10.68 10.78 10.87 | 15.45 15.48 15.50 15.53 | -4.97 -4.80 -4.72 -4.66 -4.58 | -4.97 -4.89 -4.83 -4.79 SE -4.75 | 050 050 050 050 050 050 | 100. 100. 100. 100. 100. 1.960 100. 1.979 | | | | | | | within 1.0 | (() · |
| 100 101 102 103 | 10000. 10100. 10200. 10342. 10400. 10452. 10453. | 10.48 10.68 10.78 10.87 | 11 ======= 15.45 15.48 15.50 15.53 15.54 | -4.97 -4.80 -4.72 -4.66 -4.58 | -4.97 -4.89 -4.83 -4.79 SE -4.75 SE | 050 050 050 050 050 050 | 100. 100. 100. 100. 100. 1.960 100. 1.979 1.980 | | | | | | | within 10 | (|
| 100 101 102 103 | 10000. 10100. 10200. 10342. 10400. 10452. 10453. | 10.48 10.68 10.78 10.87 | 11 ======= 15.45 15.48 15.50 15.53 15.54 | -4.97 -4.80 -4.72 -4.66 -4.58 VATION DIF | -4.97 -4.89 -4.83 -4.79 SE -4.75 SE FERENCE LOOD AND | 050 050 050 050 050 050 | 100. 100. 100. 100. 100. 1.960 100. 1.979 1.980 | | | | | | | wthin 1.0 | (|
| 100 101 102 103 104 | 10000. 10100. 10200. 10342. 10400. 10452. 10453. | 10.48 10.68 10.78 10.87 | 11 15.45 15.48 15.50 15.53 15.54 ELE RETW 105 | -4.97 -4.80 -4.72 -4.66 -4.58 VATION DIF | -4.97 -4.89 -4.83 -4.79 SE -4.75 SE SE FERENCE LOOD AND | 050 050 050 050 050 050 | 100. 100. 100. 100. 100. 1.960 100. 1.979 1.980 | | | | | | | within 1.0 | (() · |
| 100 101 102 103 104 | 10000. 10100. 10200. 10300. 10400. 10452. 10453. ======== | 10.48 10.68 10.78 10.96 | 11 ======= 15.45 15.48 15.50 15.53 15.54 ==================================== | -4.97 -4.80 -4.72 -4.66 -4.58 VATION DIF VEEN BASE F 21 -1.02 | -4.97 -4.89 -4.83 -4.79 SE -4.75 SE FERENCE LOOD AND 0.2[4.60 | 050 050 050 050 050 050 050 EC. | 100. 100. 100. 100. 100. 1.960. 1.979. 1.980. | | | | | | | within 1.0 | |
| 100 101 102 103 104 EFF F | 10000. 10100. 10200. 10300. 10452. 10453. TED AVG F | 10.48 10.68 10.78 10.87 10.96 | 11 15.45 15.48 15.50 15.53 15.54 ELE RETW 101 -4.75 | -4.97 -4.80 -4.72 -4.66 -4.58 EVATION DIF JEEN BASE F 2[-1.02 | -4.97 -4.89 -4.83 -4.79 -5.55 -4.75 -5.65 -6.75 | 050 050 050 050 050 050 EC. | 100. 100. 100. 100. 100. 1.960. 1.979. 1.980. **EXEMPLE EXELUTE 1.00 FEET | | | | | | | within 10 | |
| 100 101 102 103 104 EFF F | 10000. 10100. 10200. 10300. 10452. 10453. TED AVG F | 10.48 10.68 10.78 10.87 10.96 | 11 15.45 15.48 15.50 15.53 15.54 ELE RETW 101 -4.75 | -4.97 -4.80 -4.72 -4.66 -4.58 EVATION DIF JEEN BASE F 2[-1.02 | -4.97 -4.89 -4.83 -4.79 SE -4.75 SE FERENCE LOOD AND 0.2[4.60 HE REACH M | 050 050 050 050 050 C. 050 EC. | 100. 100. 100. 100. 100. 1.960. 1.979. 1.980. EERREEREEREERE | | | | | | | within 10 | |
| 100 101 102 103 104 WEIGH | 10000. 10100. 10200. 10300. 10452. 10453. TED AVG F | 10.48 10.68 10.78 10.96 10.96 ERREREE 11.02 | 11 15.45 15.48 15.50 15.53 15.54 ELE RETW 10! -4.75 0 WITH 10 ======== | -4.97 -4.80 -4.72 -4.66 -4.58 VATION DIF FEN BASE F 2[-1.02 100.[OF T | -4.97 -4.89 -4.83 -4.79 SE -4.75 SE SE FERENCE LODD AND 0.2[4.60 HE REACH V | 050 050 050 050 050 050 050 050 050 050 | 100. 100. 100. 100. 100. 1.960. 1.979. 1.980. EERRERERERERERERERERERERERERERERERERER | | | | | | | within 10 | |
| 100 101 102 103 104 WEIGH FHF F ZONE ==================================== | 10000. 10100. 10200. 10300. 10342. 10400. 10452. 10453. ==================================== | 10.48 10.68 10.78 10.87 10.96 ERREACH 4 = 05 EACH = A | 15.45 15.48 15.50 15.53 15.54 ELE RETW 101 -4.75 0 WITH 10 ================================== | -4.97 -4.80 -4.72 -4.66 -4.58 EVATION DIF FEN BASE F 2[-1.02 100.[OF T | -4.97 -4.89 -4.83 -4.79 -5.5 -4.75 -4.75 -4.60 HE REACH V | 050 050 050 050 050 050 050 050 050 050 | 100. 100. 100. 100. 100. 1.960. 1.979. 1.980. EERREEREEREERE | | | | | | | within 10 | |
| 100 101 102 103 104 WEIGH FHF F ZONE ===== 105 106 107 | 10000. 10100. 10200. 10300. 10342. 10400. 10452. 10453. =================================== | 10.48 10.68 10.78 10.96 10.96 EXERCE 4 = 05 EACH = A EXERCE 11.02 11.12 11.26 | 11 15.45 15.48 15.50 15.53 15.54 ELE RETW 10! -4.75 0 WITH 10 ======== | -4.97 -4.80 -4.72 -4.66 -4.58 VATION DIF FEN BASE F 2[-1.02 100.[OF T | -4.97 -4.89 -4.83 -4.79 -4.75 -4.75 -4.75 -4.60 HE REACH W | 050 050 050 050 050 050 C. 050 EC. 20222222 VITHIN | 100. 100. 100. 100. 100. 1.960. 1.979. 1.980. ************************************ | | | | | | | within 100 | |
| 100 101 102 103 104 WEIGH FHF F ZONE ==================================== | 10000. 10100. 10200. 10300. 10342. 10400. 10452. 10453. =================================== | 10.48 10.68 10.78 10.87 10.96 ERREACH 4 = 05 EACH = A | 15.45 15.48 15.50 15.53 15.54 ELE RETW 101 -4.75 0 WITH 10 ================================== | -4.97 -4.80 -4.72 -4.66 -4.58 EXATION DIF FEN BASE F 2[-1.02 100.[OF T | -4.97 -4.89 -4.83 -4.79 SE -4.75 SE SE SE FERENCE LODD AND 0.2[4.60 HE REACH V | 050 050 050 050 050 050 050 050 050 050 | 100. 100. 100. 100. 100. 100. 1.960. 1.979. 1.980. EXERCEPEEEEEEEEEEEEEEEEEEEEEEEEEEEEEEEEE | | | | | | | | (|
| 100 101 102 103 104 WEIGH FHF F ZONE ===== 105 106 107 | 10000. 10100. 10200. 10300. 10342. 10400. 10452. 10453. =================================== | 10.48 10.68 10.78 10.96 10.96 EXERCE 4 = 05 EACH = A EXERCE 11.02 11.12 11.26 | 15.45 15.48 15.50 15.53 15.54 ELE RETW 101 -4.75 0 WITH 10 ================================== | -4.97 -4.80 -4.72 -4.66 -4.58 EXATION DIF FEN BASE F 2[-1.02 100.[OF T | -4.97 -4.89 -4.83 -4.79 -4.75 -4.75 -4.75 -4.60 HE REACH V | 050 050 050 050 050 050 C. 050 EC. 20222222 VITHIN | 100. 100. 100. 100. 100. 1.960. 1.979. 1.980. EERRERERERERERERERERERERERERERERERERER | | | | | | | | |
| 100 101 102 103 104 EFF F ZONE EFF F 20NE 105 106 107 | 10000. 10100. 10200. 10300. 10342. 10400. 10452. 10453. =================================== | 10.48 10.68 10.78 10.96 10.96 EXERCE 4 = 05 EACH = A EXERCE 11.02 11.12 11.26 | 11 15.45 15.48 15.50 15.53 15.54 ELE RETW 101 -4.75 0 WITH 10 ======== 15.64 15.76 15.78 15.81 | -4.97 -4.80 -4.72 -4.66 -4.58 VATION DIF FEN RASE F 21 -1.02 100.[OF T | -4.97 -4.89 -4.83 -4.79 -5.5 -4.75 -4.75 -4.60 HE REACH V | 050 050 050 050 050 050 050 050 050 050 | 100. 100. 100. 100. 100. 1.960. 1.979. 1.980. EEEEEEEEEEEEEEEEEEEEEEEEEEEEEEEEEEEE | | | | | | | | |
| 100 101 102 103 104 WEIGH FHF F ZONE ====== 105 106 107 108 | 10000. 10100. 10200. 10300. 10342. 10400. 10452. 10453. ======== TED AVG F OR REACH FOR THE R ======== 10500. 10600. 10600. 10853. 10854. 10894. | 10.48 10.68 10.78 10.87 10.96 EXEMPTE 11.02 11.12 11.26 11.39 | 11 15.45 15.48 15.50 15.53 15.54 ELE RETW 101 -4.75 0 WITH 10 ================================== | -4.97 -4.80 -4.72 -4.66 -4.58 VATION DIF VEEN BASE F 21 -1.02 100.1 OF T | -4.97 -4.89 -4.83 -4.79 SE -4.75 SE SE SE SE SE SE SE SE SE SE SE SE SE | 050 050 050 050 050 050 050 050 050 050 | 100. 100. 100. 100. 100. 1.960. 1.979. 1.980. EERRERERERERERERERERERERERERERERERERER | | | | | | | | (|

| 112 11200. 11.81 16.80 -4.99 -4.72 045 113 11300. 11.82 16.83 -5.01 -4.76 050 | 100. |
|---|--------------------------|
| 11314. SEC. 3 | 2.141 |
| | 2.150 2.157 |
| 114 11400. 13.46 17.11 -3.65 -4.65 045 11419. SEC. 2 | 2.161 |
| 115 11500. 15.52 17.52 -2.00 -4.40 045 | 99. |
| 116 11600. 16.03 17.84 -1.81 -4.19 040 117 11700. 16.20 18.17 -1.97 -4.02 040 | 98. 97. |
| 118 11800. 16.36 18.50 -2.14 -3.88 040 | 93. |
| | 2.265 |
| ELEVATION DIFFERENCE | : \$ 2 8 2 8 2 2 2 2 2 3 |
| BETWEEN BASE FLOOD AND 10[2[0.2[| |
| WEIGHTED AVG FOR REACH -3.7880 4.12 | |
| FHF FOR REACH 5 = 040 WITH 92. [DF THE REACH WITHIN 1.0 |) FEET |
| ZONE FOR THE REACH = A 8 | ********** |
| 120 12000. 16.77 19.23 -2.46 -2.46 025 | 100. |
| 121 12100, 17.34 19.90 -2.56 -2.51 025 | 100. |
| 122 12800. 18.17 20.78 -2.61 -2.54 025 123 12300. 19.00 21.67 -2.67 -2.58 025 | 100. |
| 125 12300 14.00 21.87 -2.87 -2.58 025 124 12400 19.83 22.56 -2.73 -2.61 025 | 100. |
| 125 12500. 80.66 23.44 -2.78 -2.64 025 126 12600. 21.49 24.33 -2.84 -2.66 025 | 100. |
| 126 12600. 21.49 24.33 -2.84 -2.66 025 127 12700. 22.38 25.22 -2.90 -2.69 025 | 100 |
| 128 12800. 23.15 26.10 -2.95 -2.72 025 | 100. |
| 129 12900. 23.98 26.99 -3.01 -2.75 030 130 13000. 24.81 27.88 -3.07 -2.78 030 | 100. |
| 131 13100. 25.64 28.76 -3.12 -2.81 030 | 100. |
| 132 13200. 26.47 29.65 2.18 -2.84 030 | 100 |
| 133 13300. 27.30 30.54 -3.24 -2.87 030 134 13400. 28.13 31.42 -3.29 -2.89 030 | 100. |
| 135 13500. 28.96 32.31 -3.35 -2.92 030 | 100. |
| <u>136</u> <u>13600.</u> <u>29.79</u> <u>33.20</u> <u>-3.41</u> <u>-2.95</u> <u>030</u> | 100. |
| 137 13700. 30.62 24.08 -3.46 2.98 030 138 13800. 31.45 34.97 -3.52 -3.81 030 | 100. |
| 139 13900. 32.28 35.86 -3.58 -3.04 030 | 100. |
| 140 14000. 33.11 36.74 -3.63 -3.06 030 141 14100. 33.94 37.63 -3.69 -3.09 030 | 100. |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | 100. |
| 5 143 14300 35.60 39.40 -3.80 -3.15 030 | 100. |
| 144 14400. 36.43 40.29 -3.86 -3.18 030 145 14500. 37.26 41.18 -3.92 -3.21 030 | 100. |
| 14509. SEC. 2 | .788 |
| ELEVATION DIFFERENCE | |
| BETWEEN BASE FLOOD AND | |
| 10[2[0.2[WEIGHTED AVG FOR REACH -3.21 -1.03 3.40 | |
| FHE FOR REACH 6 = 030 WITH 100. C OF THE REACH WITHIN 1.0 | FEET |
| ZONE FOR THE REACH = A 6 | zeszezzz / |
| 1// 1//00 27 20 /1 /0 2 0/ 2 0/ 2/2 | Combine |
| 146 14600. 37.72 41.68 -3.96 -3.96 040 147 14700. 37.76 41.76 -4.00 -3.98 040 | 100. |
| 148 14800. 37.77 41.80 -4.03 -4.00 040 | 100. |
| 149 14900. 37.78 41.84 -4.06 -4.01 040 150 15000. 37.78 41.88 -4.10 -4.03 040 | 100. |
| OPO COAP OLATE OLATE ACCOUNT OCA | |

| 151 15100. 37.79 41.92 -4.13 -4.05 040 100. | |
|--|--------------------------|
| 152 15200. 37.80 41.96 -4.16 -4.06 040 100. | 10% 2% 0.2% |
| 153 15300. 37.81 42.00 -4.19 -4.08 040 100. 154 15400. 37.81 42.04 -4.23 -4.10 040 100. | |
| 155 15500. 37.82 42.08 -4.26 -4.11 040 100. | |
| <u>156 15600. 37.83 42.12 -4.29 -4.13 040 100.</u> | -4.11 -1.48 3.76 |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | (" |
| 159 15900. 37.85 42.25 -4.40 -4.18 040 100. | EUR E D / A - 10 |
| 160 16000. 37.86 42.29 -4.43 -4.20 040 100. 161 16100. 37.87 42.33 -4.46 -4.21 040 100. | FHF For Reach 4 = 040 |
| 16139. SEC. 3.096 | 100% within 1.0 feet for |
| 162 16200. 37.96 42.43 -4.47 -4.23 040 100. 163 16300. 38.20 42.63 -4.43 -4.24 040 100. | Zone A8 |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | Lone Ao |
| 165 16500. 38.79 43.12 -4.33 -4.25 045 100. | |
| 166 16600. 39.08 43.36 -4.28 -4.25 045 100. 167 16700. 39.38 43.60 -4.22 -4.25 045 100. | |
| 168 16800. 39.67 43.84 -4.17 -4.25 045 100. | |
| 169 16900。 39.97 44.08 -4.11 -4.24 040 100。 170 17000。 40.26 44.33 -4.07 -4.23 040 100。 | |
| <u>171 17100. 40.56 44.57 -4.01 -4.23 040 100.</u> | |
| 172 17200. 40.85 44.81 -3.96 -4.22 040 100. 173 17300. 41.15 45.05 -3.90 -4.20 040 100. | |
| 173 17300, 41,15 45,05 -3,90 -4,20 040 100. 174 17400, 41,44 45,29 -3,85 -4,19 040 100. | |
| 17449. SEC. 3.351 | (|
| 175 17500. 41.85 45.71 -3.86 -4.18 040 100. 176 17600. 42.49 46.49 -4.00 -4.18 040 100. | |
| 177 17700. 43.24 47.43 -4.19 -4.18 040 100. | |
| 178 17800. 43.99 48.38 -4.39 -4.18 040 100. 179 17900. 44.74 49.33 -4.59 -4.19 040 100. | |
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Draft Memorandum

SRF No. 16924.00

To: Tom Johnson, PE, PTOE

Labella Associates

From: Phil Kulis, PE, Senior Project Manager

Tom Sachi, PE, Senior Project Manager

Ashley Sherry, PE, Engineer III

Date: May 31, 2024

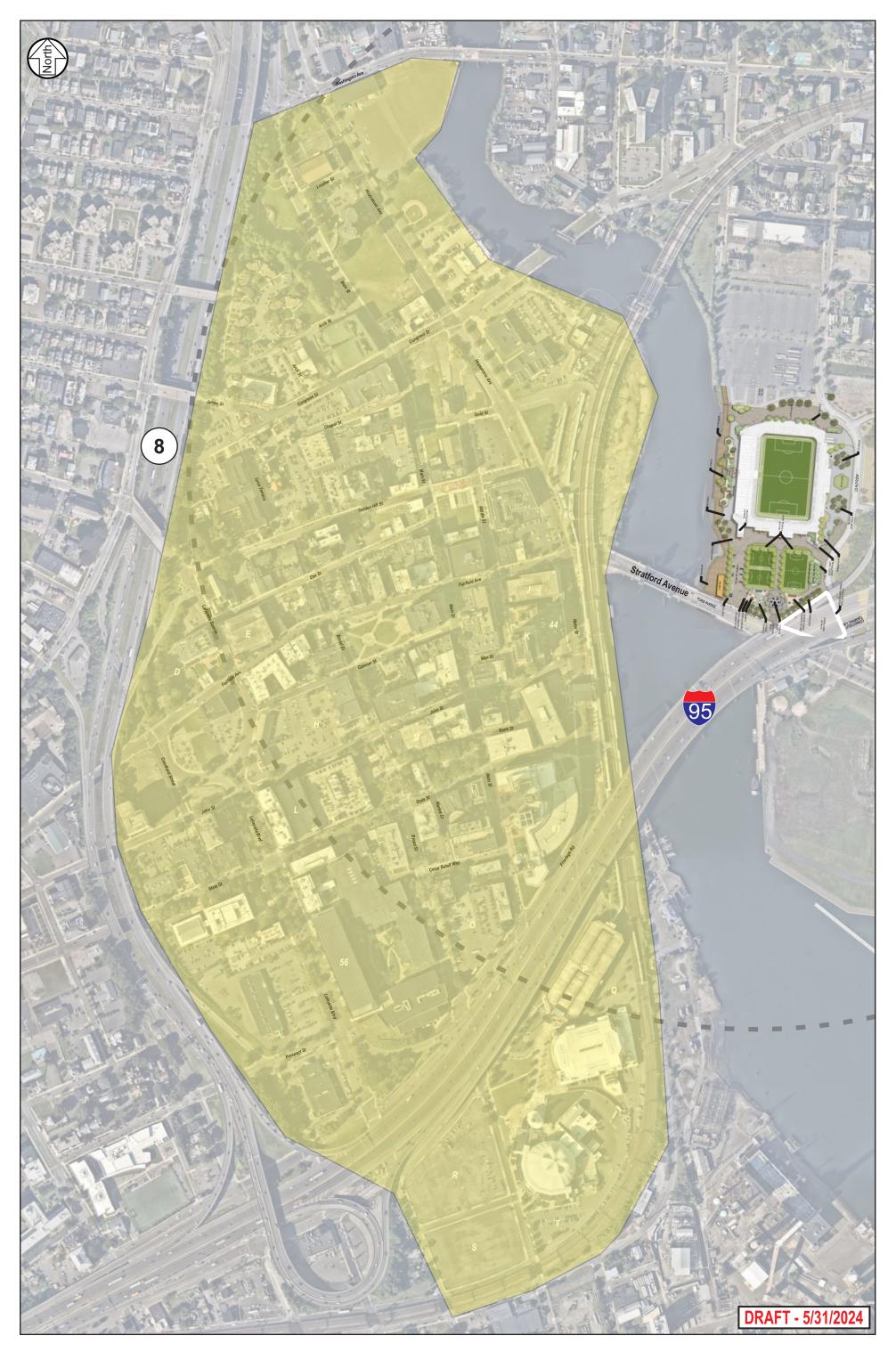
Subject: Bridgeport Soccer Stadium Parking Study – Existing Conditions

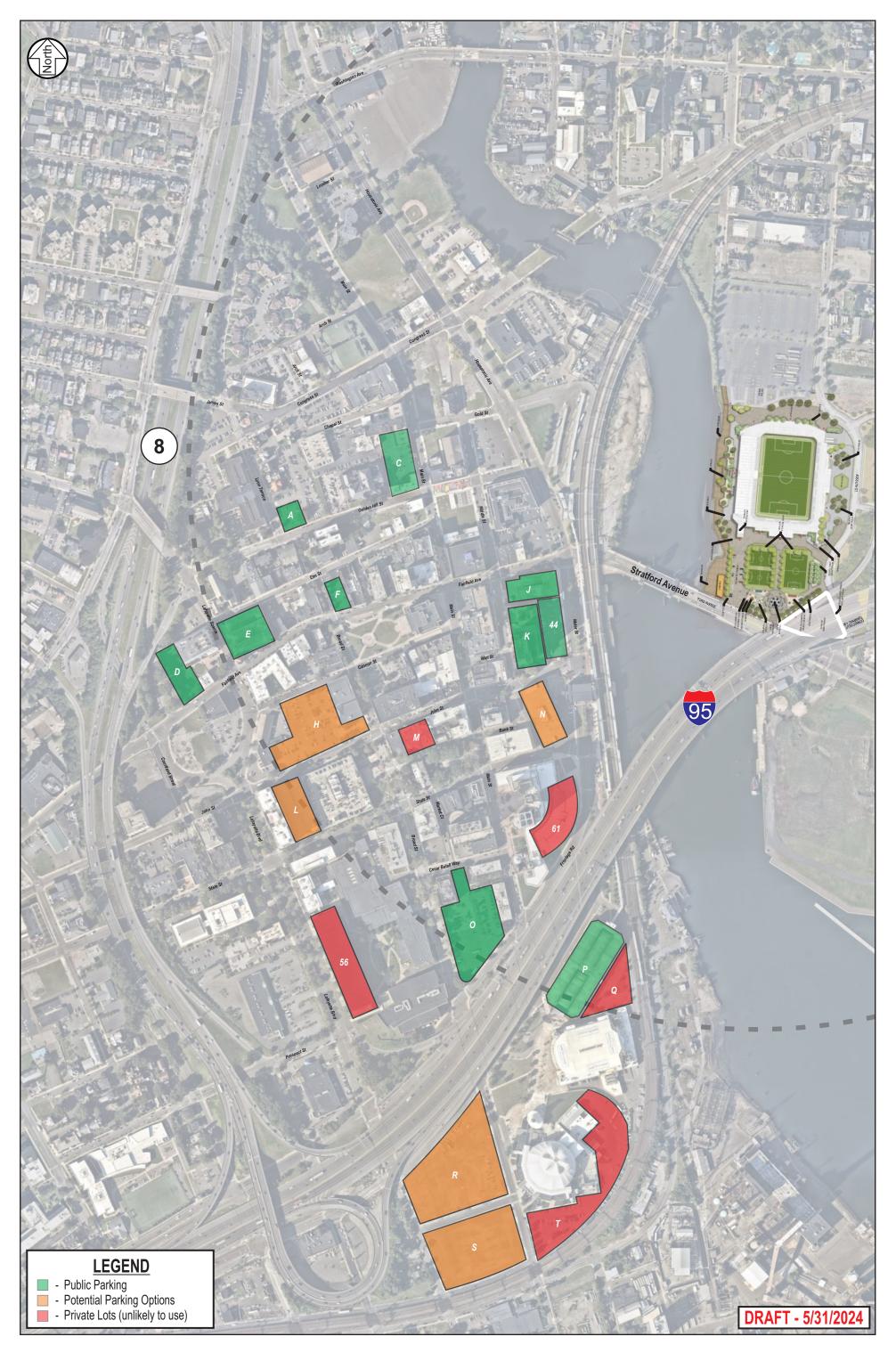
Introduction

SRF has completed a study of the existing parking conditions in Downtown Bridgeport, Connecticut in support of a future detailed parking analysis for stadium events at the proposed Bridgeport Soccer Stadium (see Figure 1). The proposed stadium is located on the east side of the Pequonnock River, while the majority of the parking will be located on the west side of the river in the core of Downtown Bridgeport. It is expected that the majority of attendees will need to cross the Stratford Avenue bridge to access parking and transit options. Therefore, a detailed review of the existing parking options located in Downtown was completed. Note, given the lack of public parking options on the east side of the river near the stadium, there was not a detailed study completed in this area. The boundaries of the parking study were approximately the Pequonnock River to the east, Washington Avenue to the north, Highway 8 to the west and the railroad tracks to the south, as shown in Figure 1. Note, this study area approximately reflects a one-half mile walkshed from the stadium, which is a typical walk that could be expected from an event attendee. Note, a few larger parking areas are shown outside of the one-half mile radius from the stadium but were included within the analysis. The main objectives of this study are to review the existing parking utilization within the project area, document locations that may be suitable for event parking, and plan for future parking analysis necessary for stadium events. The following assumptions and data is offered for your consideration.

Existing Conditions

The existing conditions were reviewed to establish a baseline of the existing parking supply and demand during a typical event timeframe. It was assumed that events would occur on either a weeknight or Saturday evening at 7:00 p.m. Therefore, parking data was collected between approximately 6:00 and 7:00 p.m. when event attendees would be expected to arrive. The parking lot and garage locations shown in Figure 2 detail all of the public or potential event parking opportunities that were identified. Additionally, on-street parking was collected to understand the magnitude of parking available along City roadways.





Parking Utilization Survey

Parking utilization surveys were collected on Wednesday, May 1 and Saturday, May 4, 2024 between approximately 6:00 and 7:00 p.m. at the surface lots, garages, and on-street locations shown in Figure 2. This information will serve as the baseline of parking demand at these locations on a typical weekday evening and Saturday evening. Note, the University of Bridgeport did have an afternoon commencement ceremony occurring at the Hartford Healthcare Amphitheater on Saturday. While the majority of attendees had left by 6:00 p.m., the parking lots surrounding the amphitheater were restricted to use by event attendees only. Note, this is a one time a year event and should be considered when scheduling potential soccer matches at the proposed stadium. Results of the parking utilization surveys are detailed within Table 1 for the public parking locations.

Table 1. Parking Utilization Survey - Public Parking Lots

| | | | Parking D | emand | | | |
|---------------------------|---------|---------|---------------------|---------|---------------------|-----------|----------|
| Lot ID | Parking | Wednesd | ay, May 1 | Saturda | y, May 4 | Weeknight | Saturday |
| | Supply | 6:00 PM | Percent Utilized | 6:00 PM | Percent Utilized | Surplus | Surplus |
| A | 32 | 9 | 28% | 11 | 34% | 23 | 21 |
| С | 65 | 21 | 32% | 20 | 31% | 44 | 45 |
| D | 50 | 33 | 66% | 15 | 30% | 17 | 35 |
| Е | 895 | 58 | 6% | 52 | 6% | 837 | 843 |
| F | 32 | 14 | 44% | 17 | 53% | 18 | 15 |
| J | 596 | 184 | 31% | 197 | 33% | 412 | 399 |
| 44 | 89 | 15 | 17% | 10 | 11% | 74 | 79 |
| K (1) | 318 | 37 | 12% | 0 | 0% | 281 | 318 |
| 0 | 250 | 39 | 16% | 56 | 22% | 211 | 194 |
| P (1) | 1,400 | 272 | 19% | 0 | 0% | 1,128 | 1,400 |
| Total Lots and Garages | 3,727 | 682 | 18% | 378 | 10% | 3,045 | 3,349 |
| On-Street | 890 | 478 | 54% | 536 | 60% | 412 | 354 |
| Total Public Parking | 4,617 | 1,160 | 25% | 914 | 20% | 3,457 | 3,703 |

⁽¹⁾ Typically closed on weekends, but infrastructure is set up for events

As shown in Table 1, the public parking facilities in Downtown are currently between 20 to 25 percent utilized during the Saturday and weekday evening timeframes, respectively. During a weeknight evening, this would result in a surplus of 3,457 parking stalls and on a Saturday evening there is a surplus of 3,703 parking stalls. Note that on-street parking is between 54 to 60 percent utilized.

There are two (2) parking garages that were included in the analysis were observed to be closed on the weekends. Lot K, or Park City Plaza Garage, which is located near the Stratford Avenue and Water Street intersection, is one of the locations that is closed. Additionally, Lot P, or the Harbor Yard Transit Garage, located adjacent to Total Mortgage Arena is noted to be closed on weekends except for events. It is recommended that the development team begin discussions with these garage operators about potential use for weekend events.

In addition to the public parking locations shown in green on Figure 2 and Table 1, there were several other parking locations identified that have the potential to be utilized for event parking (shown in orange in Figure 2). These locations were either only noted as being used for events or had some public/private components. The parking utilization is shown in Table 2.

Table 2. Parking Utilization Survey - Potential Parking Locations

| | | | Parking Demand | | | | |
|------------------------------|---------|------------------|---------------------|-----------------|---------------------|-----------|----------|
| Lot ID | Parking | Wednesday, May 1 | | Saturday, May 4 | | Weeknight | Saturday |
| | Supply | 6:00 PM | Percent Utilized | 6:00 PM | Percent Utilized | Surplus | Surplus |
| Н | 354 | 20 | 6% | 6 | 2% | 334 | 348 |
| L (1) | 727 | 136 | 19% | 0 | 0% | 591 | 727 |
| R (2) | 494 | 0 | 0% | 0 | 0% | 494 | 494 |
| S (2) | 366 | 0 | 0% | 0 | 0% | 366 | 366 |
| N (3) | 469 | 34 | 7% | 16 | 3% | 435 | 453 |
| Total Garages and Lots | 2,410 | 190 | 8% | 22 | 0.9% | 2,220 | 2,388 |

- (1) Lot is closed on evenings and weekends (monthly permits only)
- (2) Lots are closed for events only
- (3) Lot restricted to monthly pass users only. Parking ticket machine was broken during collection.

At the potential locations, there is a parking demand between one (1) to eight (8) percent during the Saturday and weekday evenings, respectively. However, it should be noted that these lots may not be used for event parking. Lot H, was observed to be partially public and partially private parking. Lot L, or the Wright Building Garage, was observed to close to public parking in the evenings and weekends, with a monthly parking pass required to open the gate. Lots R and S, surface lots by the arena, were gated off for event parking only, and lastly, Lot N, or the Bridgeport Transit Garage, was restricted to monthly pass users only as the parking ticket machine was out of order. There is potential that if additional parking options were needed to accommodate event parking at the proposed Bridgeport Soccer Stadium, that these lots could be explored as potential options.

Preliminary Future Parking Demand

A high level estimate the potential parking demand for an event was completed by Labella. Based on their trip generation estimates, the following preliminary parking demand was determined for a 10,000 person event:

- Assumed 10 percent of attendees are walking/biking trips from nearby neighborhoods.
- Of the 9,000 remaining attendees, it was assumed that 20 percent will utilize transit and 80 percent will utilize vehicles. This results in 1,800 transit attendees and 7,200 auto attendees.
- With the 7,200 auto trips, it was assumed that there is a vehicle occupancy of 2.5 persons per vehicle, resulting in the need to park 2,880 vehicles.
- It is expected that 570 on-site parking stalls will be provided, leaving the <u>remaining 2,310 vehicles</u> to park within Downtown Bridgeport.

Based on this analysis, a preliminary parking demand estimate was completed using the public parking locations in Table 1. The results of the preliminary analysis are shown in Table 3, detailing the potential surplus or deficits that may occur. Note, an analysis was done for the Saturday event for two (2) scenarios, with and without Lots K and P, which were noted to be closed on Saturdays.

Table 3. Parking Utilization Survey - Potential Parking Locations

| Parking Analysis | Weekday Evening | Saturday Evening (all public locations) | Saturday Evening (without closed garages) |
|----------------------------|-----------------|--|---|
| Existing Parking Demand | 1,160 | 914 | 914 |
| Expected Event Demand | 2,310 | 2,310 | 2,310 |
| Total Demand | 3,470 | 3,224 | 3,224 |
| Total Supply | 4,617 | 4,617 | 2,899 |
| Expected Surplus/(Deficit) | 1,147 | 1,393 | (-325) |

Based on the results of the preliminary parking analysis, it is expected that with the parking locations listed in Table 1, there will be a surplus of 1,147 parking stalls on a weekday evening event. If Lots K and P are available for use on a Saturday for an event there is expected to be a surplus of 1,393 parking stalls. However, if those lots are closed, there would be a 325 parking stall deficit during an event. Therefore, exploration of use of Lots K and P is recommended to accommodate event parking demands for the proposed Bridgeport Soccer Stadium. With those lots included in the analysis, there is not currently a need to explore use of the lots within Table 2.

Next Steps

Further details of the parking study are expected to be completed in the future. This is expected to include further detailed collection reports of the data collected in the field and any analysis updates as additional information from the development and Labella teams is determined. This memo is intended to provide a review of the initial data collection and preliminary parking findings to allow the traffic study to move forward with distributing auto trips to the roadway network in any associated traffic modeling efforts. As further study efforts and event management planning efforts are completed, the following items are recommended to be considered by the project team:

- Contact the owners/operators of Lot K, Park City Parking Garage and Lot P, Harbor Yard Transit Garage.
 - o Lot K is operated by Imperial Parking Company
 - o Lot P is operated by Connecticut Department of Transportation.
- Given Lot K's location (immediately adjacent to the bridge were attendees cross into Downtown),
 there will likely be a high desire by fans for use of this garage. Additionally, Lot P is set up to
 handle large event parking demands given its location and use for arena and amphitheater events.
 Both of these garages would be prime parking locations for the proposed Bridgeport Soccer
 Stadium event attendees.
- Given the location of the majority of the parking needed for events, the transit platforms, and bars and restaurants within the area, there is expected to be over 7,500 people crossing the Stratford Avenue bridge before and after events.
 - With narrow sidewalks on the lift portion of the bridge, there is expected to be significant issues crossing that many people before/after a game.
 - o Additional considerations of closing lanes of traffic on the bridge will be necessary to safely and efficiently transport people from the stadium side to Downtown before and after games.
- Consideration should be given to avoid scheduling games during conflicting events at either Total Mortgage Arena or Hartford Healthcare Amphitheater, as parking demands may overlap and cause a potential parking deficit.

Prepared For:

Swanston Organization. LLC. 750 E Main St Stamford, CT 06902

Submitted by:

LaBella Associates 400 S Tryon St, Suite 1300 Charlotte, NC 28285



Bridgeport CT MLS Stadium Engineering Report

30% REPORT JUNE 19, 2024 2230111

| Bridgeport CT MLS Stadium | VERSION: | 30% Design |
|---------------------------|----------|---------------|
| Engineering Report | DATE: | June 19, 2024 |

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| Engineering Report | DATE: | June 19, 2024 |

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1. EXECUTIVE SUMMARY

This Engineering Report (Report) provides engineering information for proposed water, sewer, and stormwater infrastructure improvements that are necessary to serve a proposed stadium. This Report will be submitted to regulatory agencies for approval and permitting.



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2. PROJECT BACKGROUND AND HISTORY

2.1 Site Information

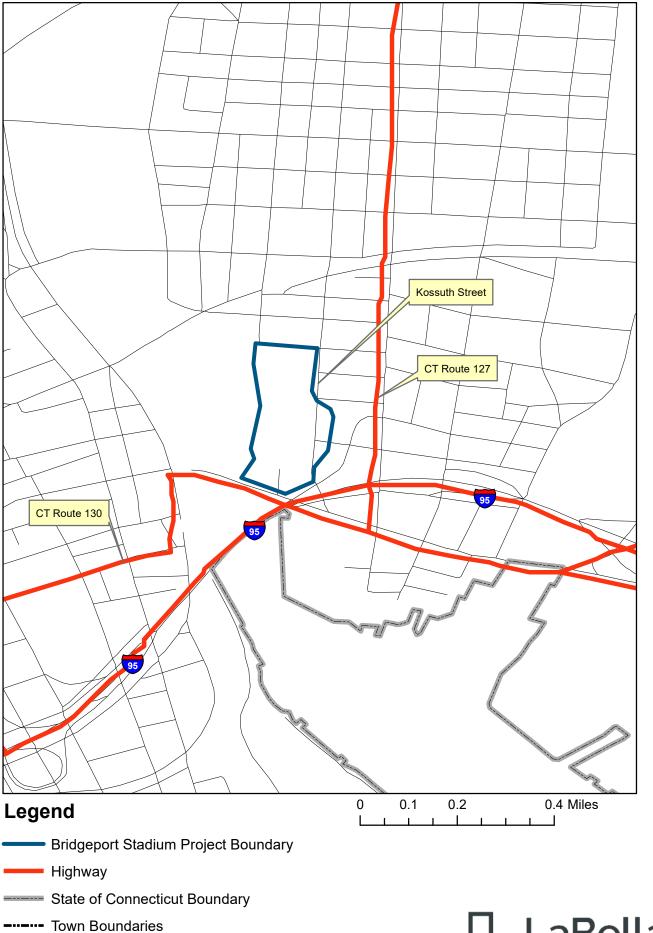
The project site is currently occupied by a dog track, associated buildings, and parking lot. The project intent is to redevelop the site to serve as a venue for professional sporting events. The project entails the construction of a modular soccer stadium and related improvements.

2.1.1 Location

The project site is located at 255 Kossuth St and 141 Stratford Ave in the City of Bridgeport in Fairfield county, CT. The project site is bordered by Pulaski St to the North, Kossuth St to the East, Stratford Ave to the South, and Pequonnock River to the West. Refer to Figure 2.1 for Site Location Map.



Site Location Map



Municipal Road

LaBella Powered by partnership

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2.1.2 Geologic Conditions

The site geologic conditions are summarized in a separate document titled "Geotechnical Subsurface Investigation and Engineering Report Bridgeport Stadium Bridgeport, Connecticut" prepared by LaBella Associates and dated June 17, 2024.

2.1.3 Environmental Resources

The site environmental resources are summarized in a separate document titled "Wetland and Watercourse Evaluation Report" prepared by BL Companies and dated September 29, 2023.

2.1.4 Environmental Justice

The project site is located in Environmental Justice Block Groups 2023: 090010740001.

2.1.5 Environmental Remediation

The site soil and groundwater are contaminated. The nature and extent of the contamination are currently under investigation. Appropriate remedial activities and controls will be implemented after a Phase III Environmental Site Assessment is performed and a Remedial Action Plan is prepared.

2.1.6 Floodplain Considerations

The site floodplain considerations are summarized in a separate document titled "Floodplain Assessment for Proposed Bridgeport Stadium" prepared by LaBella Associates and dated July 8, 2024.



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2.2 Ownership

The property is privately owned by Swanston Organization, LLC.

2.3 Existing Facilities and Present Condition

2.3.1 Water

Water is supplied to the site by the City of Bridgeport water system through an existing 16-inch diameter pipe. A fire flow test was performed on this water main by Aquarion Water Company on July 15, 2024 at 5:45pm, and the test results indicate that the available fire flow capacity is 7, 258 gpm @ 20 psi. The fire flow test report is included in Appendix A.

2.3.2 Wastewater

Wastewater generated on site is conveyed to the City of Bridgeport wastewater system through a connection to a 12-inch pipe.

2.3.3 Stormwater

Stormwater collected on site is conveyed to the Pequonnock River. There are three (3) existing outfalls. Some stormwater flow from the City of Bridgeport is routed through the onsite stormwater system to these outfalls.



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3. PROPOSED IMPROVEMENTS

3.1 Water and Sewer

The proposed modular stadium will be constructed to seat 7,500 people. The stadium will be designed to accommodate a future expansion that will increase the seating capacity of the stadium. At a later time, a new stadium with the capacity to seat 20,000 people may replace the expanded stadium. To ensure the water and sewer infrastructure serving the site are adequately sized, the seating capacity of the full buildout stadium will be used to estimate the demand.

| Table 3-1: Projected Water Demand at Buildout ⁽¹⁾ | | | | |
|---|--------|---------------|--|-----------------------------|
| Type of Use | Unit | Unit Quantity | Hydraulic Loading Rate ⁽²⁾ (gpd/unit) | Average Daily Flow (gpd) |
| Stadium | Seat | 20,000 | 3.5 | 70,000 |
| Employees ⁽³⁾ | Person | 1,000 | 7 | 7,000 |
| Concessions ⁽⁴⁾ | Meal | 20,000 | 5 | 100,000 |
| Average Daily Flow (gpd) | | | 177,000 | |
| Average Daily Flow (gpm) | | | 123 | |
| Max Day Peak Factor: 2 | | | | |
| Max Daily Flow (gpd) | | | 354,000 | |
| Max Daily Flow (gpm) | | | 246 | |
| Hourly Peak Factor: 4 | | | | |
| Peak Hourly Flow (gpd) | | | 708,000 | |
| Peak Hourly Flow (gpm) | | | 492 | |

- 1. Projected wastewater flows assume full buildout and maximum occupancy of facilities.
- 2. Hydraulic loading rates from table 4 of Connecticut Public Health Code On-Site Sewage Disposal Regulations and Technical Standards for Subsurface Sewage Disposal Systems unless otherwise noted below.
- 3. Assumed the hydraulic loading rate for a stadium employee is double that of a stadium guest, and assumed quantity of employees.
- 4. Assumed stadium concessions is equivalent to a Take-Out Food Service and the total number of meals served in the stadium is equal to the seating capacity of the stadium.



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Peak demand can also be estimated by assuming that all fixtures that consume water in the facility are in use simultaneously.

| | Table 3-2: Projected Peak Water Demand ⁽¹⁾ | | | | | | |
|-----------------------|--|---------------------------------|---------------------------------------|-----------|---------------------------------------|--|--|
| Type of Use | Unit | Unit Quantity ⁽²⁾ | Fixture Consumption ⁽³⁾ | | Hydraulic Loading Rate (gpm) | Peak Instantaneous Flow (gpm) | |
| Sink | Each | 354 | 0.5 | gpm | 0.5 | 177 | |
| Toilet ⁽⁴⁾ | Each | 355 | 1.6 | gal/flush | 1.6 | 568 | |
| Urinal ⁽⁴⁾ | Each | 83 | 1.0 | gal/flush | 1.0 | 83 | |
| Shower | Each | 40 | 2.5 | gpm | 2.5 | 100 | |
| Kitchen Sink | Each | 20 | 2.5 | gpm | 2.5 | 50 | |
| | | | | | Total | 976 | |

- 1. The projected flow is for the current buildout (7,500 seat stadium) because floor plans are not available at this time for the full buildout (20,000 seat stadium).
- 2. Unit quantities are estimated based on counts of the fixtures shown on the first floor plan, except it was assumed each concession stand has one kitchen sink and the kitchen on the first floor was assumed to have 4 kitchen sinks. Assumed the 2nd and 3rd floor of the stadium would have the same fixture counts as the 1st floor, except the West side of the 2nd floor and 3rd floor were assumed to be the same as the East side of the 1st floor.
- 3. Fixture consumption assumed to be compliant with Connecticut regulations establishing minimum efficiency standards for plumbing fixtures and other water-saving devices (Section 21a-86a).
- 4. Assumed toilets and urinals are flushed once per minute.

Based on the peak flows estimated in Table 3-1 and Table 3-2 in comparison to the estimated flow available in the existing water main per fire flow testing (Appendix A), the existing 16-inch water main has adequate capacity to meet the peak demand of the facility while providing fire suppression flow.

Site wastewater will be conveyed into the City of Bridgeport wastewater system. The connection between the two systems will be examined further to ensure that the existing pipes receiving the wastewater discharge from the site have adequate capacity to convey the peak flows from the site.



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3.2 Stormwater

The project is anticipated to disturb 14 acres of soil by a conservative estimate. This exceeds more than 5 acre of disturbance; therefore, a Stormwater Pollution Control Plan will be prepared for this project in accordance with CTDEEP requirements.

The soil and groundwater on site are contaminated; therefore, stormwater collected from redeveloped areas of the site will not be discharged on site through infiltration.

The stormwater runoff from the existing parking lots is collected by catch basins in the pavement and conveyed off site.

The proposed parking lots will be paved with permeable pavement to improve stormwater quality. The permeable pavement subbase will be equipped with underdrains placed over an impermeable liner to prevent infiltration and collect the stormwater so it can be conveyed off site.

Stormwater runoff from the remaining redeveloped areas of the site (stadium roof, sidewalks, etc, ...) will also be collected and discharged off site. The design intent is to minimize the amount of impervious area and treat as much collected stormwater runoff as practicable from the redeveloped area with tree filters to improve the quality of that stormwater runoff before it is discharged off site.

3.3 Engineer's Opinion of Probable Construction Cost

An Opinion of Probable Construction Cost will be prepared.

3.4 Project Schedule

A Project Schedule will be prepared.

3.5 Next Steps

A list of approvals that are required for construction will be prepared.



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Appendix A: Fire Flow Test Results



Aquarion Water Company Fire Flow Test

Test Location: BRIDGEPORT, CT

Test Date: 07/15/2024 Test Time: 05:45 PM

Flow Hydrant: 1633 Location: Kossuth St @ Nichols St

Flow Hydrant Parameters:

16" Main Size:

Pipe/Nozzle Diameter: 4.0 Diffuser inches

Pito Pressure: 40 psi PSI Before: 94 psi

Residual Hydrant: 1649 Location: Howe St @ Kossuth St

Residual Hydrant Parameters:

PSI Before: 94 psi Residual During Flow: 82 psi PSI After: 94 psi 12 psi PSI Drop:

Test Results:

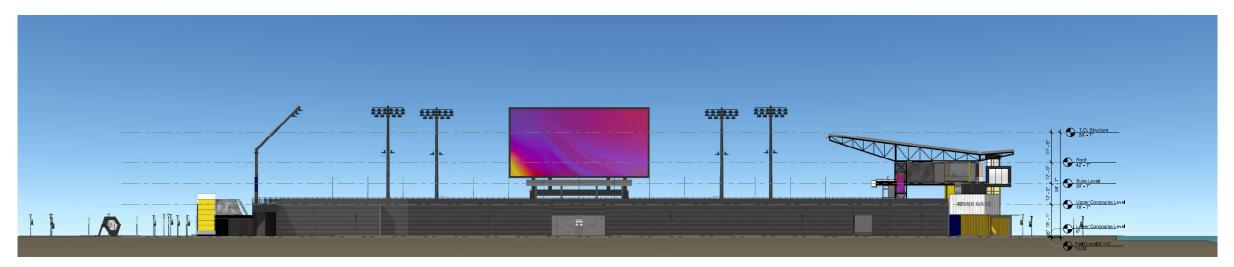
GPM Available: 2,720 GPM @20 psi: 7,258

Test Performed By: JP&WILLB

NOTE: Static Pressure readings are actual, and test results are not corrected for elevation differential.

Test Method: Calibrated Orifice

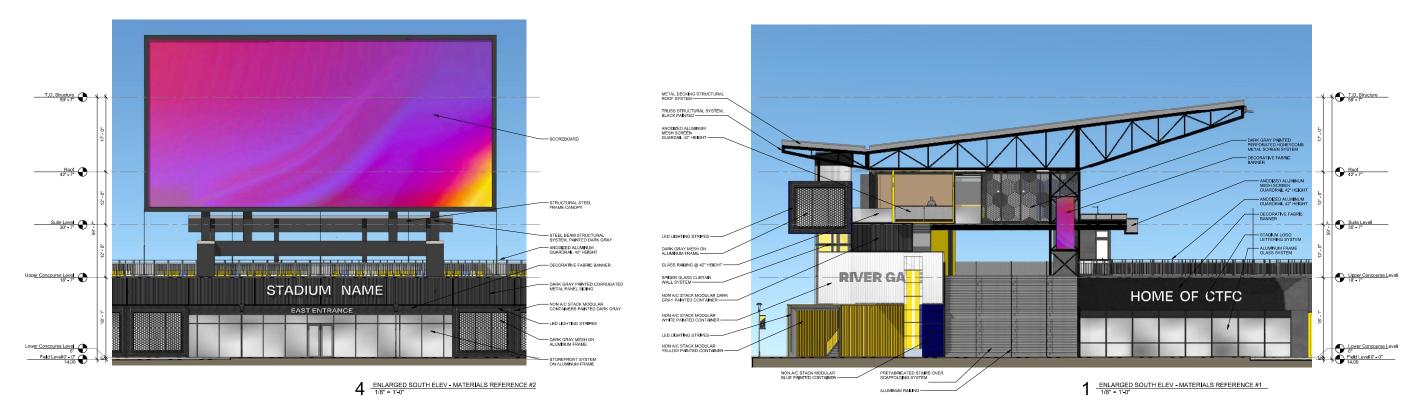
Disclaimer: This data represents system conditions on the date and time that the test was performed. System conditions may vary significantly throughout the year. The design of new water service installations and the identification and gathering of all necessary data is the sole responsibility of the Developer or his representative. In all instances, the water service designer should apply engineering judgment to ensure proper design. Aquarion Water Company does not guarantee the accuracy of this data.

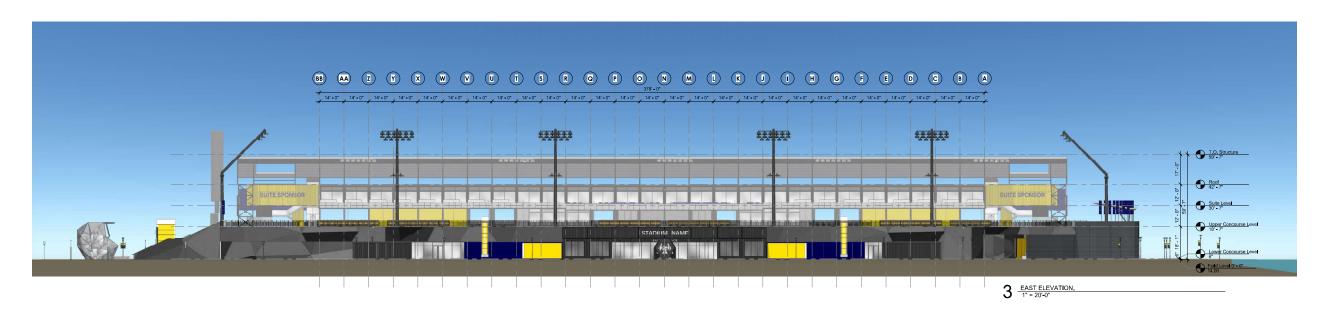


3 NORTH ELEVATION.
1" = 20'-0"



2 SOUTH ELEVATION.
1" = 20'-0"









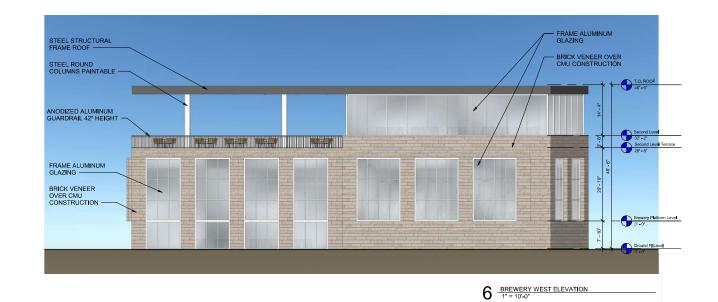


2 Technical Review - West - East Interior Elevation
1" = 20'-0"

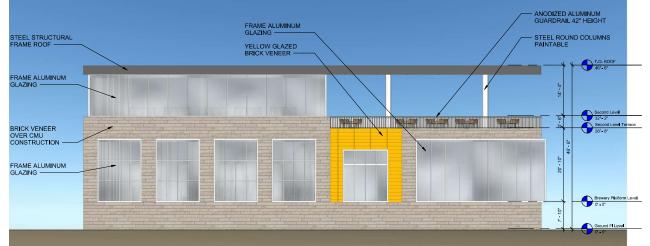




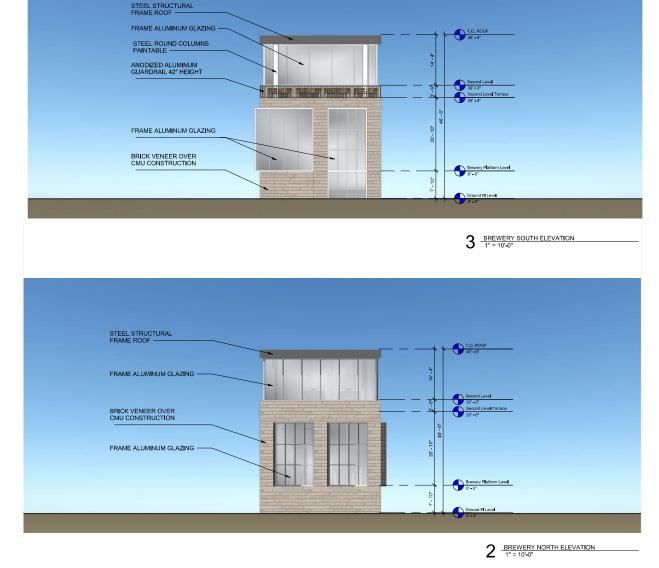
Bridgeport, Connecticut.

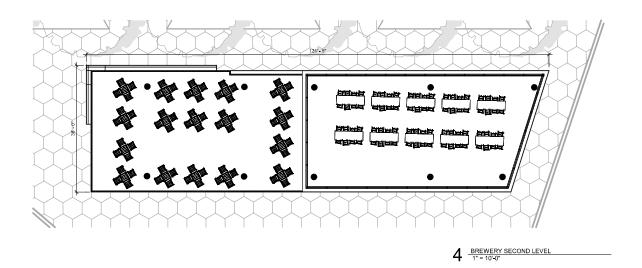


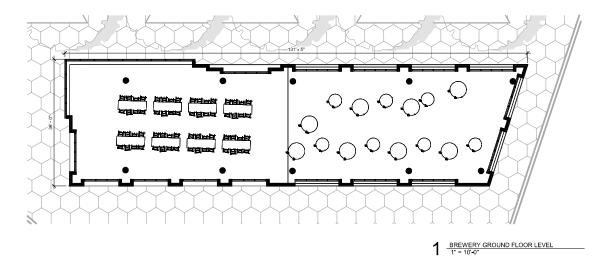
— ANODIZED ALUMINUT GUARDRAIL 42" HEIG



5 BREWERY EAST ELEVATION
1" = 10'-0"







07/19/24

BREWERY ELEVATIONS

Technical Review Package A09





AERIAL SOUTHEAST PERSPECTIVE - NIGHT NTS



4 WEST PERSPECTIVE - NIGHT NTS



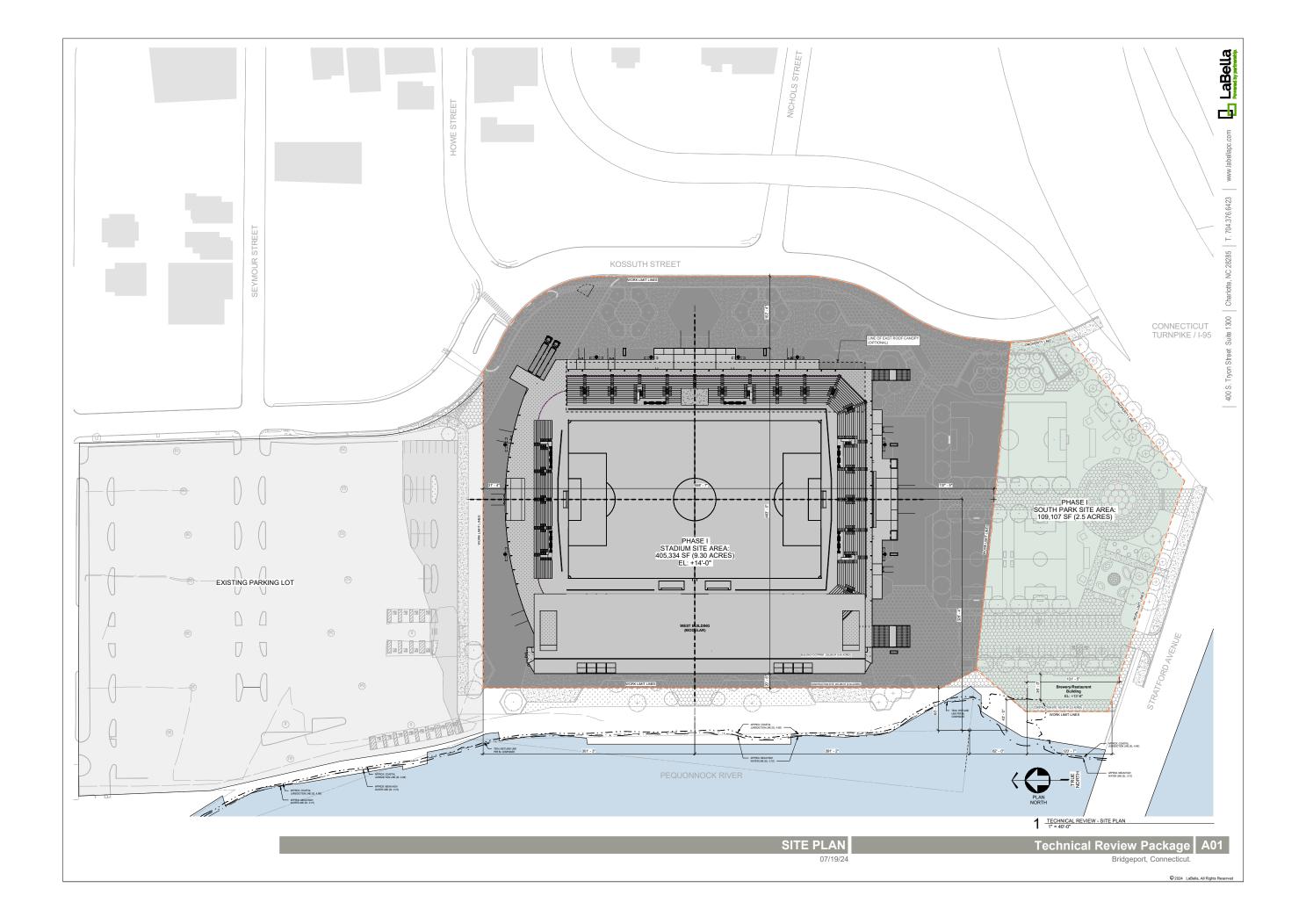
3 AERIAL NORTHWEST PESPECTIVE - NIGHT NTS

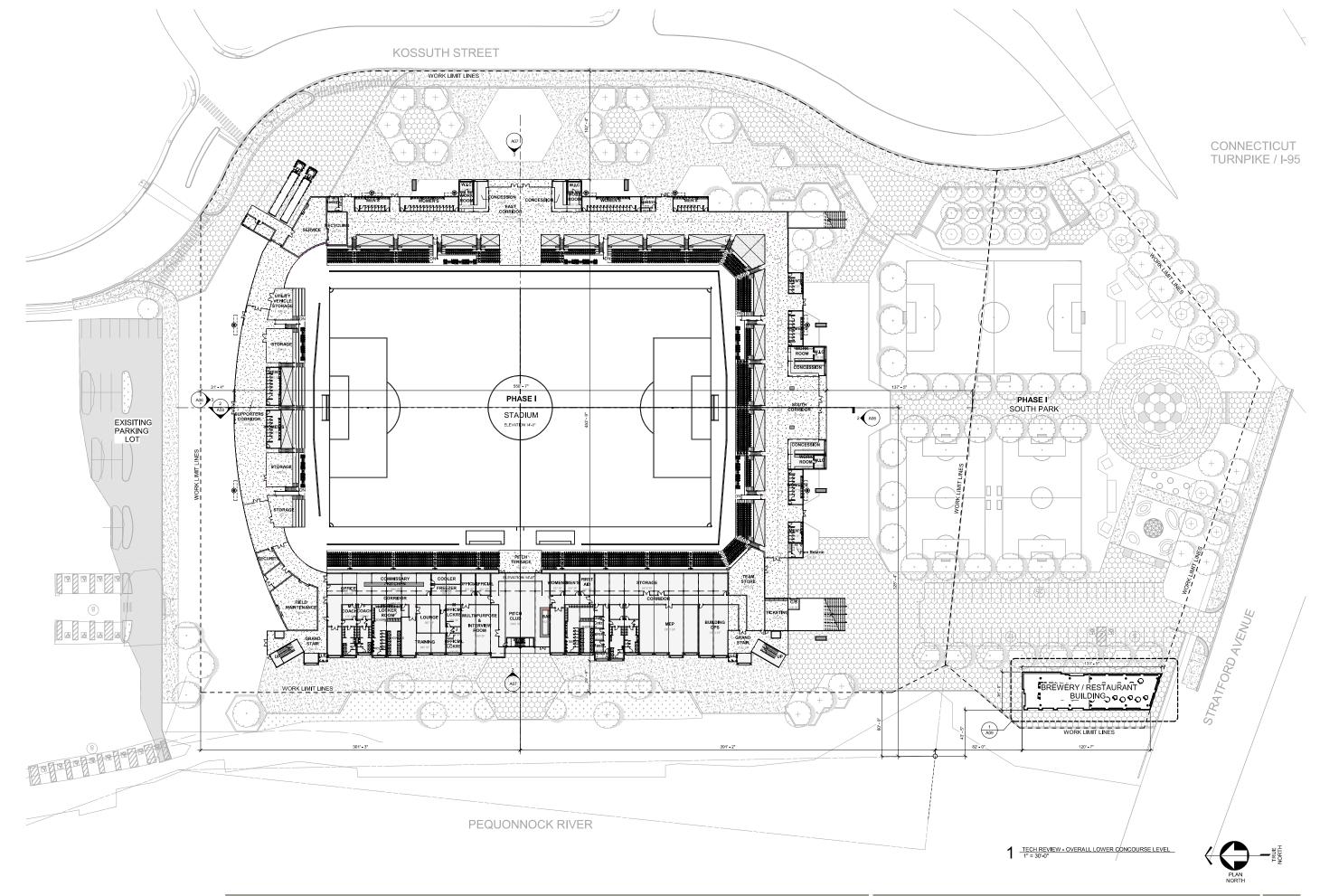


SOUTHWEST PERSPECTIVE CLOSE UP NTS



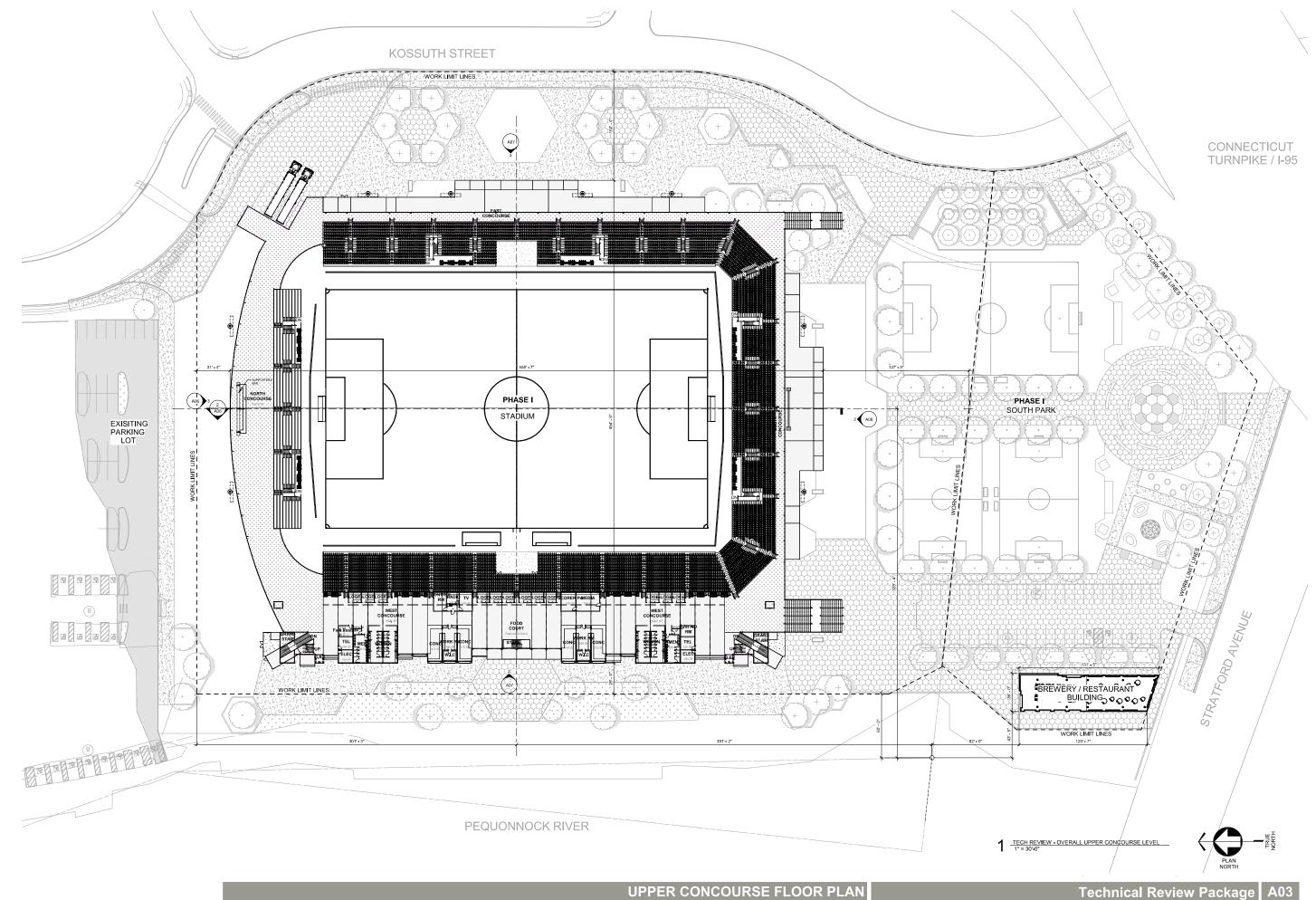
BRIDGEPORT CT - UNITED STADIUM - TECHNICAL REVIEW PACKAGE





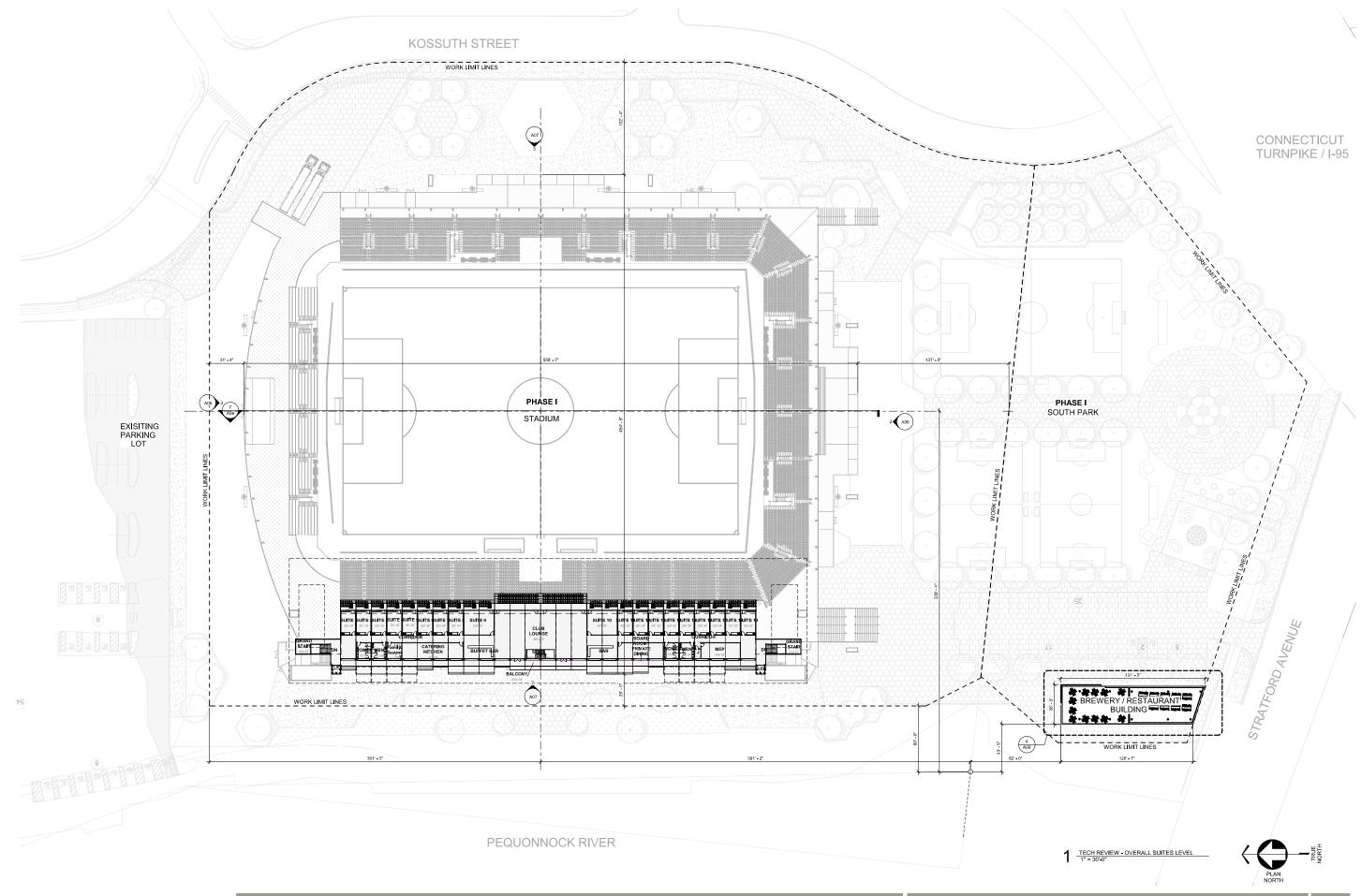
LOWER CONCOURSE FLOOR PLAN

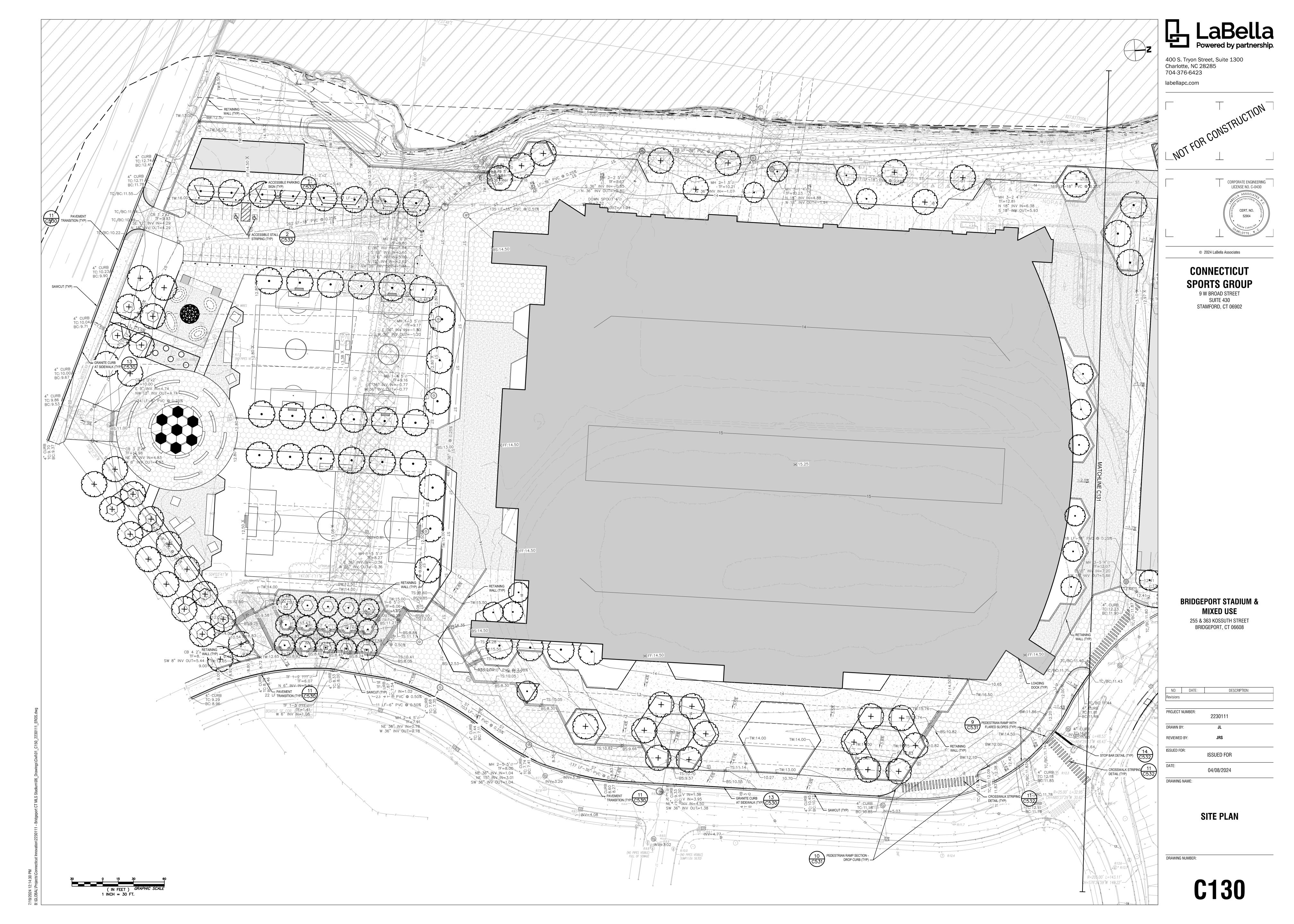
Technical Review Package | A02



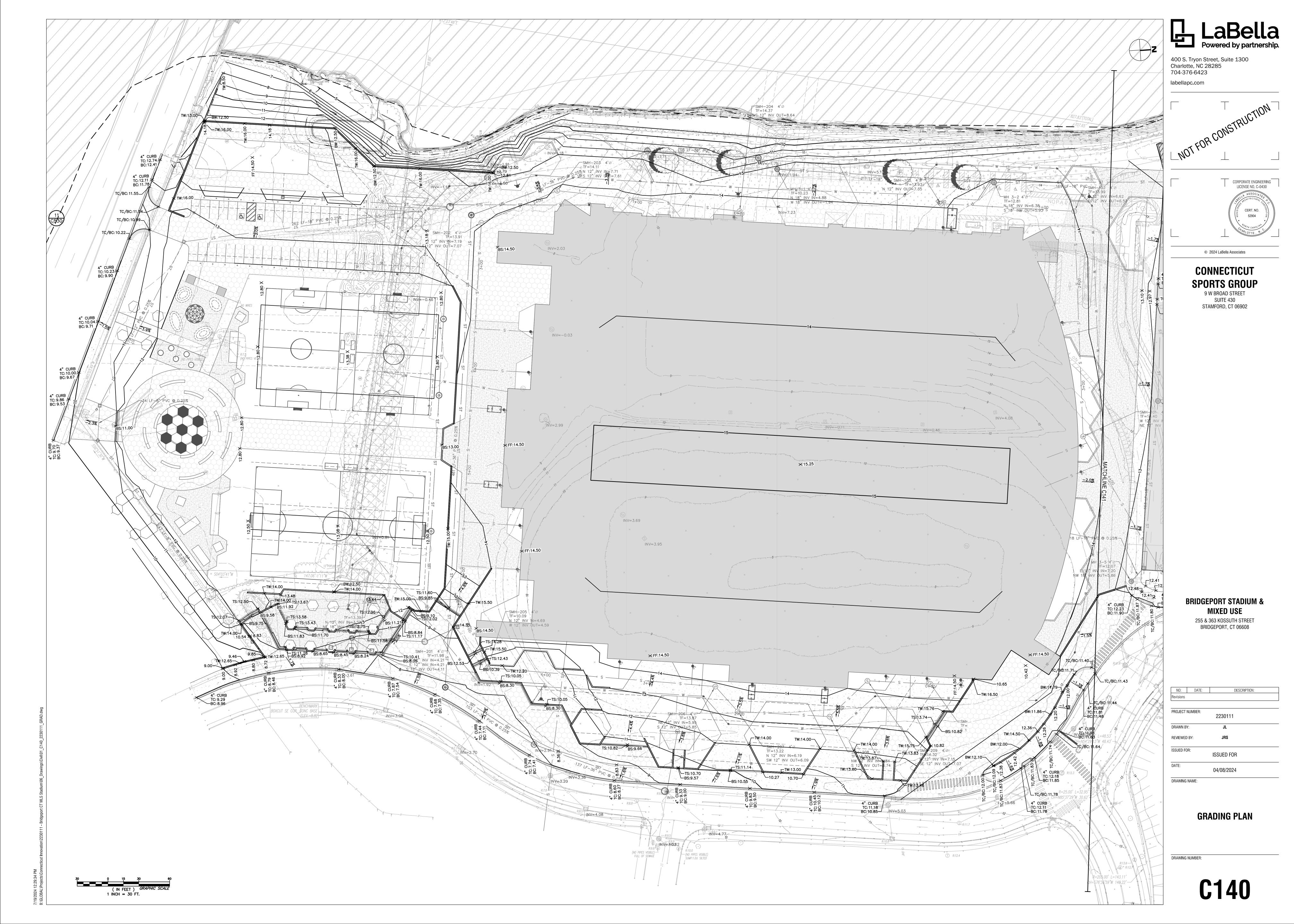
Bridgeport, Connecticut.



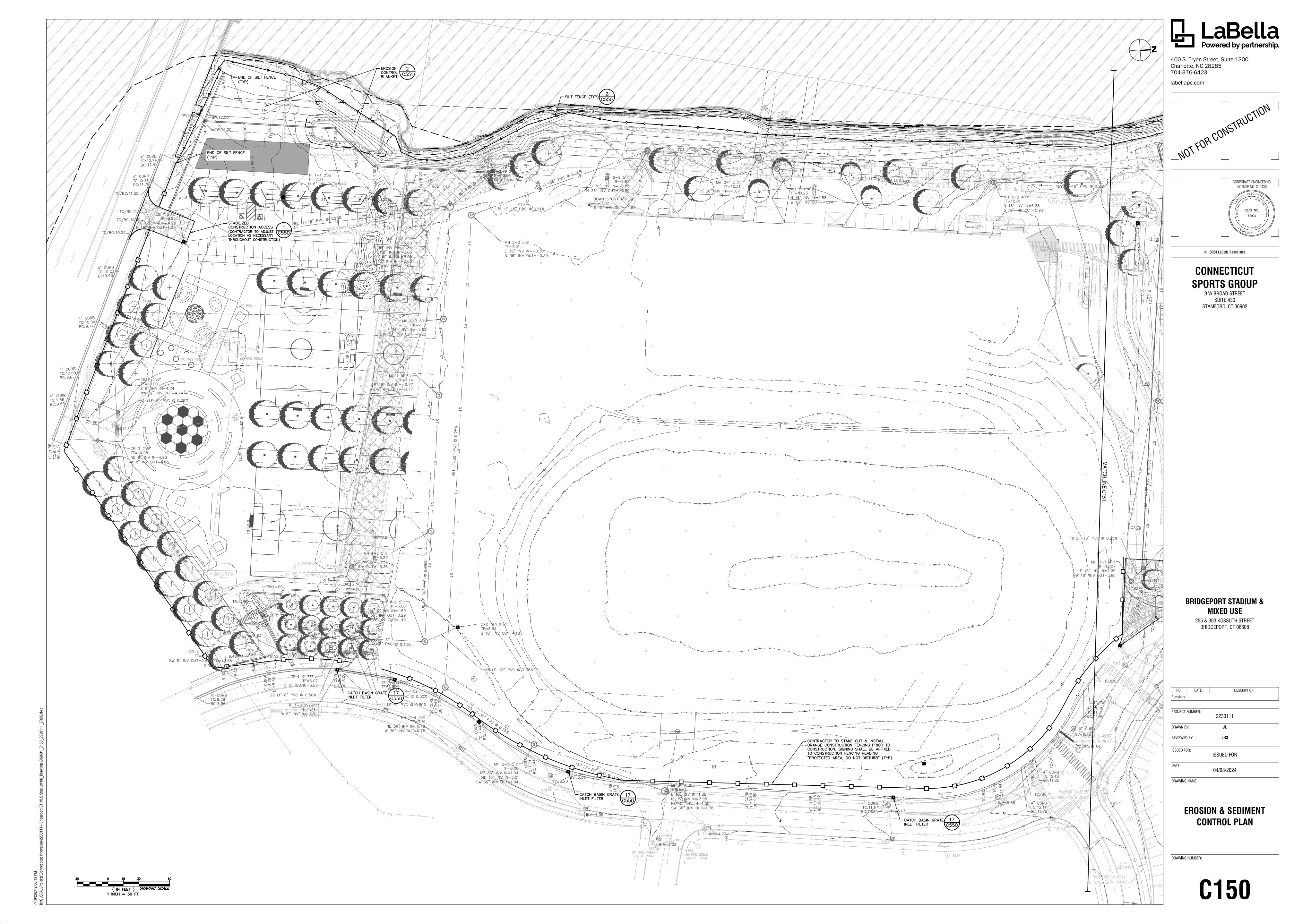


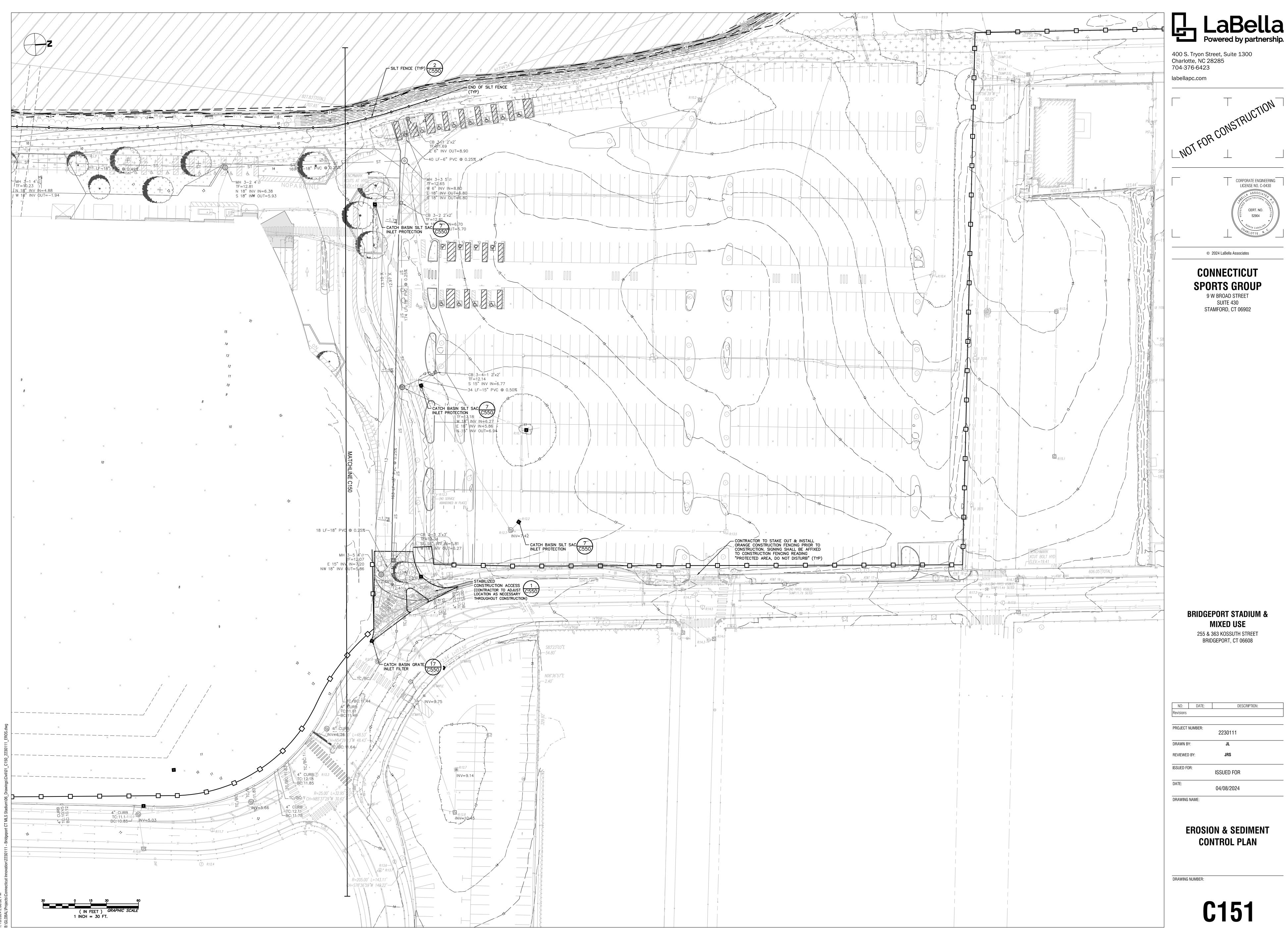


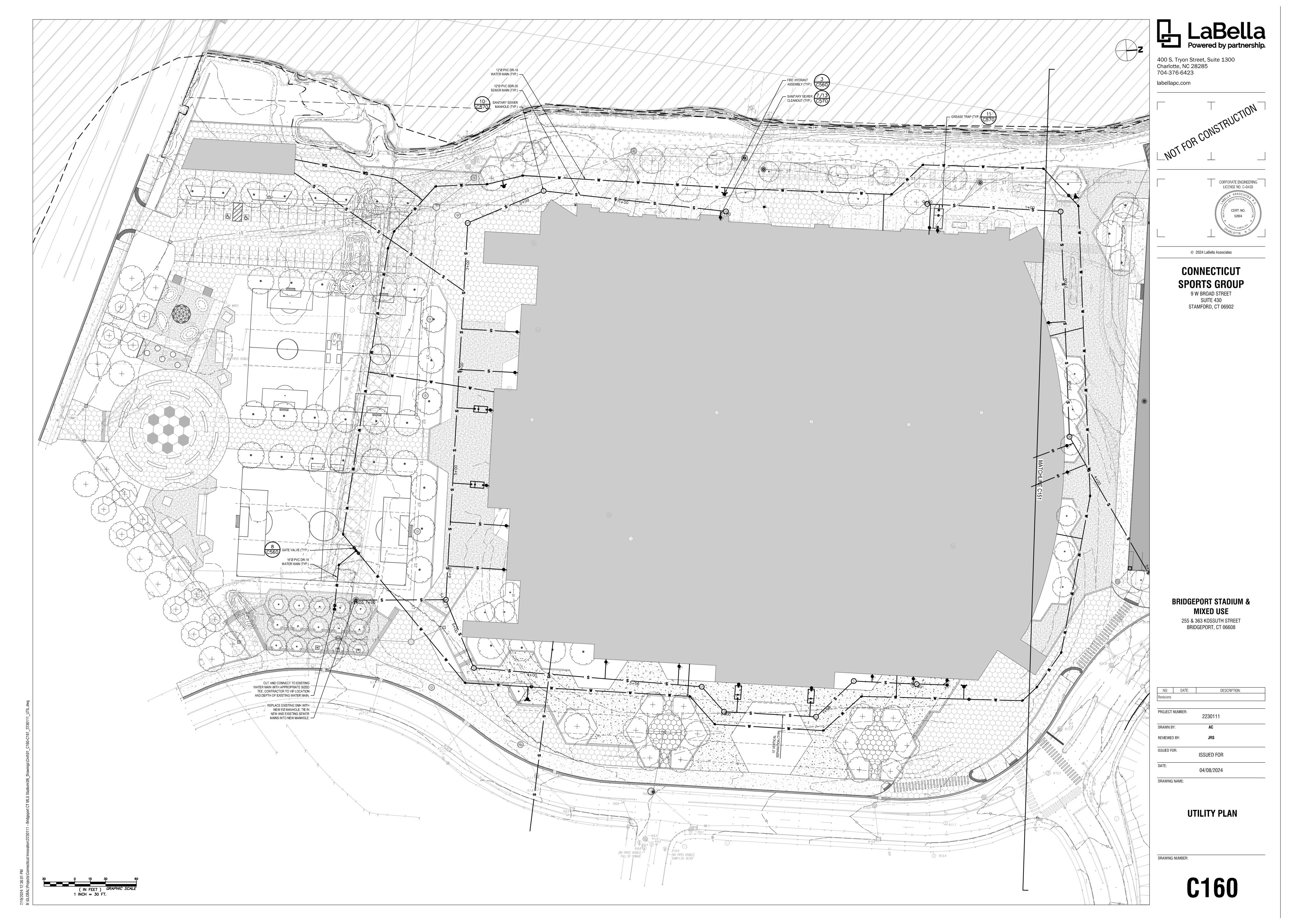


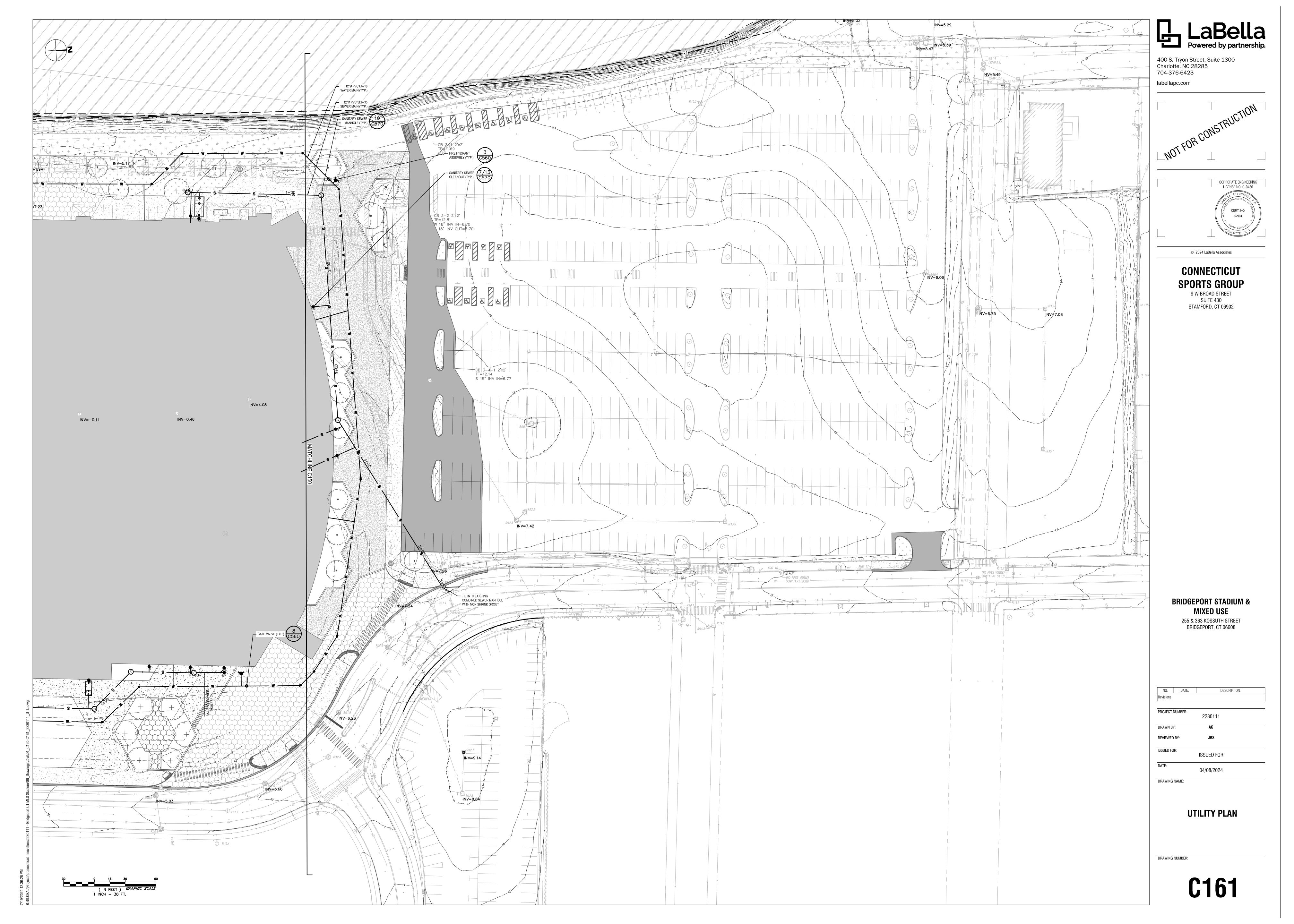


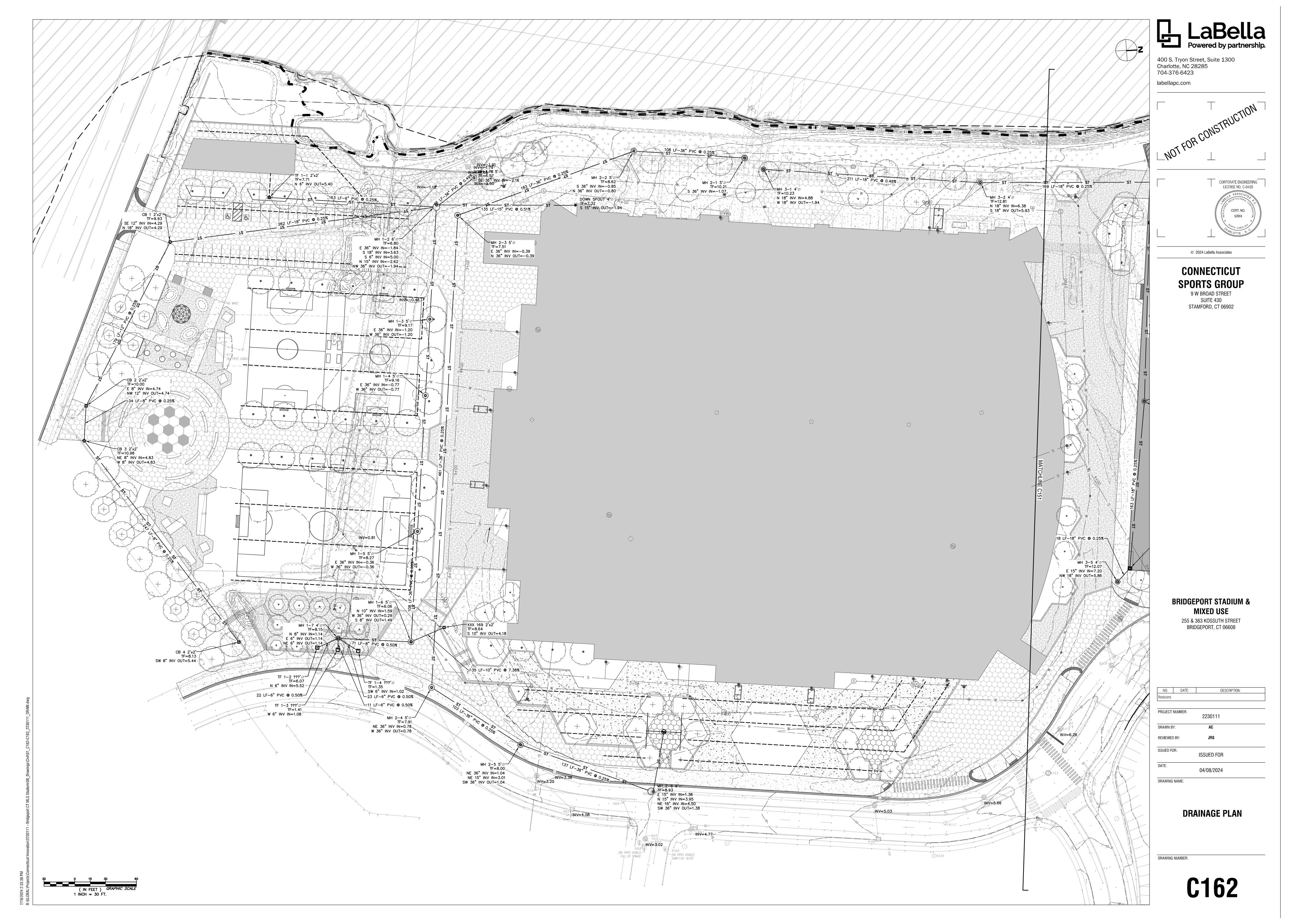


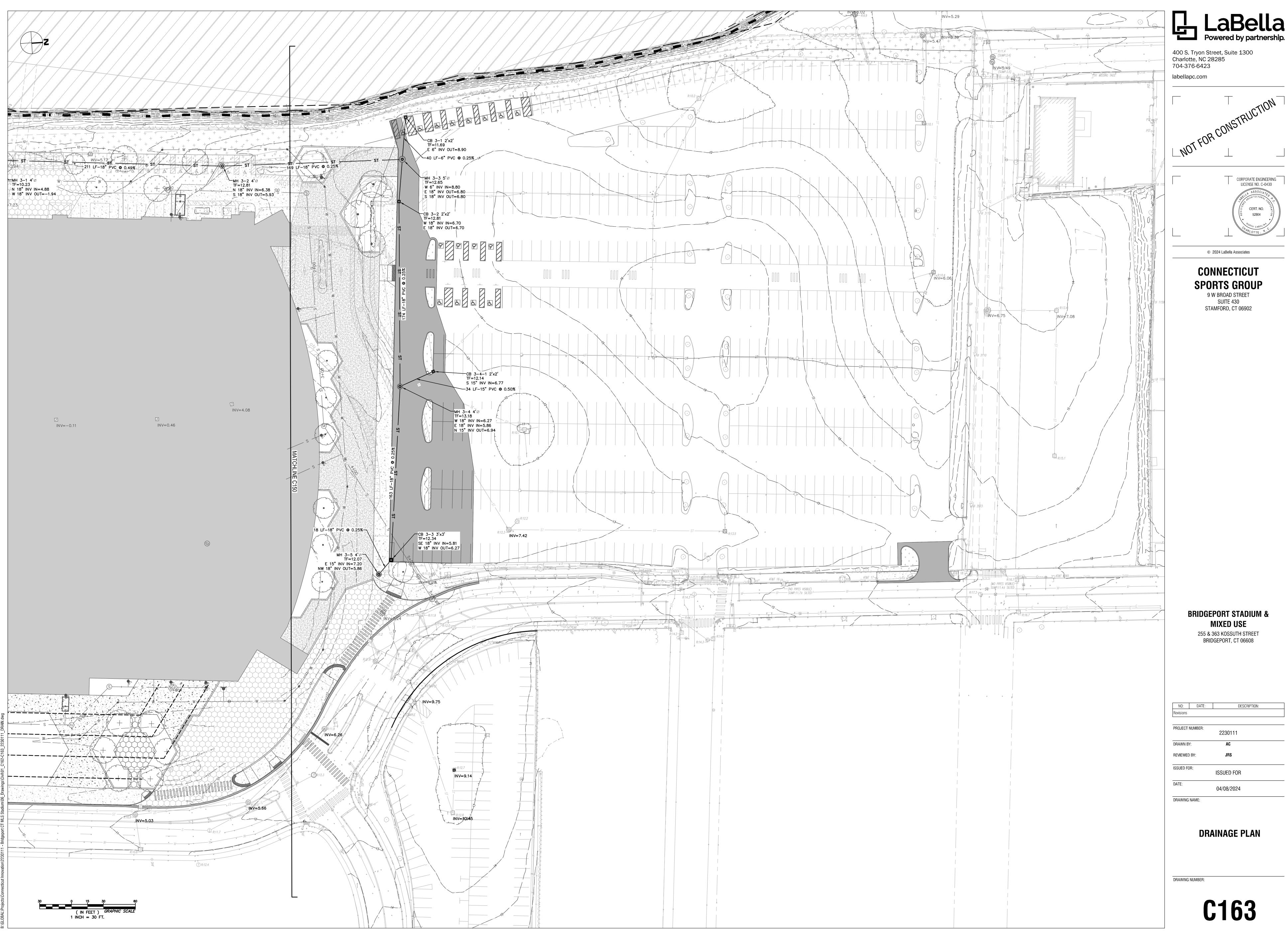




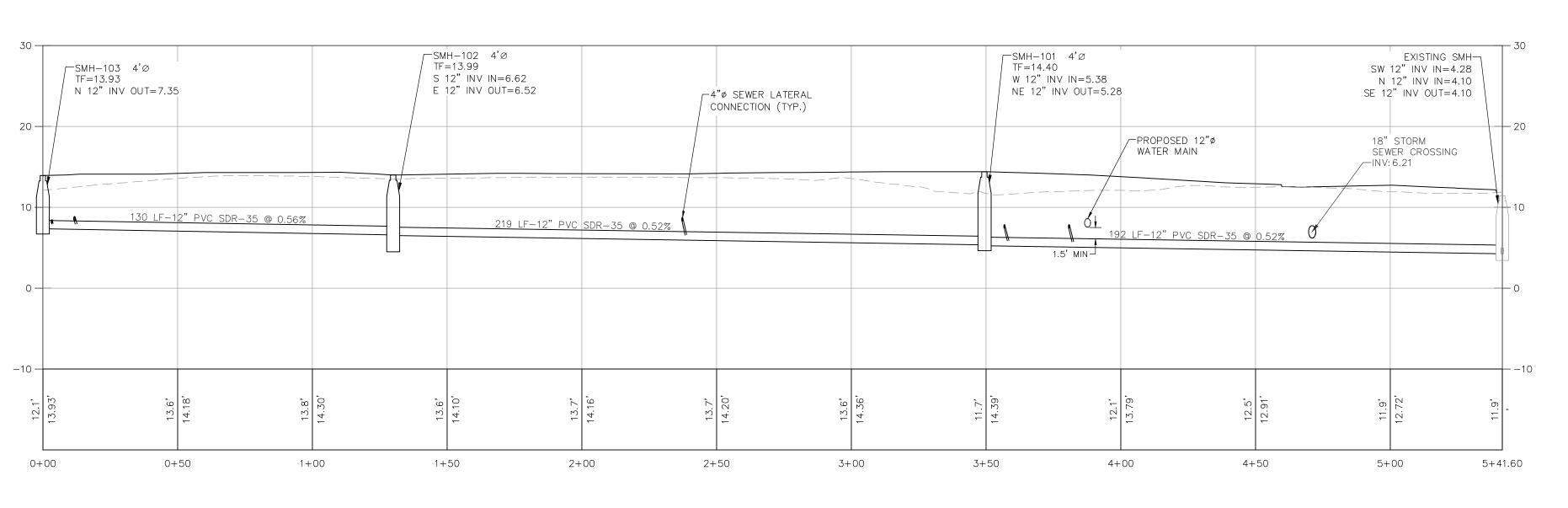












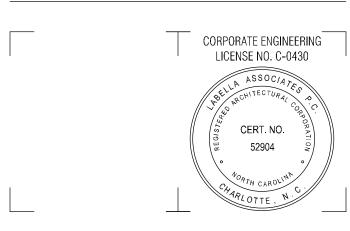
2 SANITARY SEWER PROFILE STA: 0+00 TO 5+41.60

H-SCALE: 1" = 30'
V-SCALE: 1" = 10'



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9 W BROAD STREET SUITE 430 STAMFORD, CT 06902

BRIDGEPORT STADIUM &
MIXED USE

255 & 363 KOSSUTH STREET
BRIDGEPORT, CT 06608

NO: DATE: DESCRIPTION:
Revisions

PROJECT NUMBER:
2230111

DRAWN BY:
AC
REVIEWED BY:
JRS
ISSUED FOR:
ISSUED FOR

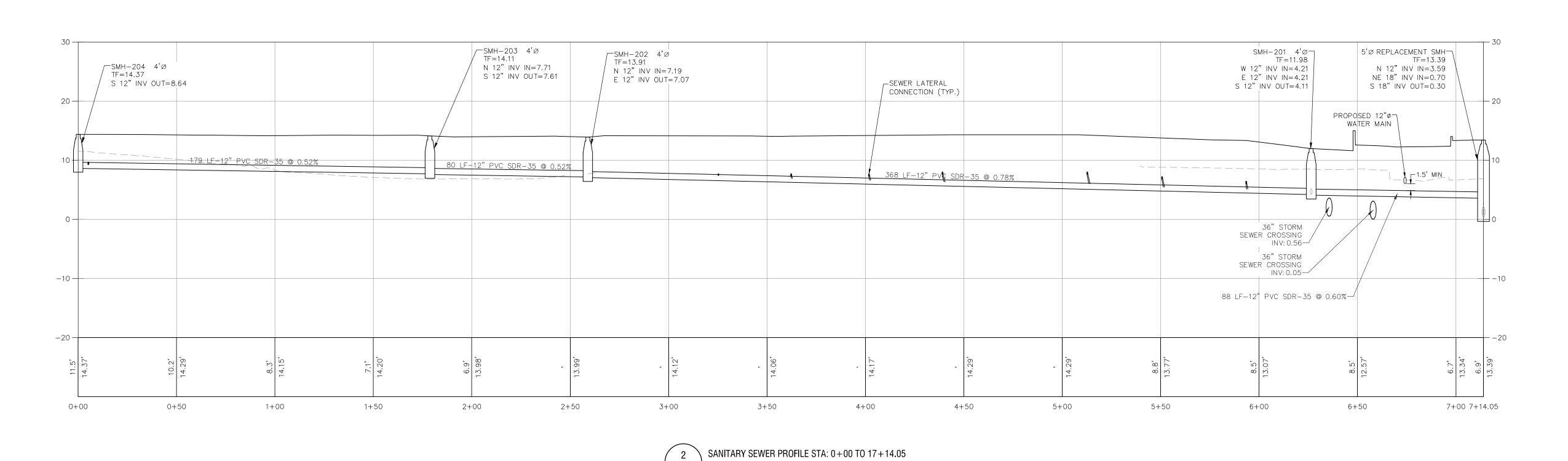
DATE:
04/08/2024

DRAWING NAME:

SANITARY SEWER PLAN & PROFILE NORTH SIDE STA 0+00 TO 5+41.60

DRAWING NUMBER:



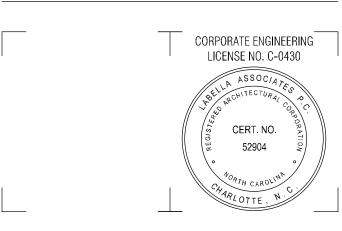


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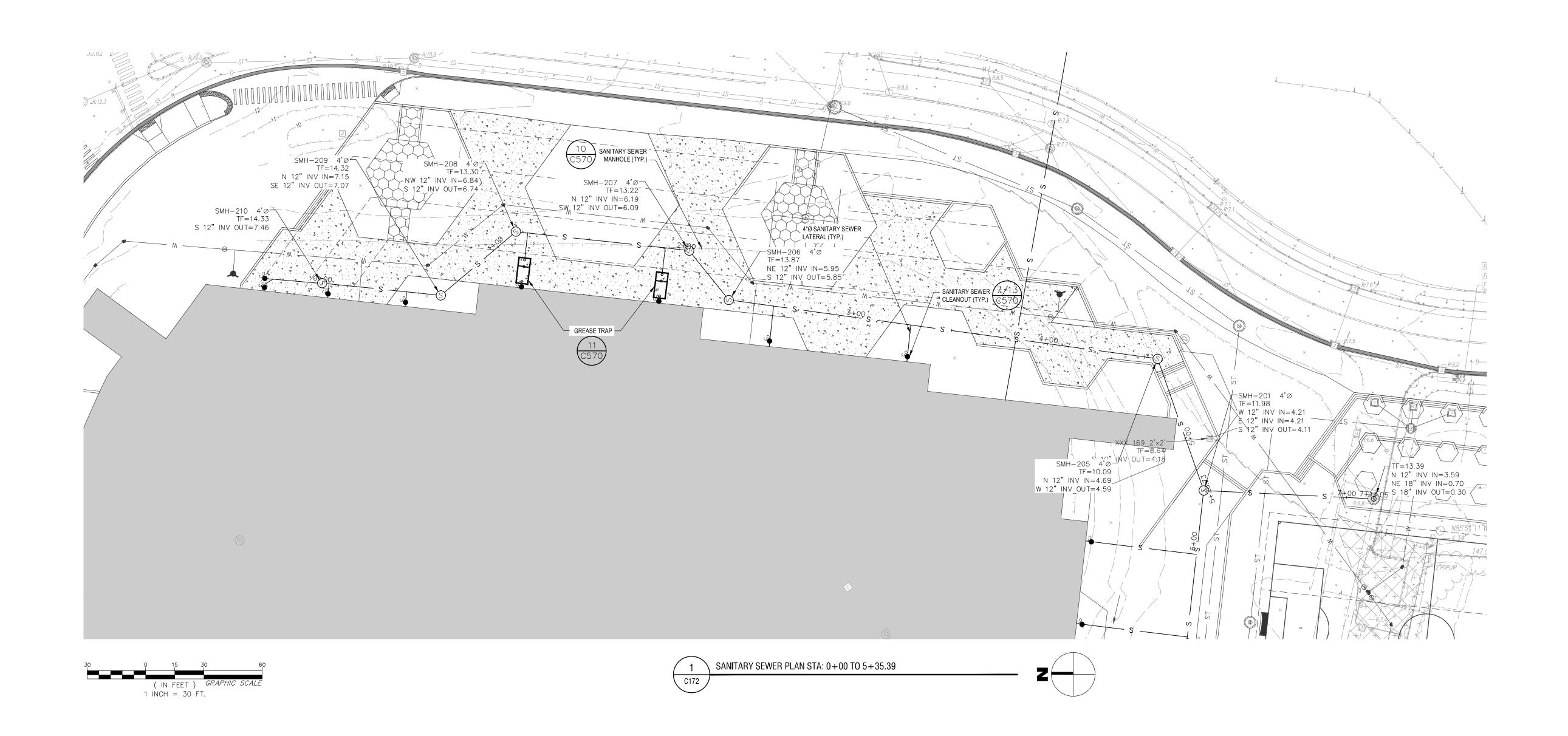
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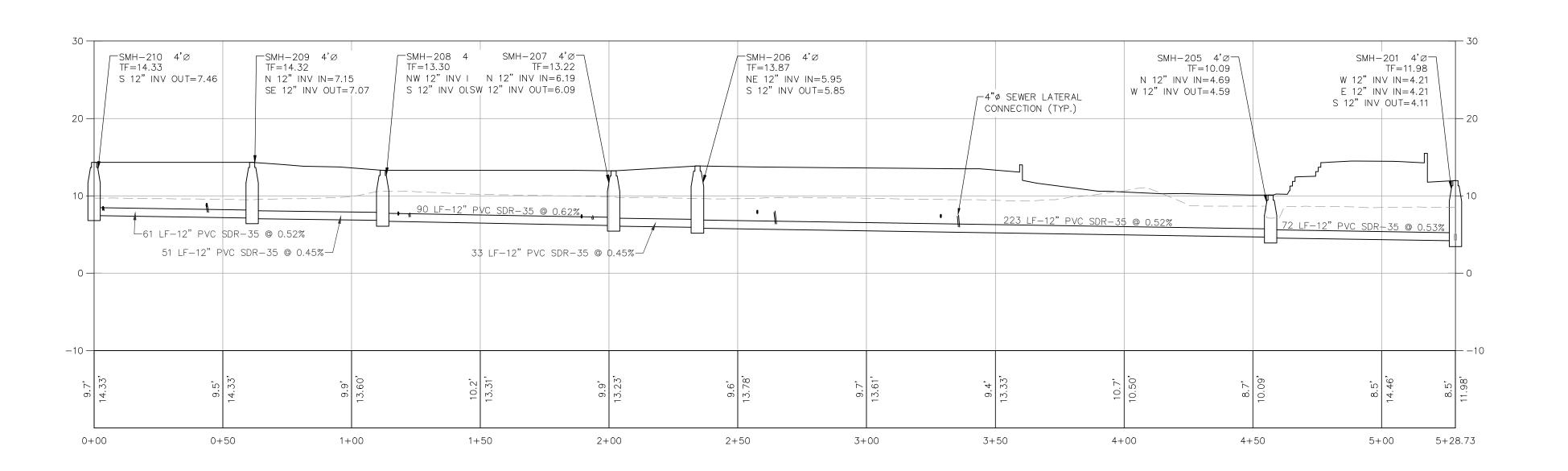
04/08/2024

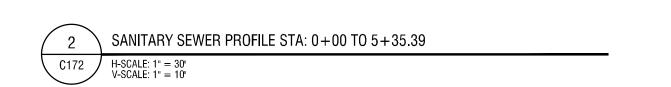
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DRAWING NUMBER:

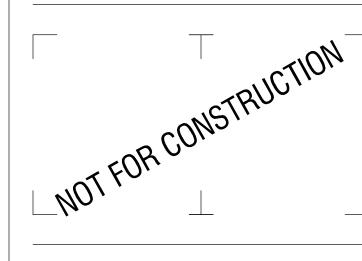


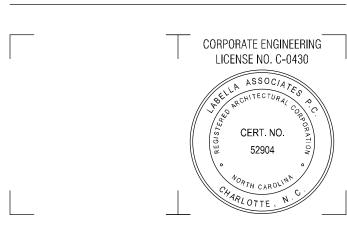






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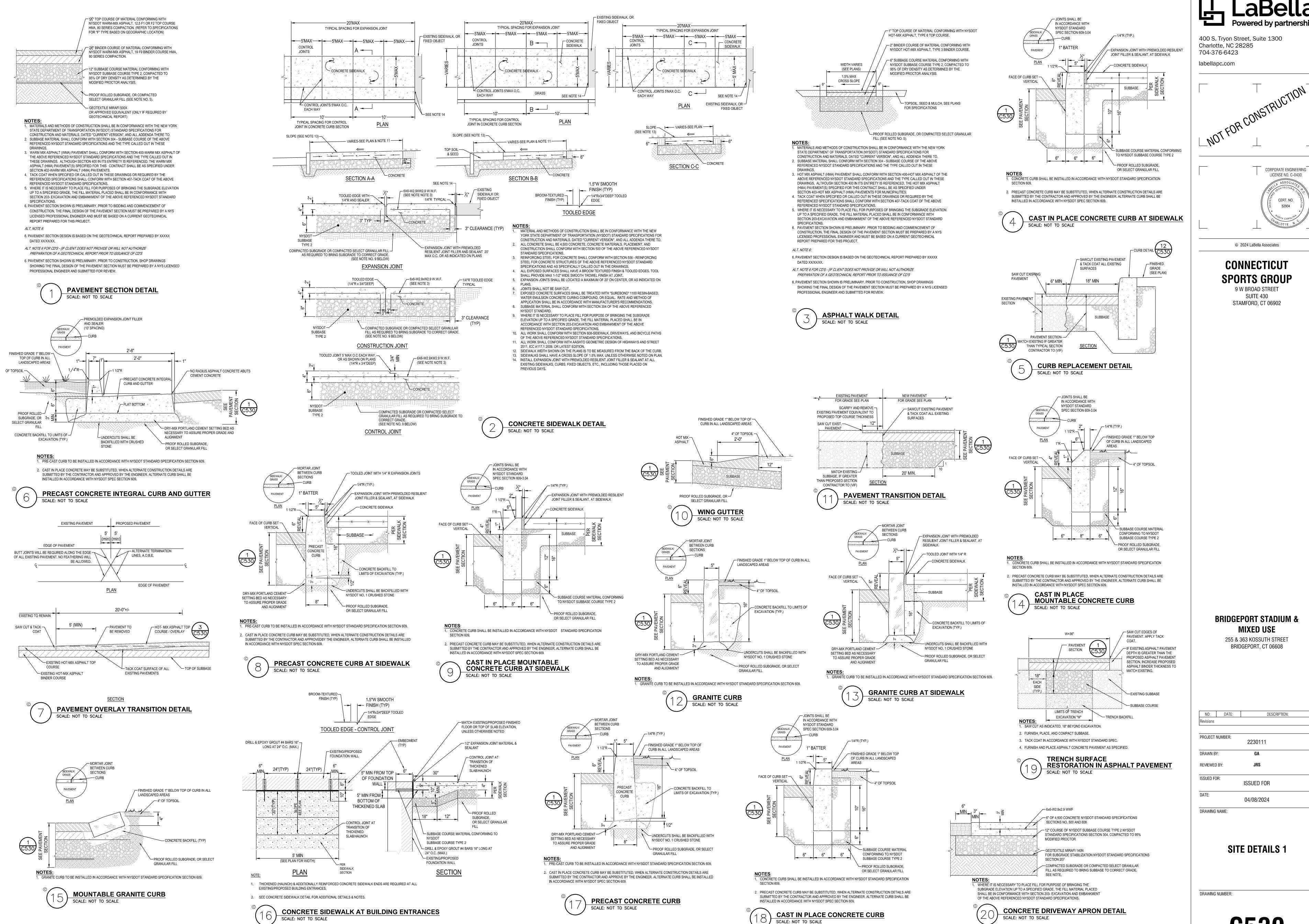
BRIDGEPORT STADIUM &
MIXED USE

255 & 363 KOSSUTH STREET
BRIDGEPORT, CT 06608

| N0: | DATE: | DESCRIPTION: |
|------------|--------|--------------|
| Revisions | | |
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| PROJECT N | UMBER: | 2230111 |
| DRAWN BY | : | |
| REVIEWED | BY: | AC |
| | | JRS |
| ISSUED FOI | ₹: | ISSUED FOR |
| DATE: | | 04/08/2024 |

SANITARY SEWER PLAN & PROFILE EAST SIDE STA 0+00 TO 5+35.39

DRAWING NUMBER:



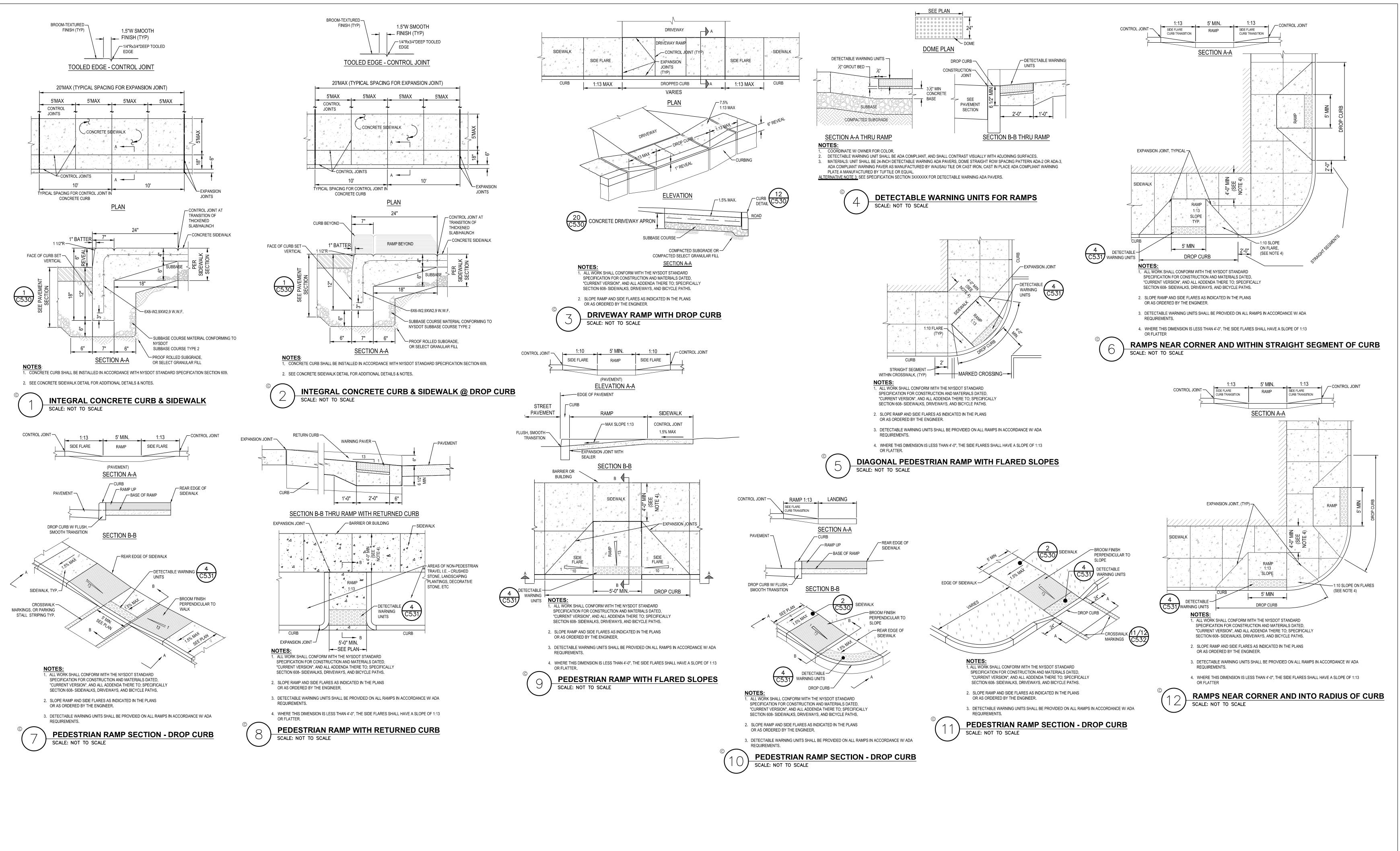
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04/08/2024



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ASSOCIATES

CERT. NO.

PARTH CAROLINA

CHARLOTTE. N. C.

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255 & 363 KOSSUTH STREET
BRIDGEPORT, CT 06608

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Revisions

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2230111

DRAWN BY: GA

REVIEWED BY: JRS

ISSUED FOR:

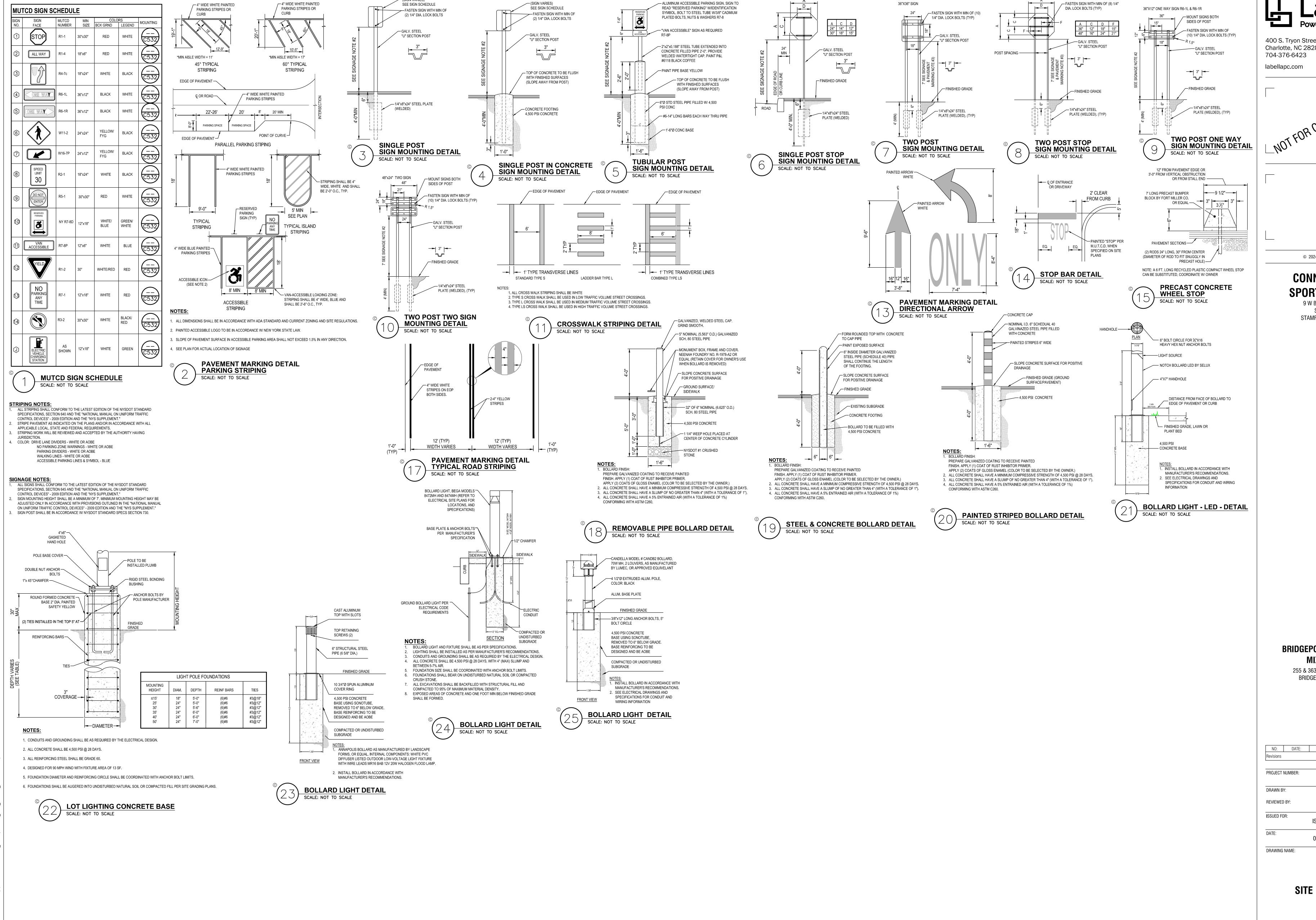
DATE:

04/08/2024

DRAWING NAME:

SITE DETAILS 2

DRAWING NUMBER:



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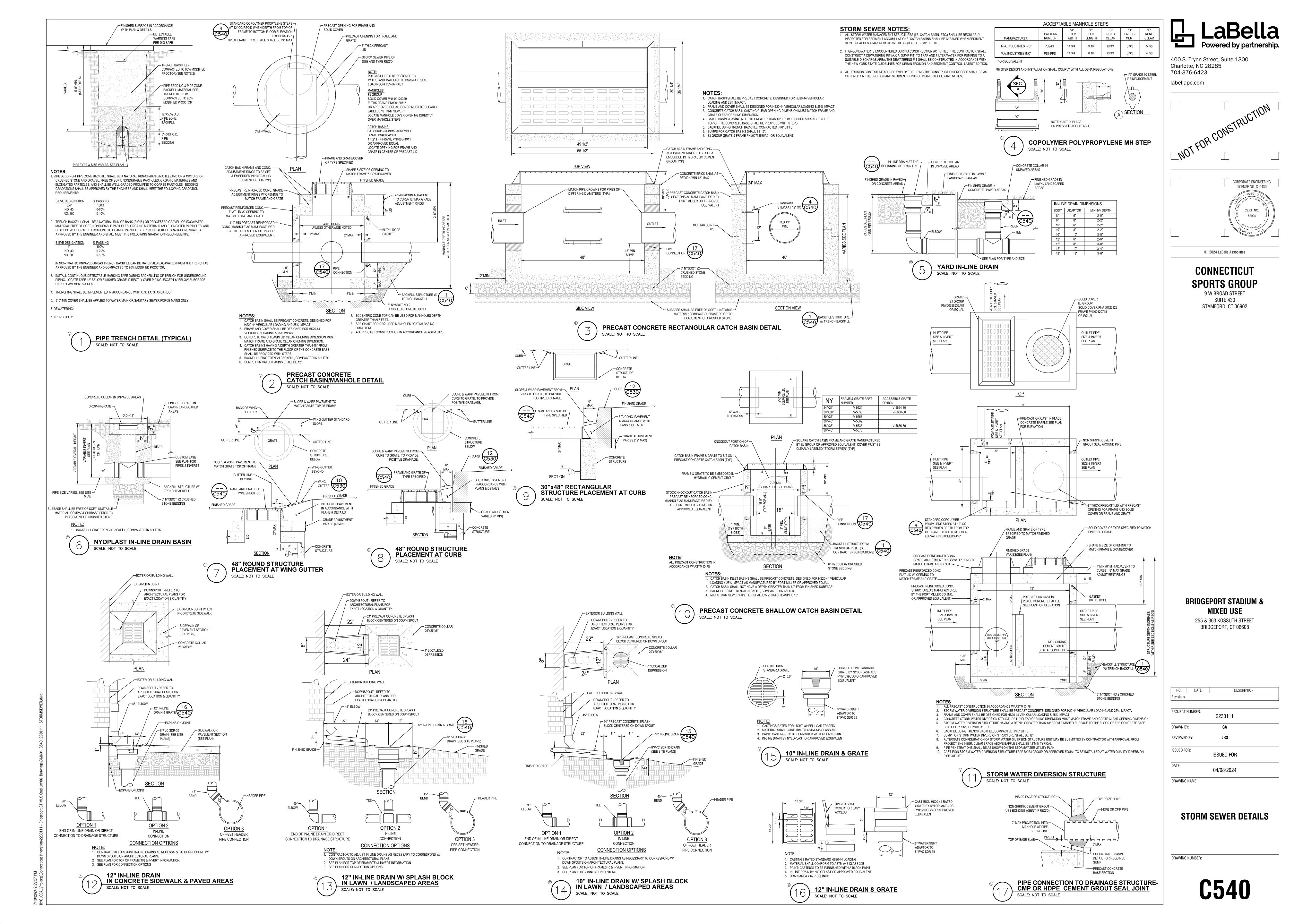
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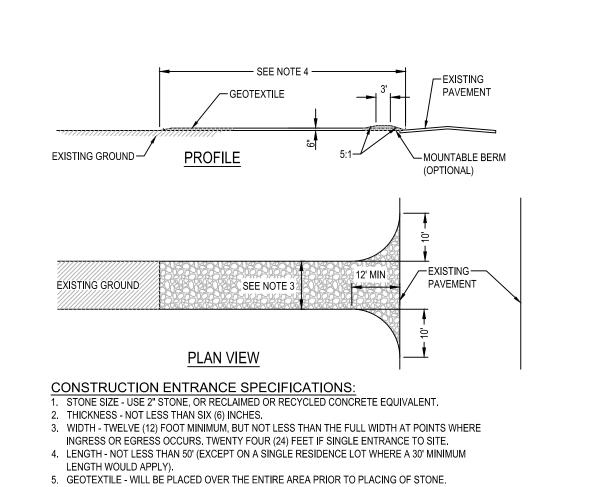
52904

BRIDGEPORT STADIUM & MIXED USE 255 & 363 KOSSUTH STREET BRIDGEPORT, CT 06608

DESCRIPTION: 2230111 **ISSUED FOR**

SITE DETAILS 3



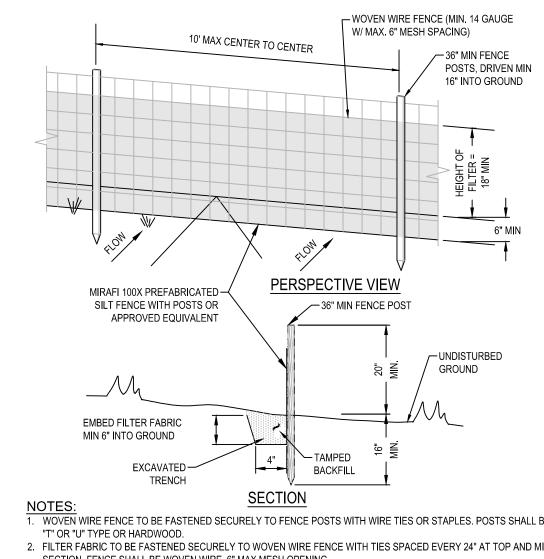


6. SURFACE WATER - ALL SURFACE WATER FLOWING OR DIVERTED TOWARD CONSTRUCTION ENTRANCES SHALL BE PIPED ACROSS THE ENTRANCE. IF PIPING IS IMPRACTICAL, A MOUNTABLE BERM WITH 5:1 SLOPES WILL BE PERMITTED. 7. MAINTENANCE - THE ENTRANCE SHALL BE MAINTAINED IN A CONDITION WHICH WILL PREVENT TRACKING OR FLOWING OF SEDIMENT ONTO PUBLIC RIGHTS-OF-WAY. THIS MAY REQUIRE PERIODIC TOP DRESSING WITH ADDITIONAL STONE AS CONDITIONS DEMAND AND REPAIR AND/OR CLEANOUT OF ANY MEASURES USED TO TRAP SEDIMENT. ALL SEDIMENT SPILLED, DROPPED, WASHED OR TRACKED ONTO PUBLIC RIGHTS-OF-WAY MUST BE REMOVED IMMEDIATELY. 8. WASHING - WHEELS SHALL BE CLEANED TO REMOVE SEDIMENT PRIOR TO ENTRANCE ONTO PUBLIC RIGHTS-OF-WAY. WHEN WASHING IS REQUIRED, IT SHALL BE DONE ON AN AREA

STABILIZED WITH STONE AND WHICH DRAINS INTO AN APPROVED SEDIMENT TRAPPING DEVICE.

9. PERIODIC INSPECTION AND NEEDED MAINTENANCE SHALL BE PROVIDED AFTER EACH RAIN.

CONSTRUCTION ACCESS DETAIL SCALE: NOT TO SCALE



NOTES:

1. WOVEN WIRE FENCE TO BE FASTENED SECURELY TO FENCE POSTS WITH WIRE TIES OR STAPLES. POSTS SHALL BE STEEL 2. FILTER FABRIC TO BE FASTENED SECURELY TO WOVEN WIRE FENCE WITH TIES SPACED EVERY 24" AT TOP AND MID SECTION. FENCE SHALL BE WOVEN WIRE, 6" MAX MESH OPENING. 3. WHEN TWO SECTIONS OF FILTER FABRIC ADJOIN EACH OTHER THEY SHALL BE OVERLAPPED BY 6" AND FOLDED. 4. MAINTENANCE SHALL BE PERFORMED AS NEEDED AND MATERIALS REMOVED WHEN "BULGES" DEVELOP IN THE SILT FENCE. 5. MAXIMUM DRAINAGE AREA FOR OVERLAND FLOW TO A SILT FENCE SHALL NOT EXCEED 1/4 ACRE PER 100 FEET OF FENCE. 6. SILT FENCE SHALL BE USED WHERE EROSION COULD OCCUR IN THE FORM OF SHEET EROSION. 7. SILT FENCE SHALL NOT BE USED WHEN A CONCENTRATION OF WATER IS FLOWING TO THE BARRIER. 8. MAXIMUM ALLOWABLE SLOPE LENGTHS CONTRIBUTING RUN-OFF TO A SILT FENCE ARE: SLOPE STEEPNESS MAXIMUM SLOPE LENGTH(FT)

OVERFLOW PORTS

- SILT SACK BY DANDY

PRODUCTS, INC. OR

APPROVED EQUAL

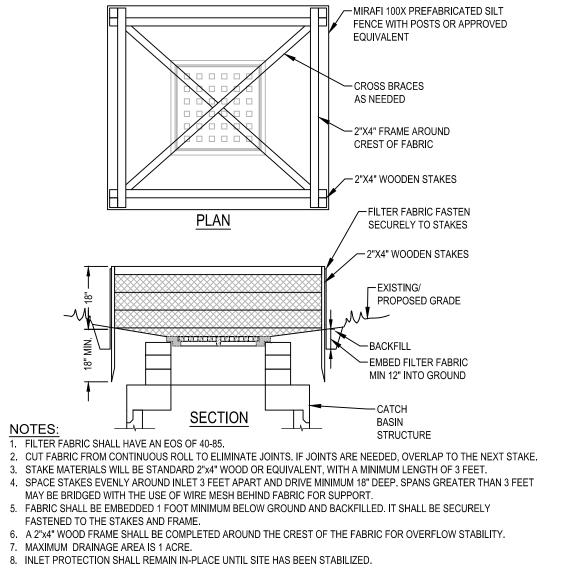
5:1 OR FLATTER SILT FENCE INSTALLATION DETAIL

— STORM SEWER GRATE

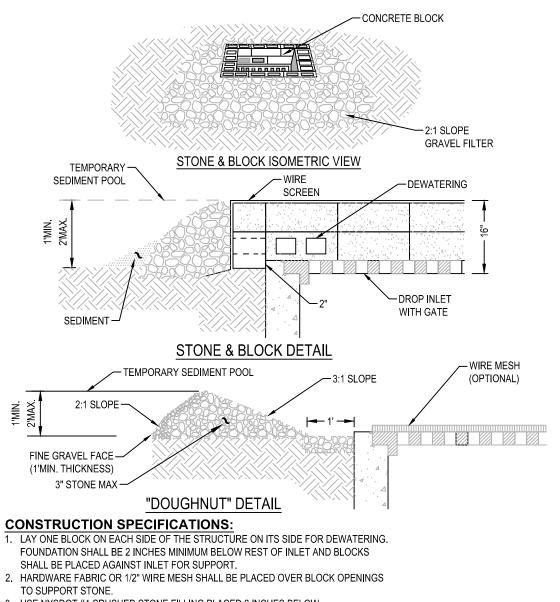
REINFORCED

CONTAINMENT

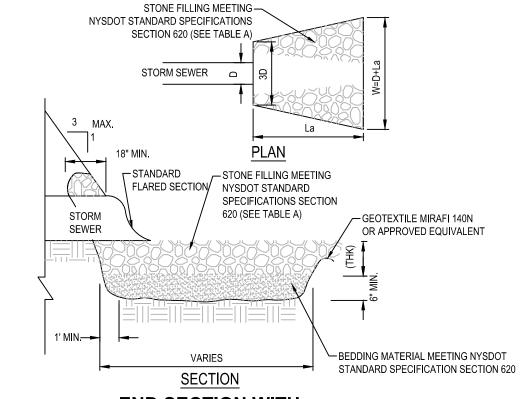
CORNERS



TEMPORARY OUT OF PAVEMENT FILTER FABRIC DROP INLET PROTECTION DETAIL SCALE: NOT TO SCALE



3. USE NYSDOT #4 CRUSHED STONE FILLING PLACED 2 INCHES BELOW TOP OF THE BLOCK ON A 2:1 SLOPE OR FLATTER. 4. FOR STONE STRUCTURES ONLY, A 1 FOOT THICK LAYER OF THE FILTER STONE WILL BE PLACED AGAINST THE 3 INCH STONE AS SHOWN ON THE DRAWINGS. MAXIMUM DRAINAGE AREA 1 ACRE. 5. MAXIMUM DRAINAGE AREA IS 1 ACRE. CATCH BASIN STONE AND BLOCK INLET PROTECTION DETAIL



STONE APRON SIZING REQUIREMENT - TABLE "A"

STANDARD STONE

FILLING APRON

MATERIAL

MEDIUM

MEDIUM

HEAVY

MEDIUM

MEDIUM

HEAVY

MEDIUM

HEAVY

DIA. (D) | SLOPE, %

< 4

MINIMUM

APRON

dMAX

14"-18"

15"-18" 22"-27"

15"-18" 22"-27"

9"-12" 14"-18"

9"-12" | 14"-18"

15"-18" 22"-27"

15"-18" 22"-27"

15"-18" 22"-27"

9"-12" 14"-18"

15"-18" 22"-27"

THICKNESS

OUTLET

APRON

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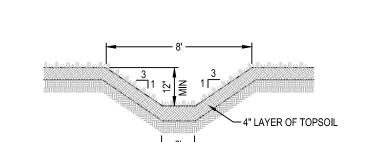
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Charlotte, NC 28285

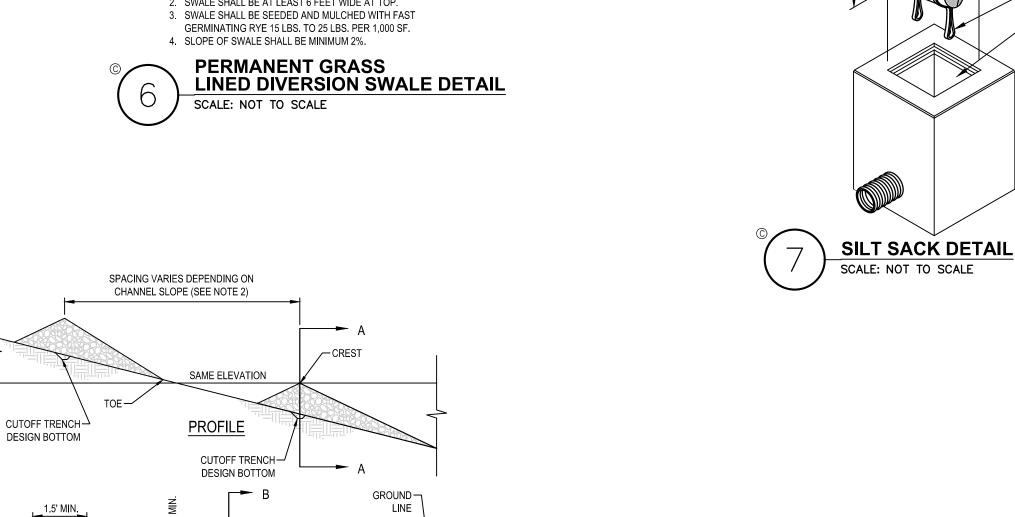
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END SECTION WITH STONE LINED APRON DETAIL

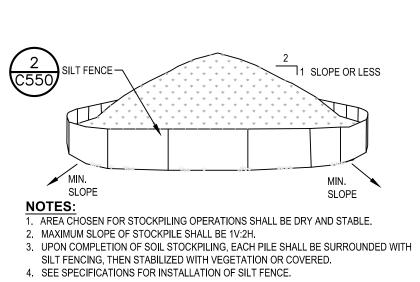


2. SWALE SHALL BE AT LEAST 6 FEET WIDE AT TOP. 3. SWALE SHALL BE SEEDED AND MULCHED WITH FAST GERMINATING RYE 15 LBS. TO 25 LBS. PER 1,000 SF. 4. SLOPE OF SWALE SHALL BE MINIMUM 2%.

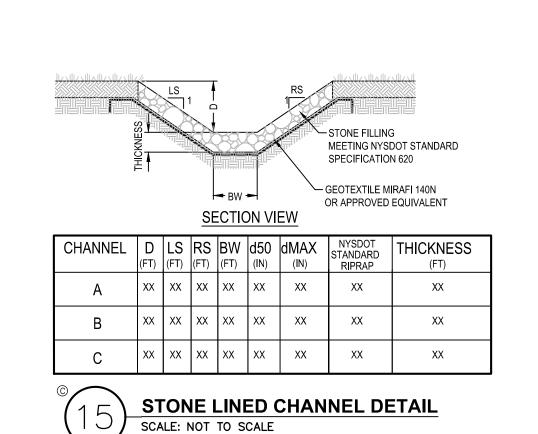


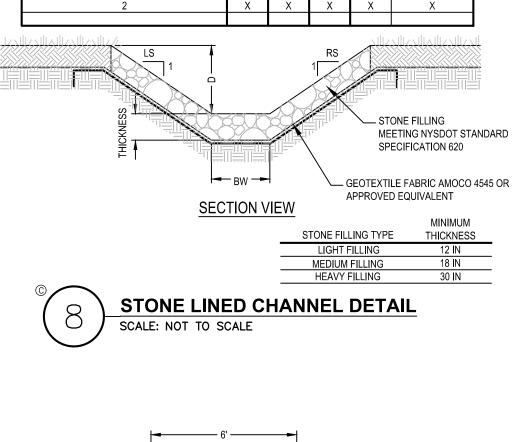
CUTOFF TRENCH DESIGN BOTTOM

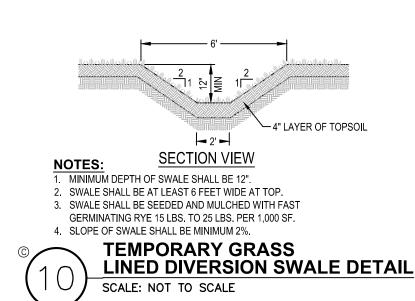
- GEOTEXTILE MIRAFI 140N OR APPROVED EQUIVALENT

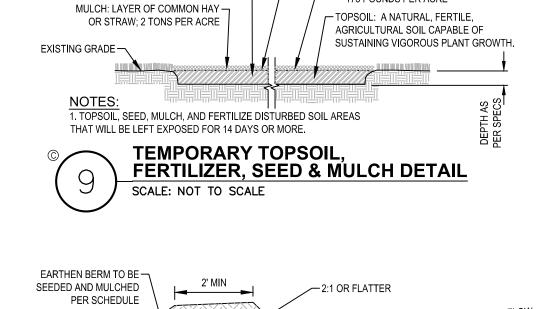












SOIL PH SHALL BE TESTED,

LIME SHALL BE APPLIED AS

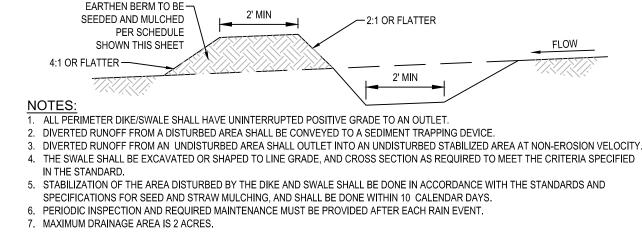
REQUIRED TO BRING SOIL PH TO 6.5

__TEMPORARY SEED, SEE VEGETATIVE

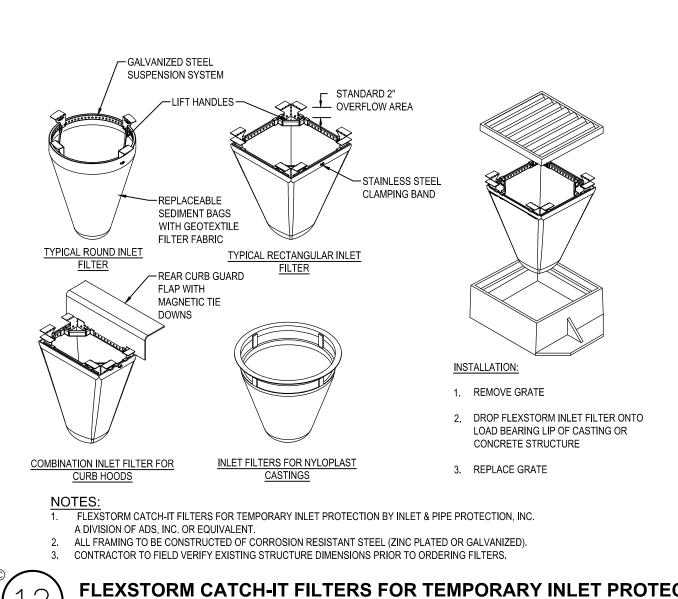
COVER SPECIFICATIONS THIS SHEET

FERTILIZER: COMMERCIAL 5-10-5,

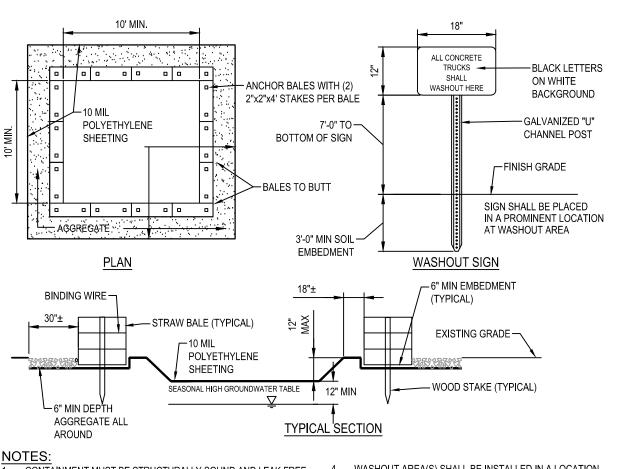
175 POUNDS PER ACRE







FLEXSTORM CATCH-IT FILTERS FOR TEMPORARY INLET PROTECTION

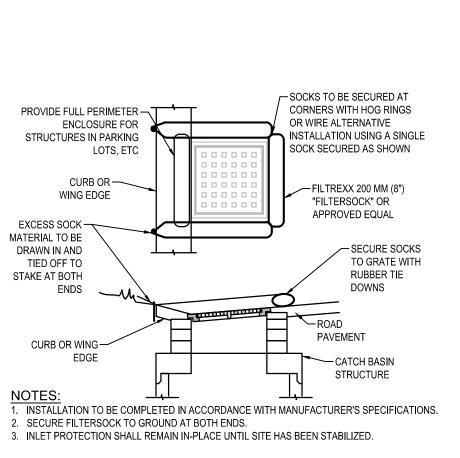


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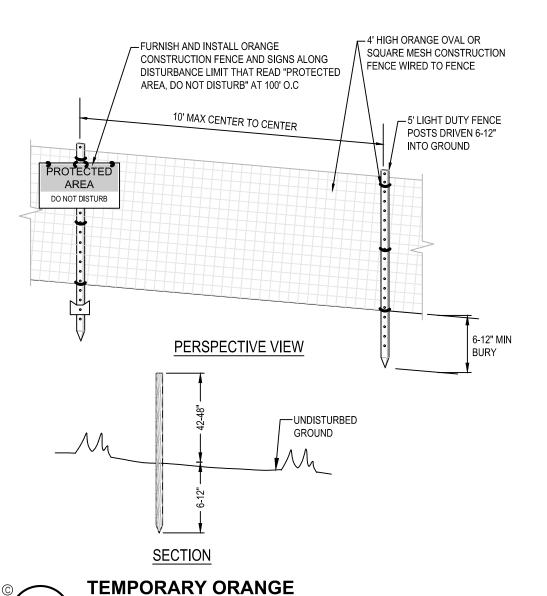
1. CONTAINMENT MUST BE STRUCTURALLY SOUND AND LEAK FREE

4. WASHOUT AREA(S) SHALL BE INSTALLED IN A LOCATION FASILY ACCESSIBLE BY CONCRETE TRUCKS. AND CONTAIN ALL LIQUID WASTES. 2. CONTAINMENT DEVICES MUST BE OF SUFFICIENT QUANTITY OR 5. ONE OR MORE AREAS MAY BE INSTALLED ON THE VOLUME TO COMPLETELY CONTAIN THE LIQUID WASTES CONSTRUCTION PROGRESSES. WASHOUT MUST BE CLEANED OR NEW FACILITIES CONSTRUCTED 6. AT LEAST WEEKLY, REMOVE ACCUMULATION OF SAND AND READY TO USE ONCE WASHOUT IS 75% FULL. THIS INCLUDES AND AGGREGATE AND DISPOSE OF PROPERLY. REPLACEMENT OF THE 10 MIL POLYETHLENE SHEETING.

CONCRETE WASHOUT AREA DETAIL







CONSTRUCTION FENCE DETAIL

SCALE: NOT TO SCALE

EROSION & SEDIMENT CONTROL DETAILS 1

DRAWING NAME:

PROJECT NUMBER:

DRAWN BY:

REVIEWED BY:

ISSUED FOR:

DRAWING NUMBER:

GEOTEXTILE MIRAFI 140N OR -APPROVED EQUIVALENT

STONE FILLING

CONSTRUCTION SPECIFICATIONS:

2. SET SPACING OF CHECK DAMS IN ACCORDANCE W/ THE FOLLOWING:

1'-9" HIGH CHECK DAM: (SPACING = 100xCHECK DAM HEIGHT (FT. CHANNEL SLOPE %

5. ENSURE THAT CHANNEL APPURTENANCES SUCH AS CULVERT

6. MAXIMUM DRAINAGE AREA IS 2 ACRES.

CHECK DAM SPACING INCREMENT 2'-6" DEEP DITCH/SWALE W/

SECTION B-E

CONTRACTOR TO ADJUST SPACING ACCORDINGLY BASED ON ACTUAL DEPTH & SLOPE OF DITCH.

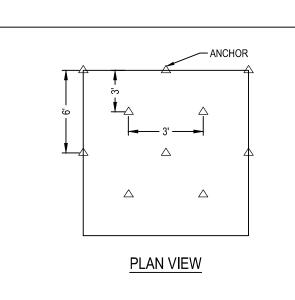
3. EXTEND THE STONE A MINIMUM OF 1.5 FEET BEYOND THE DITCH BANKS TO PREVENT CUTTING AROUND THE DAM.

ENTRANCES BELOW CHECK DAM ARE NOT SUBJECT TO DAMAGE OR BLOCKAGE FROM DISPLACED STONE.

STONE CHECK DAM DETAIL

4. PROTECT THE CHANNEL DOWNSTREAM OF THE LOWEST CHECK DAM FROM SCOUR AND EROSION WITH STONE OR LINER

STONE SHALL BE PLACED ON A FILTER FABRIC FOUNDATION TO THE LINES, GRADES AND LOCATIONS SHOWN ON THE PLAN.



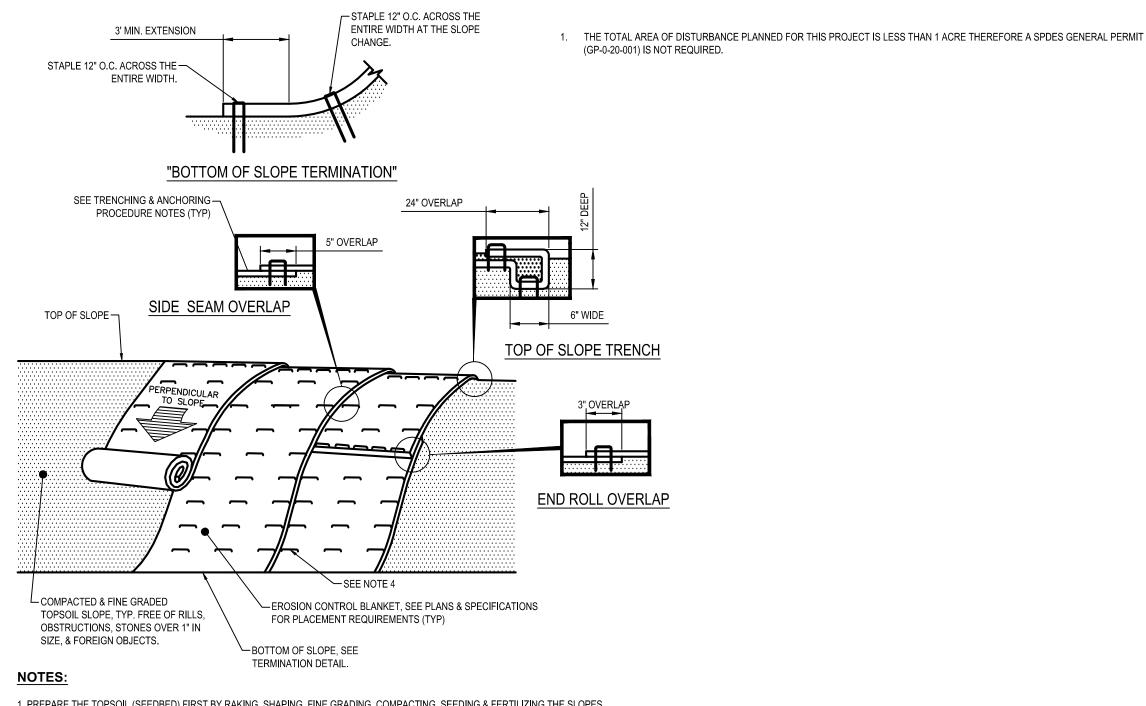
- ANCHOR (TYP) LANDLOK TRM 450 TOPSOIL AND SEED AFTER TO INSTALLATION OF LANDLOK TRM 450 -COMPACTED BACKFILL

SECTION VIEW

LANDLOK TRM 450 TURF REINFORCEMENT NOTES: INSTALL LANDLOK TRM 450 TURF REINFORCEMENT PER MANUFACTURER'S RECOMMENDATIONS.

- . GRADE AND COMPACT AREA OF INSTALLATION, REMOVING ALL ROCKS, VEGETATION, ETC. 3. EXTEND TRM 3'-0" OVER CREST OF SLOPE AND EXCAVATE A 12"X12" TERMINAL ANCHOR TRENCH.
- 4. ANCHOR TRM IN TRENCH @ 1'-0" SPACING, BACKFILL AND COMPACT SOIL.
- 5. UNROLL TRM DOWN SLOPE WITH SMALL NETTING ON BOTTOM, LARGE NETTING ON TOP. (ON SLOPES > 3:1, NETTING TO BE UNROLLED DOWN SLOPE)
- 6. OVERLAP ADJACENT ROLLS AT LEAST 6" AND ANCHOR EVERY 12".
- 7. LAY TRM LOOSE TO MAINTAIN DIRECT CONTACT WITH SOIL (DO NOT PULL TAUGHT).
- 8. SECURE TRM TO GROUND SURFACE USING U-SHAPED WIRE STAPLES. 9. TRM TO BE ANCHORED IN A CHECKERBOARD PATTERN (SEE PLAN VIEW).
- 10. 3" MINIMUM TOPSOIL AND SEED AFTER INSTALLATION OF TURF REINFORCEMENT.





1. PREPARE THE TOPSOIL (SEEDBED) FIRST BY RAKING, SHAPING, FINE GRADING, COMPACTING, SEEDING & FERTILIZING THE SLOPES. 2. USE THE TRENCHING & ANCHORING PROCEDURES DETAILED HEREIN TO SECURE ANY EXPOSED MATERIAL ENDS. SECURE ALL PRODUCT OVERLAPS. OVERLAP IN THE DIRECTION OF WATER FLOW, PERPENDICULAR TO THE SLOPE.

3. KEEP EROSION CONTROL BLANKET IN SOLID CONTACT WITH THE TOPSOIL.

4. USE THE REQUIRED NUMBER OF STAPLES/STAKES TO SECURELY FASTEN THE EROSION CONTROL BLANKET TO THE SLOPE. IN LOOSE SOIL CONDITIONS, THE USE OF STAPLES/STAKES LENGTHS GREATER THAN 6" MAYBE NECESSARY FOR PROPER SECURING. STAPLE PATTERNS & OVERLAPS ARE DEPENDENT ON SITE CONDITIONS & MANUFACTURER'S REQUIREMENTS. CONTRACTOR SHALL CONSULT WITH MANUFACTURER FOR ACTUAL SITE SPECIFIC REQUIREMENTS.

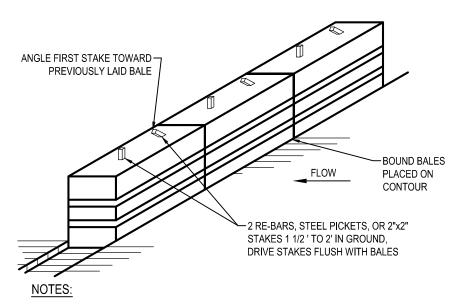
TRENCHING & ANCHORING PROCEDURE NOTES:

SIDE SEAM OVERLAP: THE EDGES OF PARALLEL BLANKETS SHALL BE STAPLED WITH A 5" OVERLAP.

TOP OF SLOPE TRENCH: BEGIN AT THE TOP OF SLOPE BY ANCHORING THE EROSION CONTROL BLANKET IN A 6"D x 6"W TRENCH WITH A 12" OVERLAP EXTENDED BEYOND THE UP-SLOPE PORTION OF THE TRENCH, ANCHOR WITH A ROW OF STAPLES/STAKES 12" O.C. IN THE BOTTOM OF THE TRENCH. BACKFILL & COMPACT THE TRENCH AFTER STAPLING. APPLY SEED TO THE COMPACTED SOIL & FOLD THE REMAINING 12" PORTION OF THE EROSION CONTROL BLANKET BACK OVER THE SEED & COMPACTED SOIL. SECURE THE EROSION CONTROL BLANKET OVER THE COMPACTED SOIL WITH A ROW OF STAPLES/STAKES SPACED 12" O.C. ACROSS THE ENTIRE WIDTH.

END ROLL OVERLAP: CONSECUTIVE BLANKETS SPLICED DOWN THE SLOPE SHALL BE PLACED END OVER END (SHINGLE-STYLE) WITH A 3" OVERLAP. STAPLE THRU OVERLAPPED AREAS, 12" APART ACROSS THE ENTIRE WIDTH.

EROSION CONTROL BLANKET INSTALLATION DETAIL



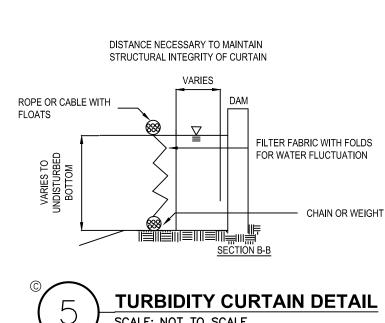
1. BALES SHALL BE PLACED AT THE TOE OF A SLOPE OR ON THE CONTOUR AND IN A ROW WITH ENDS TIGHTLY ABUTTING

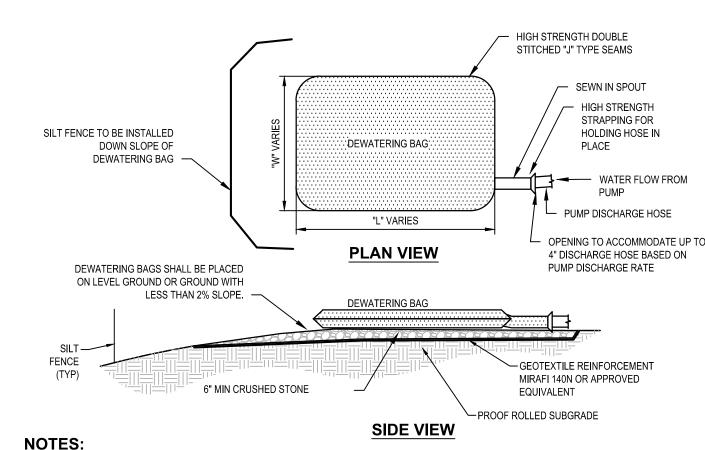
- 2. EACH BALE SHALL BE EMBEDDED IN THE SOIL A MINIMUM OF (4)INCHES AND PLACED SO THE BINDINGS ARE HORIZONTAL. 3. BALES SHALL BE SECURELY ANCHORED IN PLACE BY EITHER TWO STAKES OR RE-BARS DRIVEN THROUGH THE BALE THE FIRST STAKE IN EACH BALE SHALL BE DRIVEN TOWARD THE PREVIOUSLY LAID BALE AT AN ANGLE TO FORCE THE
- BALES TOGETHER. STAKES SHALL BE DRIVEN FLUSH WITH THE BALE. 4. INSPECTION SHALL BE FREQUENT AND REPAIR REPLACEMENT SHALL BE MADE PROMPTLY AS NEEDED.
- 5. BALES SHALL BE REMOVED WHEN THEY HAVE SERVED THEIR USEFULNESS SO AS NOT TO BLOCK OR IMPEDE STORM
- 6. HAY OR STRAW BALE DIKES SHALL BE USED WHERE EROSION COULD OCCUR IN THE FORM OF SHEET EROSION.
- 7. HAY OR STRAW BALE DIKES SHALL NOT BE USED WHEN A CONCENTRATION OF WATER IS FLOWING TO THE BARRIER.
- 8. MAXIMUM ALLOWABLE SLOPE LENGTHS CONTRIBUTING TO A HAY OR STRAW BALE DIKE ARE:

MAXIMUM SLOPE LENGTH(FT

9. MAXIMUM DRAINAGE AREA FOR OVERLAND FLOW TO A HAY OR STRAW BALE DIKE SHALL NOT EXCEED 0.25 ACRES PER 100 FEET OF DIKE FOR SLOPES < 25%.







SEDIMENT COLLECTION BAG SHALL BE EQUAL TO DIRTBAG® 55, AS MARKETED BY ACF ENVIRONMENTAL. RICHMOND. VIRGINIA (800-448-3636), OR

2. SEDIMENT COLLECTION BAG SHALL BE A NONWOVEN BAG SEWN WITH HIGH STRENGTH THREAD. THE SEAMS SHALL BE HIGH STRENGTH, DOUBLE STITCHED, "J" TYPE SEAMS.

BAGS SHALL HAVE SEWN IN FILL SPOUT LARGE ENOUGH TO ACCOMMODATE UP TO A 4" DISCHARGE HOSE. FILL SPOUT SHALL HAVE HIGH STRENGTH STRAPPING TO HOLD HOSE IN PLACE AND PREVENT PUMPED WATER FROM ESCAPING WITHOUT BEING FILTERED.

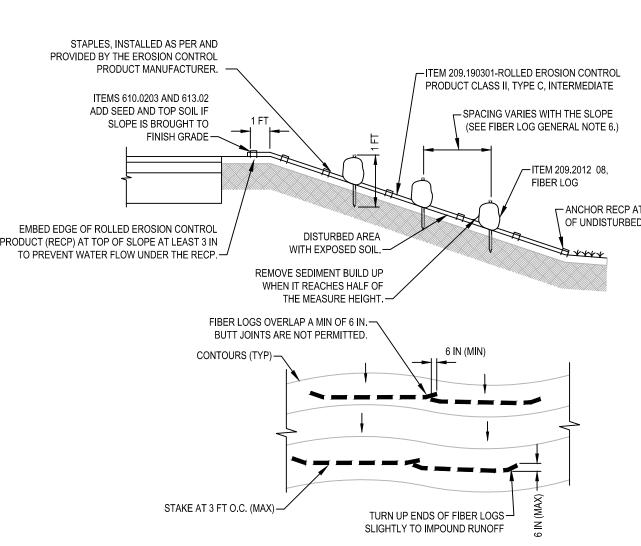
4. SEDIMENT COLLECTION BAGS SHALL BE INSTALLED IN ACCORDANCE WITH THE MANUFACTURERS INSTRUCTIONS, OR AS DIRECTED BY THE

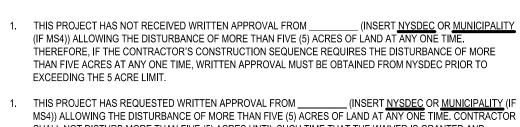
5. SEDIMENT COLLECTED SHALL BE DISPOSED OF AT AN APPROPRIATE FACILITY.

6. SEDIMENT COLLECTION BAGS SHALL BE REMOVED AND REPLACED UNDER ANY OF THE FOLLOWING CONDITIONS: WHEN BAGS ARE FULI • WHEN BAGS HAVE BEEN IN PLACE FOR MORE THAN 30 DAYS (REMOVAL REQUIRED DUE TO ULTRAVIOLET DETERIORATION). WHEN BAGS ARE DAMAGED.

4. ALL SEDIMENT COLLECTION BAGS SHALL BE INSPECTED DAILY BY THE CONTRACTOR.

5. CARE SHALL BE TAKEN DURING REMOVAL TO MINIMIZE LOSS OF ENTRAPPED SEDIMENT





SHALL NOT DISTURB MORE THAN FIVE (5) ACRES UNTIL SUCH TIME THAT THE WAIVER IS GRANTED AND WRITTEN AUTHORIZATION IS RECEIVED FROM NYSDEC. CONSTRUCTION SEQUENCING NOTES

PRIOR TO COMMENCING ANY CLEARING, GRUBBING, EARTHWORK ACTIVITIES, ETC.AT THE SITE, THE

SPDES GENERAL PERMIT GP-0-20-001 COMPLIANCE NOTES:

CONSIDERED COMPLETE WITHOUT THE SWPPP.

THIS PLAN SET AND THE ACCOMPANYING SWPPP ENTITLED "INAMEI" HAVE BEEN SUBMITTED AS A SET. THESE

ENGINEERING DRAWINGS ARE CONSIDERED AN INTEGRAL PART OF THE SWPPP, THEREFORE THE PLAN SET IS NOT

CONTRACTOR SHALL FLAG THE WORK LIMITS AND SHALL INSTALL TEMPORARY EROSION AND SEDIMENT CONTROL MEASURES (I.E. SILT FENCES, TREE PROTECTION/BARRIER FENCES, STABILIZED CONSTRUCTION ENTRANCES. STORM DRAIN SEDIMENT FILTERS, DRAINAGE DITCH SEDIMENT FILTERS, ETC.) INDICATED ON THE PROJECT DRAWINGS. TEMPORARY EROSION AND SEDIMENT CONTROL MEASURES MUST BE CONSTRUCTED, STABILIZED, AND FUNCTIONAL BEFORE SITE DISTURBANCE BEGINS WITHIN THEIR TRIBUTARY 2. THE CONTRACTOR SHALL CLEAR AND GRUB THE AREA OF THE STORMWATER MANAGEMENT FACILITIES, THIS AREA SHALL NOT EXCEED FIVE (5) ACRES IN EXTENT WITHOUT TEMPORARY STABILIZATION. 3. THE STORMWATER DETENTION BASIN SHALL BE UTILIZED AS A TEMPORARY SEDIMENT TRAP DURING

CONSTRUCTION. THE CONTRACTOR SHALL INSTALL THE OUTLET CONTROL STRUCTURES AND THE EARTHEN BERM. THE BASIN SHALL BE GRADED TO THE TOP OF THE AQUATIC BENCH AS INDICATED IN THE TYPICAL STORMWATER MANAGEMENT BASIN SECTION PRESENTED IN THE PROJECT DRAWINGS. 4. PRIOR TO COMMENCING CLEARING, GRUBBING AND/OR EARTHWORK ACTIVITIES IN ANY OTHER AREA OF THE SITE, THE CONTRACTOR SHALL INSTALL INLET AND OUTLET PROTECTION MEASURES (RIPRAP OVERFLOW WEIR(S), CULVERT INLET/OUTLET PROTECTION, ETC.) AND SHALL STABILIZE THE AREAS DISTURBED DURING

THE CONSTRUCTION OF THE SEDIMENT BASIN. 5. THE CONTRACTOR SHALL INSTALL TEMPORARY DIVERSION MEASURES WITH ASSOCIATED STABILIZATION MEASURES (I.E., VEGETATIVE COVER, DRAINAGE DITCH SEDIMENT FILTERS, STORM DRAIN SEDIMENT FILTERS, ETC.)TO ASSURE THAT STORMWATER RUNOFF IS CONVEYED TO THE TEMPORARY SEDIMENT BASIN. 6. TEMPORARY DIVERSION MEASURES SHALL BE LOCATED IN A MANNER THAT WILL ASSURE THAT THE AREA TRIBUTARY TO EACH DIVERSION DOES NOT EXCEED FIVE (5) ACRES. THESE TEMPORARY DIVERSION

MEASURES SHALL BE INSPECTED DAILY AND REPAIRED/STABILIZED AS NECESSARY TO MINIMIZE EROSION. 7. THE CONTRACTOR SHALL COMMENCE SITE CONSTRUCTION ACTIVITIES INCLUDING CLEARING & GRADING OF THE PROPOSED AREA OF DISTURBANCE AS REQUIRED.

OF ALL EXPOSED STORM SEWER PIPES. 9. CONSTRUCT ALL UTILITIES, CURB AND GUTTER, GUTTER INLETS, AREA INLETS, AND STORM SEWER MANHOLES. AS SHOWN ON THE PLANS. INLET PROTECTION MAY BE REMOVED TEMPORARILY FOR THIS CONSTRUCTION, PLACE REQUIRED RIP-RAP AT LOCATIONS SHOWN ON THE PLANS.

8. INSTALL PROTECTIVE MEASURES AT THE LOCATIONS OF ALL GRATE INLETS, CURB INLETS, AND AT THE ENDS

10. FINALIZE PAVEMENT SUB-GRADE PREPARATION. 11. REMOVE PROTECTIVE MEASURES AROUND INLETS AND MANHOLES NO MORE THAN 24 HOURS PRIOR TO PLACING STABILIZED BASE COURSE. 12. INSTALL SUB-BASE MATERIAL AS REQUIRED FOR PAVEMENT.

3. PRIOR TO FINALIZING CONSTRUCTION OF THE STORMWATER MANAGEMENT FACILITY, ALL CATCH BASINS AND DRAINAGE LINES SHALL BE CLEANED OF ALL SILT AND SEDIMENT. 14. UPON COMPLETION OF SITE CONSTRUCTION ACTIVITIES, THE CONTRACTOR SHALL FINALIZE CONSTRUCTION OF THE STORMWATER MANAGEMENT FACILITY. CONTRACTOR SHALL FINISH GRADE THE FORBAY(S), AQUATIC

15. THE CONTRACTOR SHALL REMOVE ALL TEMPORARY EROSION AND SEDIMENT CONTROL MEASURES AND IMMEDIATELY ESTABLISH PERMANENT VEGETATION ON THE AREAS DISTURBED DURING THEIR REMOVAL.

BENCHES, AND WET POOL(S) AND STABILIZE AS INDICATED IN THE PROJECT DRAWINGS.

EROSION AND SEDIMENT CONTROL MEASURES: DAMAGE TO SURFACE WATERS RESULTING FROM EROSION AND SEDIMENTATION SHALL BE MINIMIZED BY STABILIZING DISTURBED AREAS AND BY REMOVING SEDIMENT FROM CONSTRUCTION SITE DISCHARGES. 2. AS MUCH AS IS PRACTICAL, EXISTING VEGETATION SHALL BE PRESERVED. FOLLOWING THE COMPLETION OF CONSTRUCTION ACTIVITIES IN ANY PORTION OF THE SITE, PERMANENT VEGETATION SHALL BE ESTABLISHED ON ALL EXPOSED SOILS

SITE PREPARATION ACTIVITIES SHALL BE PLANNED TO MINIMIZE THE SCOPE AND DURATION OF SOIL DISRUPTION. PERMANENT TRAFFIC CORRIDORS SHALL BE ESTABLISHED AND "ROUTES OF CONVENIENCE" SHALL BE AVOIDED. STABILIZED CONSTRUCTION ENTRANCES SHALL BE INSTALLED AT ALL POINTS OF ENTRY ONTO THE PROJECT SITE.

MAINTENANCE OF EROSION AND SEDIMENT CONTROL MEASURES NSPECT ALL AREAS THAT HAVE RECEIVED VEGETATION EVERY SEVEN DAYS & AFTER EVERY RAIN EVENT, ALL AREAS DAMAGED BY EROSION OR WHERE SEED HAS NOT ESTABLISHED SHALL BE REPAIRED AND RESTABILIZED IMMEDIATELY.

NSPECT THE ENTRANCE PAD EVERY SEVEN DAYS & AFTER EVERY RAIN EVENT. CHECK FOR MUD, SEDIMENT BUILD-UP AND PAD INTEGRITY. MAKE DAILY INSPECTIONS DURING WET WEATHER. RESHAPE PAD AS NEEDED FOR DRAINAGE AND RUNOFF CONTROL. WASH AND REPLACE STONE AS NEEDED. THE STONE IN THE ENTRANCE SHOULD BE WASHED OR REPLACED WHENEVER THE ENTRANCE FAILS TO REDUCE MUD BEING CARRIED OFF-SITE BY VEHICLES. IMMEDIATELY REMOVE MUD AND SEDIMENT TRACKED OR WASHED ONTO PUBLIC ROADS BY BRUSHING OR SWEEPING. REMOVE TEMPORARY CONSTRUCTION ENTRANCE AS SOON AS THEY ARE NO LONGER NEEDED TO PROVIDE ACCESS TO THE SITE.

INSPECT FOR DAMAGE EVERY SEVEN DAYS & AFTER EVERY RAIN EVENT. MAKE ALL REPAIRS IMMEDIATELY. REMOVE SEDIMENT FROM THE UP-SLOPE FACE OF THE FENCE BEFORE IT ACCUMULATES TO A HEIGHT EQUAL TO 1/3 THE HEIGHT OF THE FENCE. IF FENCE FABRIC TEARS, BEGINS TO DECOMPOSE, OR IN ANY WAY BECOMES INEFFECTIVE, REPLACE THE AFFECTED SECTION OF FENCE IMMEDIATELY.

NSPECT SEDIMENT CONTROL BARRIERS (SILT FENCE OR HAY BALE) AND VEGETATION FOR DAMAGE EVERY SEVEN DAYS & AFTER EVERY RAIN EVENT. MAKE ALL REPAIRS IMMEDIATELY. REMOVE SEDIMENT FROM THE UP-SLOPE FACE OF THE SEDIMENT CONTROL BARRIER BEFORE IT ACCUMULATES TO A HEIGHT EQUAL TO 1/3 THE HEIGHT OF THE SEDIMENT CONTROL BARRIER. IF SEDIMENT CONTROL BARRIER TEARS, BEGINS TO DECOMPOSE, OR IN ANYWAY BECOMES INEFFECTIVE, REPLACE THE AFFECTED SECTION OF SEDIMENT CONTROL BARRIER IMMEDIATELY. REVEGETATE DISTURBED AREA TO STABILIZE SOIL STOCK PILE. REMOVE THE SEDIMENT CONTROL BARRIER WHEN THE SOIL STOCKPILE HAS BEEN REMOVED

SCHEDULE CONSTRUCTION OPERATIONS TO MINIMIZE THE AMOUNT OF DISTURBED AREAS AT ANY ONE TIME DURING THE COURSE OF WORK, APPLY TEMPORARY SOIL STABILIZATION PRACTICES SUCH AS MULCHING, SEEDING, AND SPRAYING (WATER). STRUCTURAL MEASURES (MULCH, SEEDING) SHALL BE INSTALLED IN DISTURBED AREAS BEFORE SIGNIFICANT BLOWING PROBLEMS DEVELOP. WATER SHALL BE SPRAYED AS NEEDED. REPEAT AS NEEDED, BUT AVOID EXCESSIVE SPRAYING, WHICH COULD CREATE RUNOFF AND EROSION PROBLEMS.

NSPECT CHECK DAMS EVERY SEVEN DAYS & AFTER EVERY RAIN EVENT. IF SIGNIFICANT EROSION HAS OCCURRED BETWEEN STRUCTURES A LINER OF STONE OR OTHER SUITABLE MATERIAL SHOULD BE INSTALLED IN THAT PORTION OF THE CHANNEL. REMOVE SEDIMENT ACCUMULATED BEHIND THE DAM AS NEEDED TO ALLOW CHANNEL TO DRAIN THROUGH THE STONE CHECK DAM AND PREVENT LARGE FLOWS FROM CARRYING SEDIMENT OVER THE DAM. REPLACE STONES AS NEEDED TO MAINTAIN THE DESIGN CROSS SECTION OF THE STRUCTURES. REMOVE CHECK DAMS AS PER

INSPECT THE BLANKET EVERY SEVEN DAYS & AFTER EVERY RAIN EVENT. REPLACE WIRE STAPLES AS REQUIRED. REPAIR AND RESEED WHERE CRACKS AND DAMAGED VEGETATION IS EVIDENT. WHEN DAMAGED BEYOND REPAIR OR NO LONGER FUNCTIONING, THE BLANKET SHALL BE REPLACED.

<u>EARTH DIKE:</u>
INSPECT ALL EARTH DIKES EVERY SEVEN DAYS & AFTER EVERY RAIN EVENT. ALL AREAS DAMAGED BY EROSION SHALL

NSPECT ALL EARTH DIKES EVERY SEVEN DAYS & AFTER EVERY RAIN EVENT. ALL AREAS DAMAGED BY EROSION SHALL BE REPAIRED IMMEDIATELY.

INSPECT ALL SEDIMENT TRAPS EVERY SEVEN DAYS & AFTER EVERY RAIN EVENT. REPAIRS SHALL BE MADE AS NEEDED. SEDIMENT SHALL BE REMOVED AND THE TRAP RESTORED TO THE ORIGINAL DIMENSIONS WHEN SEDIMENT HAS ACCUMULATED TO 1/2 OF THE DESIGN DEPTH OF THE TRAP.

NSPECT ALL STORM DRAIN INLET PROTECTION DEVICES EVERY SEVEN DAYS & AFTER EVERY RAIN EVENT. MAKE REPAIRS AS NEEDED, REMOVE SEDIMENT FROM THE POOL AREA AS NECESSARY.

IF REQUIRED) - INSPECT DAILY DURING OPERATION FOR CLOGGING OR OVERFLOW. CLEAR INLET AND DISCHARGE PIPES OF OBSTRUCTIONS. IF A FILTER MATERIAL BECOMES CLOGGED WITH SEDIMENT, PIT SHALL BE DISMANTLED AND CONSTRUCT NEW PITS AS NEEDED

PARKING LOTS, ROADWAYS, AND DRIVEWAYS ADJACENT TO WATER QUALITY FILTERS SHALL NOT BE SANDED DURING SNOW EVENTS DUE TO HIGH POTENTIAL FOR CLOGGING FROM SAND IN SURFACE WATER RUNOFF. USE SALT ONLY FOR

GENERAL EROSION AND SEDIMENT CONTROL NOTE

ALL EROSION AND SEDIMENT CONTROL MEASURES ARE TO BE IN STRICT COMPLIANCE WITH "NEW YORK STATE STANDARDS AND SPECIFICATIONS FOR EROSION AND SEDIMENT CONTROL". NOVEMBER 2016. EXCESS SOIL TO BE STOCKPILED WITHIN THE LIMITS OF SITE DISTURBANCE IF NOT USED IMMEDIATELY FOR GRADING PURPOSES. INSTALL SILT FENCE AROUND SOIL STOCKPILES.

3. APPLY SURFACE STABILIZATION AND RESTORATION MEASURES. AREAS UNDERGOING CLEARING OR GRADING AND ANY AREAS DISTURBED BY CONSTRUCTION ACTIVITIES WHERE WORK IS DELAYED. SUSPENDED. OR INCOMPLETE AND WILL NOT BE REDISTURBED FOR 21 DAYS OR MORE SHALL BE STABILIZED WITH TEMPORARY VEGETATIVE COVER WITHIN 14 DAYS AFTER CONSTRUCTION ACTIVITY IN THAT PORTION OF THE SITE HAS CEASED. (SEE SPECIFICATIONS FOR TEMPORARY VEGETATIVE COVER). AREAS UNDERGOING CLEARING OR GRADING AND ANY AREAS DISTURBED BY CONSTRUCTION ACTIVITIES WHERE WORK IS COMPLETE AND WILL NOT BE REDISTURBED AVAILABLE AND WITHIN 14 DAYS AFTER WORK IS COMPLETE. (SEE SPECIFICATIONS FOR PERMANENT VEGETATIVE COVER), SEEDING FOR PERMANENT VEGETATIVE COVER SHALL BE WITHIN THE SEASONAL LIMITATIONS. PROVIDE STABILIZATION WITH TEMPORARY VEGETATIVE COVER WITHIN 14 DAYS AFTER WORK IS COMPLETE, FOR SEEDING OUTSIDE PERMITTED SEEDING PERIODS 4. SEEDED AREAS TO BE MULCHED WITH STRAW OR HAY MULCH IN ACCORDANCE WITH VEGETATIVE COVER

SPECIFICATIONS. 5. THE CONTRACTOR IS RESPONSIBLE FOR THE INSTALLATION AND MAINTENANCE OF ALL EROSION AND SEDIMENT CONTROL MEASURES THROUGHOUT THE COURSE OF CONSTRUCTION.

6. THE CONTRACTOR IS RESPONSIBLE FOR CONTROLLING DUST BY SPRINKLING EXPOSED SOIL AREAS PERIODICALLY WITH WATER AS REQUIRED. THE CONTRACTOR IS TO SUPPLY ALL EQUIPMENT AND WATER. 7. WHEN ALL DISTURBED AREAS ARE STABLE, ALL TEMPORARY EROSION AND SEDIMENT CONTROL MEASURES SHALL BE REMOVED.

BURLAP FILTER -

3" DIA. HOSE TO SUITABLE -

TOPSOIL SPECIFICATIONS

EXISTING EXCESS TOPSOIL SHALL BE REMOVED AND STORED IN TOPSOIL STOCKPILES SUFFICIENTLY REMOVED FROM OTHER EXCAVATION OR DISTURBANCE TO AVOID MIXING, SILT FENCE SHALL BE INSTALLED AROUND TOPSOIL STOCKPILE AREAS.

COMPLETE ROUGH GRADING AND FINAL GRADE, ALLOWING FOR DEPTH OF TOPSOIL TO BE ADDED. SCARIFY ALL COMPACT, SLOWLY PERMEABLE, MEDIUM AND FINE TEXTURED SUBSOIL AREAS. SCARIFY AT APPROXIMATELY RIGHT ANGLES TO THE SLOPE DIRECTION IN SOIL AREAS THAT ARE STEEPER THAN 5%. REMOVE REFUSE, WOODY PLANT PARTS, STONES OVER 3 INCHES IN DIAMETER, AND OTHER LITTER.

400 S. Tryon Street, Suite 1300

CORPORATE ENGINEERING

LICENSE NO. C-0430

CERT NO.

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SUITE 430

STAMFORD, CT 06902

Charlotte, NC 28285

704-376-6423

labellapc.com

NEW TOPSOIL SHALL BE BETTER THAN OR EQUAL TO THE QUALITY OF THE EXISTING ADJACENT TOPSOIL. IT SHALL MEET THE A. ORIGINAL LOAM TOPSOIL, WELL DRAINED HOMOGENEOUS TEXTURE AND OF UNIFORM GRADE, WITHOUT THE ADMIXTURE OF SUBSOIL MATERIAL AND FREE OF DENSE MATERIAL, HARDPAN, CLAY, STONES, SOD OR OTHER OBJECTIONABLE MATERIAL. CONTAINING NOT LESS THAN 5% NOR MORE THAN 20% ORGANIC MATTER IN THAT PORTION OF A SAMPLING PASSING A 1/4"

SIEVE WHEN DETERMINED BY THE WET COMBUSTION METHOD ON A SAMPLE DRIED AT 105°C. CONTAINING A PH VALUE WITHIN THE RANGE OF 6.5 TO 7.5 ON THAT PORTION OF THE SAMPLE WHICH PASSES A 1/4" SIEVE. CONTAINING THE FOLLOWING WASHED GRADATIONS: SIEVE DESIGNATION % PASSING 97-100

NO 200 20-60 APPLICATION AND GRADING:

SEEDING

TOPSOIL SHALL BE DISTRIBUTED TO A UNIFORM DEPTH OF 4" OVER THE AREA. IT SHALL NOT BE PLACED WHEN IT IS PARTLY FROZEN, MUDDY, OR ON FROZEN SLOPES OR OVER ICE, SNOW, OR STANDING WATER. TOPSOIL PLACED AND GRADED ON SLOPES STEEPER THAN 5% SHALL BE PROMPTLY FERTILIZED, SEEDED, MULCHED AND STABILIZED BY "TRACKING" WITH SUITABLE EQUIPMENT.

/EGETATIVE COVER SPECIFICATIONS: TEMPORARY VEGETATIVE COVER (DURING CONSTRUCTION):

SITE PREPARATION (SAME AS PERMANENT VEGETATIVE COVER)

SEED MIX: (APPLY AT RATE OF 3 TO 4 LBS PER 1000 SF) ANNUAL RYEGRASS

(SAME AS PERMANENT VEGETATIVE COVER)

PERMANENT VEGETATIVE COVER (AFTER CONSTRUCTION): BRING AREA TO BE SEEDED TO REQUIRED GRADE. A MINIMUM OF 4" OF TOPSOIL IS REQUIRED. PREPARE SEEDBED BY LOOSENING SOIL TO A DEPTH OF 4 INCHES.

REMOVE ALL STONES OVER 1 INCH IN DIAMETER, STICKS AND FOREIGN MATTER FROM THE SURFACE. LIME TO PH OF 6.5. FERTILIZER: USE 5-10-5 (NPK) OR EQUIVALENT, APPLY AT RATE OF 4 LBS/1000 SF. INCORPORATE LIME AND FERTILIZER IN THE TOP 4 INCHES OF TOPSOIL.

SMOOTH AND FIRM THE SEEDBED. SEED MIXTURE FOR USE ON LAWN AREAS: PROVIDE FRESH, CLEAN, NEW-CROP SEED MIXED IN THE PROPORTIONS SPECIFIED FOR SPECIES AND VARIETY, AND CONFORMING

TO FEDERAL AND STATE STANDARDS. LAWN SEED MIX: (APPLY AT RATE OF 5 TO 6 LBS PER 1000 SF)

SUN AND PARTIAL SHADE: WEIGHT SPECIES OR VARIETY
50% KENTUCKY BLUE GRASS PERENNIAI RYE CREEPING RED FESCUE

*MINIMUM 2 (EQUAL PROPORTIONS) VARIETIES AS LISTED IN CORNELL RECOMMENDATIONS FOR TURFGRASS.

WEIGHT SPECIES OR VARIETY
25% KENTUCKY BLUE GRASS PERENNIAL RYE 90% CREEPING RED FESCUE CHEWINGS RED FESCUE 97% **SHADE TOLERANT VARIETY

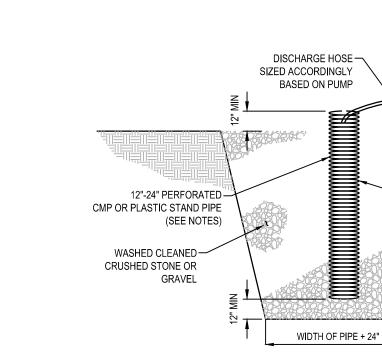
A. APPLY SEED UNIFORMLY BY CYCLONE SEEDER CULTI-PACKER OR HYDRO-SEEDER AT RATE INDICATED. B. ALL SEEDED AREAS SHALL BE PROTECTED FROM EROSION BY ONE OF THE FOLLOWING METHODS: A UNIFORM BLANKET OF STRAW APPLIED AT A RATE OF 2 TONS /ACRE MIN., TO BE APPLIED ONCE SEEDING IS COMPLETE.

ALL SEEDED SLOPES 3:1 OR GREATER SHALL BE PROTECTED FROM EROSION WITH JUTE MESH OR APPROVED EQUAL. IRRIGATE TO FULLY SATURATE SOIL LAYER, BUT NOT TO DISLODGE PLANTING SOIL. UNLESS OTHERWISE DIRECTED IN WRITING, SEED FROM MARCH 15TH TO JUNE 15TH, AND FROM AUGUST 15TH TO OCTOBER

WOOD FIBER CELLULOSE APPLIED WITH SEED MIX BY HYDROSEEDER AT RATE OF 2.000 LBS/ACRE.

COMPACTION REQUIREMENTS

| LOCATION | COMPACTION | TESTING FREQUENCY |
|---|----------------|--|
| PIPE TRENCH BACKFILL (IN PAVED AREAS) | 95% ASTM D1557 | 1 SERIES OF TESTS FOR EACH 150 FT OR LESS OF TRENCH LENGTH. SERIES INCLUDE 3 COMPACTION TESTS SPREAD EVENLY ALONG TRENCH PROFILE. |
| PIPE TRENCH BACKFILL (IN UNPAVED AREAS) | 90% ASTM D1557 | 1 SERIES OF TESTS FOR EACH 150 LF OR LESS OF TRENCH LENGTH. SERIES INCLUDE 3 COMPACTION TESTS SPREAD EVENLY ALONG TRENCH PROFILE. |
| PIPE BEDDING AND PIPE ZONE BACKFILL | 95% ASTM D1557 | 1 TEST FOR EACH 150 FT OR LESS OF TRENCH LENGTH. |
| PAVEMENT SUBBASE AND LAST LIFT OF SELECT GRANULAR FILL (FILL BETWEEN SHEET PILES) | 95% ASTM D1557 | 1 TEST FOR EVERY 2,000 SQ FT, OF LIFT AREA BUT NO FEWER THAN TWO TESTS PER LIFT |



1. SUMP PIT QUANTITY & LOCATION SHALL BE DETERMINED BY CONTRACTOR.

PERFORATIONS IN THE STANDPIPE SHALL BE EITHER CIRCULAR OR SLOTS. PERFORATION SIZE SHALL NOT EXCEED 1/2" INCH DIAMETER, PUMP RATE SHALL NOT EXCEED INFLOW RATE INTO STAND PIPE.

TO DEWATERING BAG

- TOP OF STONE OR

- WRAP STAND PIPE WITH

FILTER FABRIC CLOTH

- SIDE SLOPES TO MEET

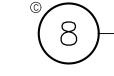
OSHA TRENCHING REQUIREMENTS

MIRAFI 140N

3. CRUSHED STONE OR GRAVEL SHALL BE NYSDOT #2 SIZE OR EQUIVALENT AND SHALL BE WASHED

TYPICAL SECTION OF SUMP PIT

4. DISCHARGE SHALL BE THROUGH DEWATERING BAGS, OR AS DIRECTED BY ENGINEER.



DEWATERING & SUMP PIT DETAIL

PRIOR TO PLACEMENT WITHIN SUMP. 5. CONTRACTOR TO SUBMIT DEWATERING PLAN TO ENGINEER FOR REVIEW & APPROVAL.

> **EROSION & SEDIMENT CONTROL DETAILS 2**

BRIDGEPORT STADIUM &

2230111

ISSUED FOR

04/08/2024

DRAWING NUMBER:

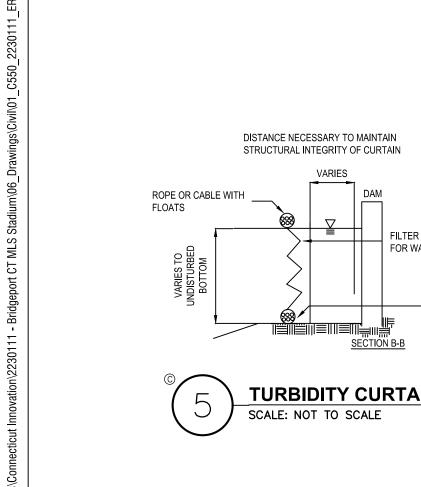
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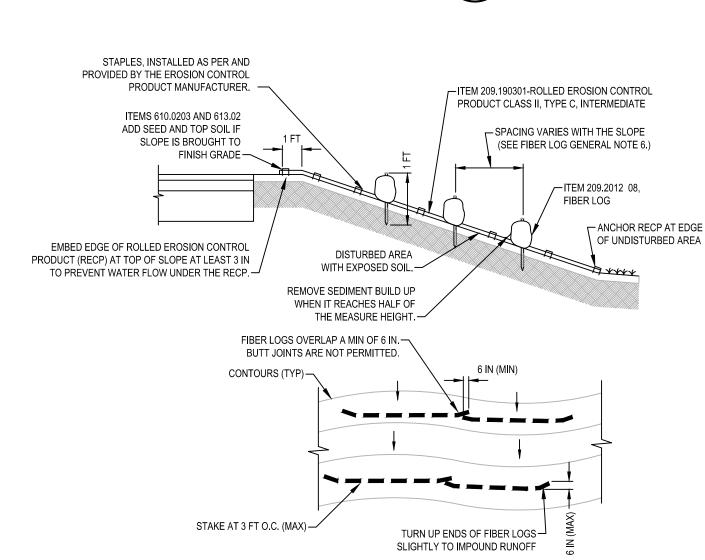
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REVIEWED BY

ISSUED FOR:

DRAWING NAME:



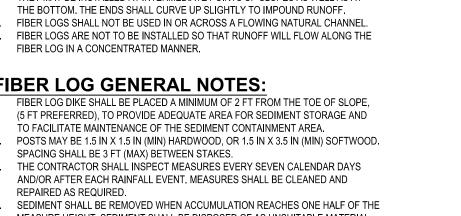


FIBER LOG APPLICATION NOTES THE PRIMARY PURPOSE OF A FIBER LOG DIKE IS TO REDUCE RUNOFF VELOCIT AND TRAP SEDIMENT. VELOCITY IS REDUCED, WATER IS IMPOUNDED BEHIND THE MEASURE, AND SEDIMENT FALLS OUT OF SUSPENSION. FIBER LOG DIKES CAN BE USED IN SENSITIVE AREAS WHERE CONTROL OF WEEDS AND INVASIVE PLANT SPECIES IS DESIRED. FIBER LOG DIKE SHALL BE INSTALLED ON A LINE OF EQUAL ELEVATION (CONTOUR). THEY MAY BE INSTALLED AT INTERMEDIATE POINTS UP SLOPES AS WELL AS AT THE BOTTOM. THE ENDS SHALL CURVE UP SLIGHTLY TO IMPOUND RUNOFF. FIBER LOGS SHALL NOT BE USED IN OR ACROSS A FLOWING NATURAL CHANNEL

6. THE FOLLOWING ARE MAXIMUM SLOPE LENGTHS TO FIBER LOG MEASURES:

MAXIMUM DRAINAGE AREA TRIBUTARY TO 100 FT OF FIBER LOG SHALL BE 0.5 AC.

7. INSTALLATION, I.E. EXCAVATION, BACKFILL, COMPACTION, FIBER LOGS SHALL BE INCLUDED IN UNIT PRICE BID FOR ITEM 209.2012 08.



FIBER LOG GENERAL NOTES: POSTS MAY BE 1.5 IN X 1.5 IN (MIN) HARDWOOD, OR 1.5 IN X 3.5 IN (MIN) SOFTWOOD 4. SEDIMENT SHALL BE REMOVED WHEN ACCUMULATION REACHES ONE HALF OF THE MEASURE HEIGHT. SEDIMENT SHALL BE DISPOSED OF AS UNSUITABLE MATERIAL.

· —

└─3" DIA. INTAKE FROM SUMP

APPROX. 3/4 DIA. BARREI END TO ACT AS BAFFLE <u>SECTION</u> **CONSTRUCTION NOTES** 1. CLEAN OUT THE SEDIMENT TANK WHEN ONE THIRD (1/3) FILLED WITH SILT.

2. STEEL DRUMS ARE USED AS AN EXAMPLE DUE TO THEIR READY AVAILABILITY. ANY TANKS MAY BE USED,

3. ALL SEDIMENT COLLECTED IN THE TANK SHALL BE DISPOSED OF IN A SEDIMENT TRAPPING DEVICE OR AS

CRADLE LEG (TYP.)-

ELEVATION

←12" (APPROX.) CLEANOUT SLOT

CUT OUT (INTERIOR

WALLS ONLY)

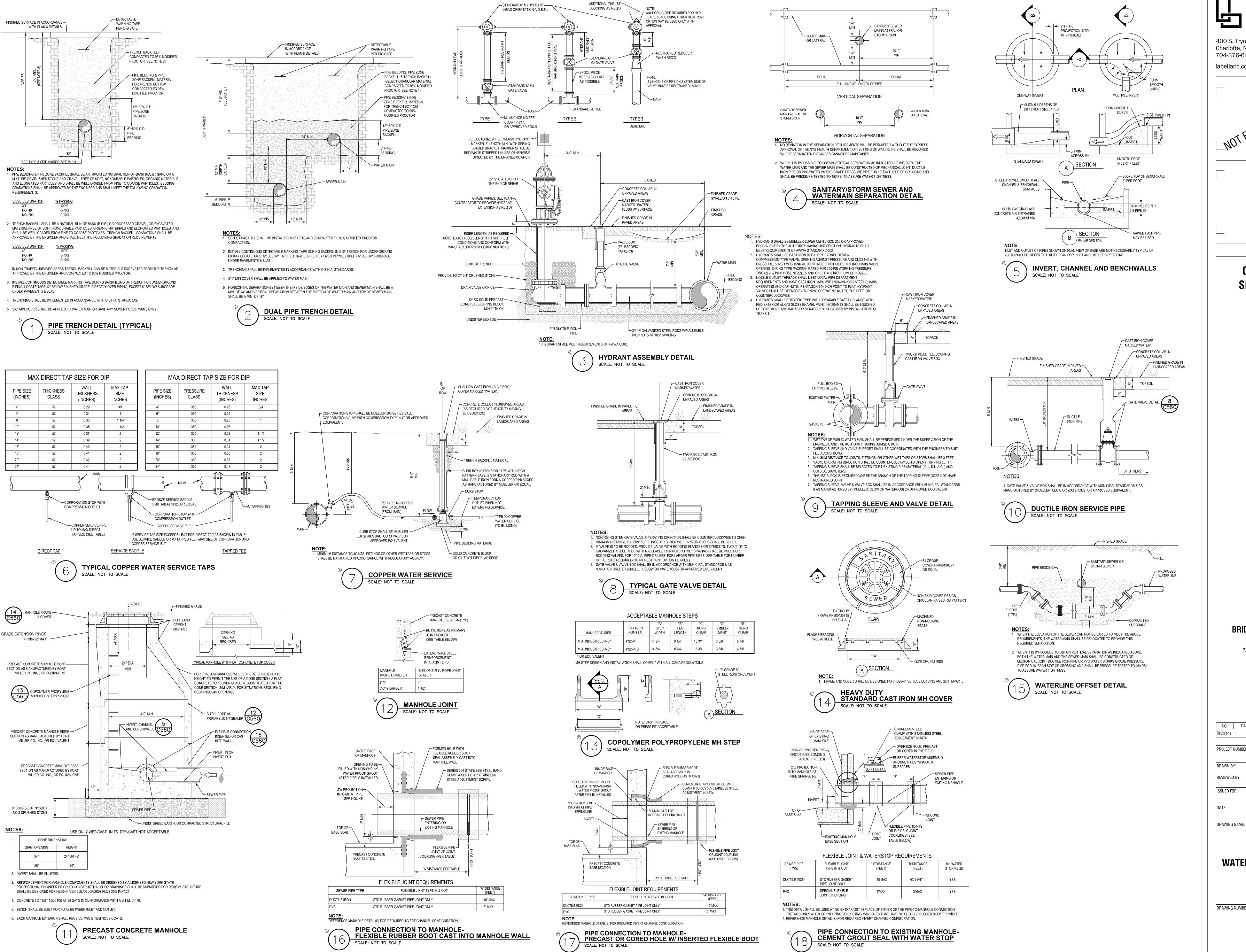
- ENDS OF BARRELS CUT TO ACT AS

– 55 GAL. DRUMS, OR SIMILAR,

WELDED END TO END

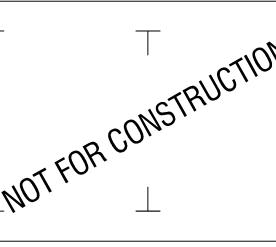
APPROVED BY THE QUALIFIED INSPECTOR. PORTABLE SEDIMENT TANK DETAIL

PROVIDING THAT THE VOLUME REQUIREMENTS ARE MET.



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SPORTS GROUP 9 W BROAD STREET SUITE 430 STAMFORD, CT 06902

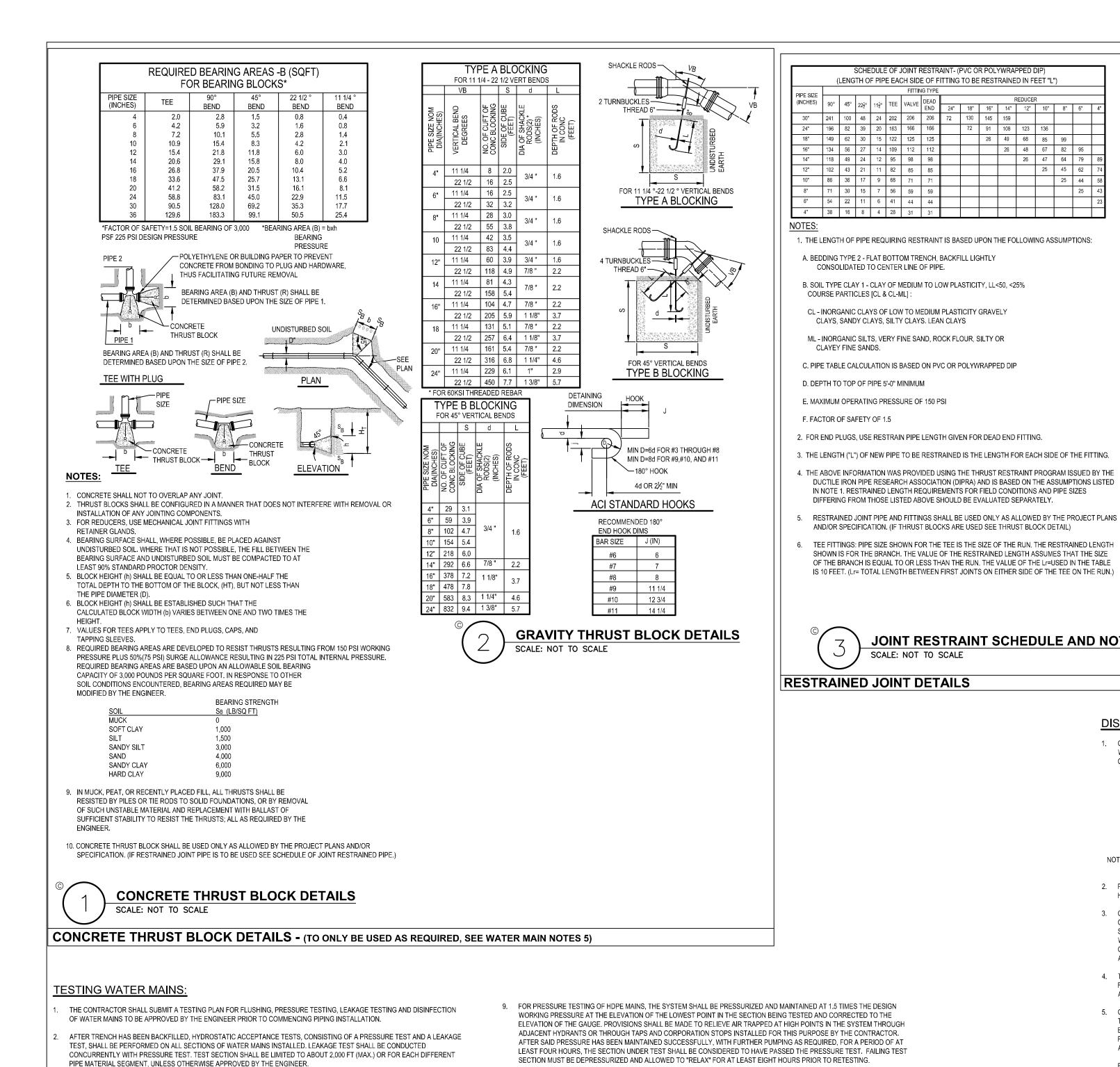
BRIDGEPORT STADIUM & MIXED USE 255 & 363 KOSSUTH STREET

BRIDGEPORT, CT 06608

NO: DATE: PROJECT NUMBER: 2230111 DRAWN BY: REVIEWED BY: ISSUED FOR: ISSUED FOR

WATER SYSTEM DETAILS 1

DRAWING NUMBER:



AFTER ALL TESTS AND INSPECTIONS HAVE BEEN PERFORMED EVIDENCE OF COMPLIANCE SHALL BE FORWARDED TO

ALL WATER FOR TESTS SHALL BE FURNISHED AND DISPOSED OF BY THE CONTRACTOR AT THE CONTRACTOR'S EXPENSE.

SOURCE AND/OR QUALITY OF WATER WHICH THE CONTRACTOR PROPOSES TO USE IN TESTING LINES SHALL BE ACCEPTABLE TO

HYDROSTATIC PRESUMPTIVE TESTS MAY BE PERFORMED WHEN SYSTEM IS PARTIALLY BACKFILLED TO SIMPLY CHECK WORK.

FOR PRESSURE TESTING OF DUCTILE-IRON MAINS, THE SYSTEM SHALL BE PRESSURIZED AND MAINTAINED AT A MINIMUM OF 150

THE LOWEST POINT IN THE SECTION BEING TESTED AND CORRECTED TO THE ELEVATION OF THE GAUGE, PROVISIONS SHALL BE

POUNDS PER SQUARE INCH. OR 1.5 TIMES THE WORKING PRESSURE. WHICHEVER IS GREATER, BASED ON THE ELEVATION OF

MADE TO RELIEVE AIR TRAPPED AT HIGH POINTS IN THE SYSTEM THROUGH ADJACENT HYDRANTS OR THROUGH TAPS AND

CORPORATION STOPS INSTALLED FOR THIS PURPOSE BY THE CONTRACTOR, AFTER SAID PRESSURE HAS BEEN MAINTAINED

FOR PRESSURE TESTING OF PVC MAINS, THE SYSTEM SHALL BE PRESSURIZED AND MAINTAINED AT A MINIMUM OF 1,25 TIMES

THE THE MAXIMUM ANTICIPATED SUSTAINED WORKING PRESSURE AT THE HIGHEST POINT ALONG THE TEST SECTION UNLESS THE PRESSURE EXCEEDS THE DESIGN PRESSURE LIMIT FOR ANY PIPE, THRUST RESTRAINT, VALVE FITTING, OR OTHER

CONTRACTOR. AFTER SAID PRESSURE HAS BEEN MAINTAINED SUCCESSFULLY, WITH FURTHER PUMPING AS REQUIRED, FOR A PERIOD OF AT LEAST TWO HOURS, THE SECTION UNDER TEST SHALL BE CONSIDERED TO HAVE PASSED THE PRESSURE TEST

APPURTENANCE OF THE TEST SECTION & NOT LESS THAN 1.5 TIMES THE STATED SUSTAINED WORKING PRESSURE AT THE LOWEST ELEVATION OF THE TEST SECTION. PROVISIONS SHALL BE MADE TO RELIEVE AIR TRAPPED AT HIGH POINTS IN THE SYSTEM THROUGH ADJACENT HYDRANTS OR THROUGH TAPS AND CORPORATION STOPS INSTALLED FOR THIS PURPOSE BY THE

SUCCESSFULLY, WITH FURTHER PUMPING AS REQUIRED, FOR A PERIOD OF AT LEAST TWO HOURS, THE SECTION UNDER TEST

BUT ACCEPTANCE OF SYSTEM SHALL BE BASED ON HYDROSTATIC TESTS RUN ON FINISHED SYSTEM AFTER IT HAS BEEN

HYDROSTATIC TESTS SHALL BE PERFORMED IN ACCORDANCE WITH THE FOLLOWING, AS MODIFIED HEREIN:

6.1. SECTION 5 OF AWWA STANDARD C600, LATEST EDITION, FOR DUCTILE-IRON MAINS.

SECTION 7 OF AWWA STANDARD C605, LATEST EDITION, FOR PVC MAINS.

6.3. CHAPTER 9 OF AWWA STANDARD M55, LATEST EDITION, FOR HDPE MAINS.

SHALL BE CONSIDERED TO HAVE PASSED THE PRESSURE TEST.

OWNER/ENGINEER AND THE MUNICIPALITY PRIOR TO ACCEPTANCE.

SCALE: NOT TO SCALE

10. LEAKAGE TEST SHALL BE PERFORMED CONCURRENTLY USING A MINIMUM TEST PRESSURE OF 150 LBS/SQUARE INCH, OR 1.5

0.96

0.89

0.83

0.76

12. IF LEAKAGE IN SYSTEM EXCEEDS THE SPECIFIED AMOUNT, THE CONTRACTOR SHALL, AT NO ADDED COST TO THE OWNER,

1.15

0.99

AFTER LEAKAGE RATE HAS STABILIZED.

AVG_TEST_PRESSURE

11. MAXIMUM ALLOWABLE LEAKAGE SHALL BE AS SHOWN IN THE FOLLOWING TABLE:

NOMINAL PIPE DIAMETER-IN

0.76

0.72

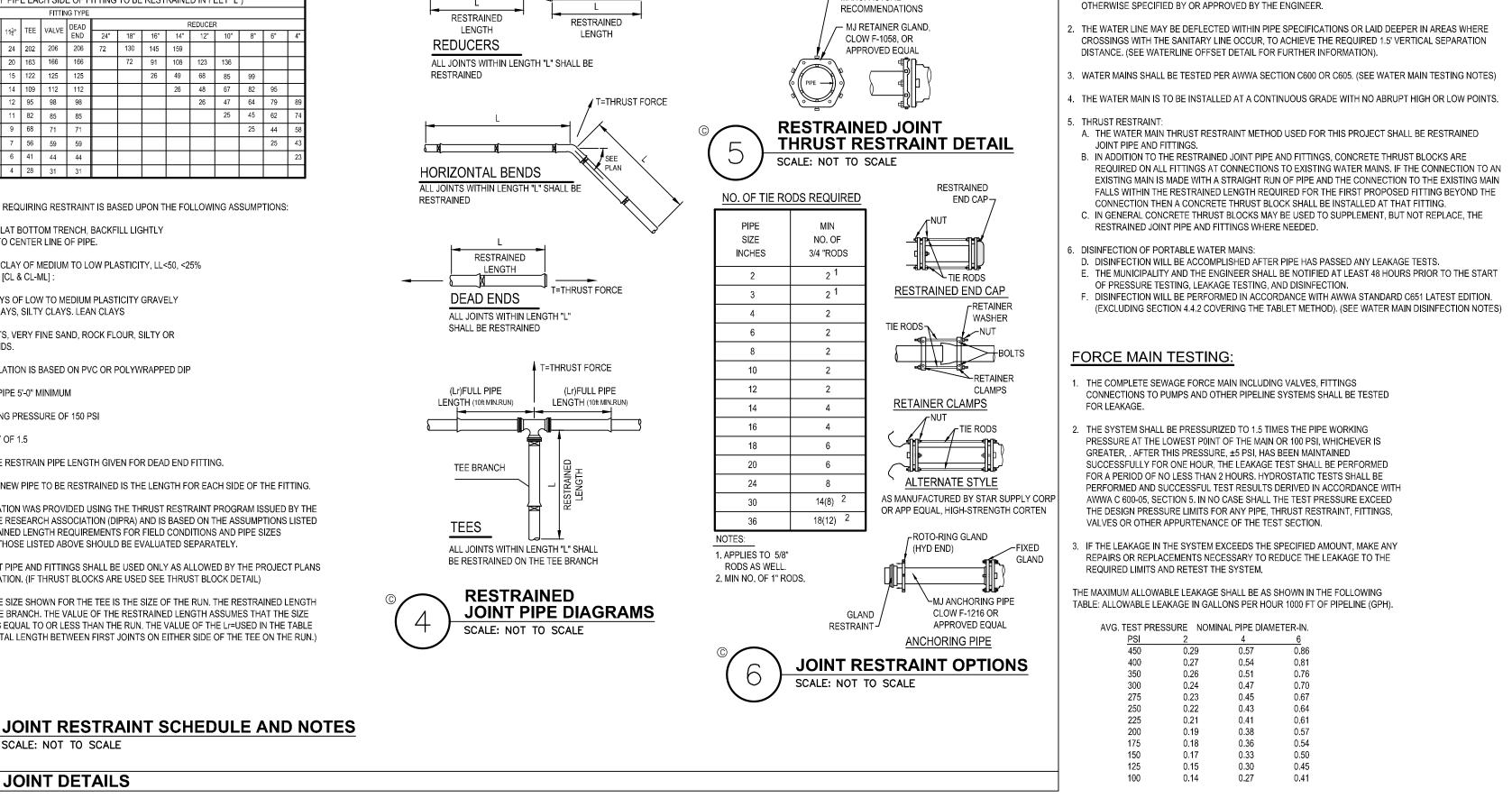
0.60

LOCATE, REPAIR, AND/OR REPLACE DEFECT(S) AND RE-TEST PIPING SYSTEM.

ALLOWABLE LEAKAGE PER 1,000 FT (305M) OF PIPELINE (GPH)

TIMES THE WORKING PRESSURE, WHICHEVER IS GREATER, BASED ON THE ELEVATION OF THE LOWEST POINT IN THE SECTION

UNDER TEST AND CORRECTED TO ELEVATION OF THE GAUGE. LEAKAGE TEST DURATION SHALL BE A MINIMUM OF 2 HOURS



DISINFECTION OF POTABLE WATER SERVICE MAINS

WATER IN ACCORDANCE WITH THE FOLLOWING TABLE (VERIEY AGAINST TOWN REQUIREMENTS

CHLORINE REQUIRED TO PRODUCE 25 MG/L CONCENTRATION IN 100 FT. OF PIPE BY DIAMETER

1.44

1. CHLORINE-WATER SOLUTION IS PREPARED BY ADDING SODIUM HYPOCHLORITE TO

100 PERCENT

0.120

HYPOCHLORITE REQUIRED FOR THE DESIRED CONCENTRATION.

APPLIED TO MAIN.

APPROVED BY THE ENGINEER

AND NEW MAIN

GATE VALVE ON THE HYDRANT LEAD).

CONTAINS 19.75 GAL/FT OF DEPTH OR 1.64 GAL/IN OF DEPTH).

THROUGHOUT THE ENTIRE MAIN DISINFECTED.

EXISTING WATER MAIN THAT IS IN SERVICE.

CONCENTRATION IN THE MAIN IS MAINTAINED AT A MINIMUM OF 25 PPM.

NOTE: 1% SOLUTIONS REQUIRE 1 POUND OF SODIUM HYPOCHLORITE IN 8 GAL OF WATER

2. PRODUCT DETERIORATION MUST BE CONSIDERED IN COMPUTING THE QUANTITY OF SODIUM

3. CHLORINE-WATER SOLUTION SHALL BE INTRODUCED INTO THE WATER MAIN WITH A GASOLINE

OR ELECTRICALLY POWERED CHEMICAL FEED PLIMP DESIGNED FOR FEEDING CHI ORINE

WITHSTAND SAFELY THE MAXIMUM PRESSURE THAT MAY BE CREATED BY PUMP. ALL

4. THE CONTRACTOR SHALL FURNISH AND INSTALL A CORPORATION STOP JUST DOWNSTREAM

5. GENERALLY, THE FOLLOWING PROCEDURE SHALL BE USED TO DISINFECT THE NEW MAIN,

FROM THE NEWLY INSTALLED GATE VALVE OR AS OTHERWISE SHOWN ON DRAWINGS OR

THE CONTRACTOR SHALL HOWEVER, REVIEW THEIR PROPOSED PROCEDURES WITH THE

A. ALL GATE VALVES AND HYDRANTS MUST BE CLOSED. THE NEW MAIN SHOULD ALREADY

BE FULL OF WATER FROM THE HYDROSTATIC TESTS; IF NOT, IT SHALL BE FILLED.

B. MIX CHLORINE-WATER SOLUTION IN 55 GALLON DRUMS; CONNECT FEED LINE TO PUMP

D. START PUMPING CHLORINE-WATER SOLUTION INTO WATER MAIN: THEN OPEN UPSTREAM

F. PERIODICALLY CHECK HYDRANT DISCHARGE FOR CHLORINE CONCENTRATION BY USING A

G. AFTER THE REQUIRED CONCENTRATION HAS BEEN ACHIEVED, ALL VALVES AND HYDRANTS

HYDRANT SHALL BE OPERATED IN ORDER TO DISINFECT THE INTERNAL APPURTENANCES.

UNTIL THE MINIMUM CHLORINE CONCENTRATION OF 25 PPM HAS BEEN ACHIEVED

ON THE MAIN LINE BETWEEN THE UPSTREAM GATE VALVE AND THE DISCHARGE

DO NOT OPERATE ANY GATE VALVE THAT IS LOCATED ON A CONNECTION TO AN

FIELD CHLORINE RESIDUAL TEST KIT. MAINTAIN HYDRANT DISCHARGE AND PUMPING RATE

C. OPEN GATE VALVE ON THE HYDRANT LEAD OF END HYDRANT; THEN OPEN HYDRANT FULLY. (NOTE: HYDRANT MUST

ALWAYS BE EITHER FULLY OPENED OF FULLY CLOSED. THE HYDRANT FLOW MAY BE CONTROLLED BY THROTTLING THE

GATE VALVE SLOWLY UNTIL FLOW FROM HYDRANT IS PROPORTIONATE TO THE AMOUNT OF CHLORINE-WATER SOLUTION

BEING PUMPED (30 PARTS WATER TO 1 PART CHLORINE-WATER SOLUTION). IF A WATER METER IS NOT AVAILABLE,

E. AFTER HYDRANT FLOW AND PUMPING RATE HAVE BEEN ADJUSTED, MAINTAIN A CONSTANT FLOW SO THAT CHLORINE

DISCHARGE RATE MAY BE DETERMINED BY USING EITHER A PITOT GAUGE IN THE DISCHARGE OR BY MEASURING THE

TIME TO FILL A CONTAINER OF KNOWN VOLUME (SUCH AS A 55 GAL, BARREL), THE PUMPING RATE CAN BE DETERMINED

BY MEASURING THE DROP IN LIQUID LEVEL IN A GIVEN LENGTH OF TIME. (NOTE: A STANDARD 55 GALLON STEEL BARREL

ENGINEER AT LEAST 48 HOURS PRIOR TO START OF DISINFECTION, ALL DISINFECTION

PROCEDURES MUST BE APPROVED BY THE ENGINEER BEFORE DISINFECTION STARTS.

CONNECTIONS SHALL BE CHECKED FOR TIGHTNESS BEFORE HYPOCHLORITE SOLUTION IS

SOLUTIONS. FEED LINES SHALL BE OF SUCH MATERIAL AND STRENGTH TO PERMIT THEM TO

PIPE SIZE CHLORINE CHLORINE SOLUTIONS

- SET SCREW, PER

MANUFACTURE

6. AFTER THE WATER SAMPLES HAVE BEEN TAKEN AND THE MINIMUM 25 PPM CHLORINE CONCENTRATION HAS BEEN VERIFIED,

9. ANY SECTION OF PIPE, VALVES OR FITTINGS, INCLUDING TAPPING SLEEVES AND VALVES WHICH ARE INSTALLED OUTSIDE THE LIMITS OF THE SYSTEM SUBJECTED TO THE CHLORINATION PROCEDURES SPECIFIED ABOVE, SHALL BE SPRAYED OR SWABBED WITH A 1% HYPOCHLORITE

10. AFTER THE WATER SAMPLES HAVE BEEN TAKEN AND THE MINIMUM 10 PPM CHLORINE RESIDUAL HAS BEEN VERIFIED. CONTRACTOR SHALL THOROUGHLY FLUSH CHLORINATED WATER FROM THE MAIN BY THE FOLLOWING METHOD:

B. SECOND, OPEN THE UPSTREAM GATE VALVE. C. THIRD, OPEN ANY HYDRANTS ON THE MAIN LINE TO REMOVE ALL CHLORINATED WATER

11. FLUSH THE MAIN WITH POTABLE WATER IN SUCH A MANNER THAT DOES NOT ADVERSELY AFFECT FISH, PLANT, OR ANIMAL LIFE. PROVIDE FOR PROPER DISPOSAL OF HEAVY CHLORINATED WATER OR NEUTRALIZE IN

ACCORDANCE WITH APPENDIX C OF AWWA C651 LATEST EDITION.

13. WATER SAMPLES SHALL BE TAKEN BY THE CONTRACTOR IN STERILIZED BOTTLES.

ASSN., 6666 WEST QUINCY AVE., DENVER, CO 80235. 15. IF A BACTERIOLOGICAL TEST PROVES THE WATER QUALITY TO BE UNACCEPTABLE; REPEAT

16. IF A BACTERIOLOGICAL TEST PROVES WATER TO BE ACCEPTABLE; REMOVE FEED LINE AND CORPORATION STOP. CORPORATION STOP WILL BE REPLACED WITH A THREADED BRASS

SAMPLES MUST BE BACTERIOLOGICALLY SAFE AND THE MUNICIPALITY, ENGINEER & HEALTH DEPARTMENT MUST PROVIDE APPROVAL BEFORE THE WATER MAIN IS PLACED INTO SERVICE.

0.38

0.33

0.30

0.17

0.15

WATER MAIN NOTES:

ALL WATER LINES SHALL BE CEMENT LINED DUCTILE IRON PIPE, CLASS 52, OR PVC C900 UNLESS

B. SECOND, CLOSE THE DISCHARGE HYDRANT. C. THIRD, SHUT OFF THE PUMP.

A. FIRST, CLOSE THE UPSTREAM GATE VALVE.

7. CHLORINATED WATER SHALL REMAIN IN THE MAIN FOR A MINIMUM OF 24 HOURS 8. IF THE CHLORINE RESIDUAL IS LESS THAN 10 PPM AT THE END OF THE 24 HOURS, REPEAT SYSTEM TREATMENT

THE CONTRACTOR SHALL RETAIN THE CHLORINATED WATER IN THE MAIN BY THE FOLLOWING METHOD:

A. FIRST, OPEN THE DISCHARGE HYDRANT.

FROM THE HYDRANT LEADS.

12. THE QUANTITY AND LOCATION OF WATER SAMPLES TO BE TAKEN SHALL BE IN ACCORDANCE WITH

14. ANALYZE WATER SAMPLES IN ACCORDANCE WITH STANDARD METHODS FOR EXAMINATION OF WATER AND WASTEWATER, 14TH EDITION, PUBLISHED BY AMERICAN WATER WORKS

PLUG UNLESS OTHERWISE DIRECTED BY ENGINEER.

1. CONTRACTOR SHALL INSPECT AND TEST THE INSTALLATIONS AS REQUIRED BY THE AUTHORITY HAVING JURISDICTION WHEN WORK IS READY FOR TESTING. AFTER ALL TESTS HAVE BEEN PERFORMED, EVIDENCE OF COMPLIANCE SHALL BE FORWARDED TO OWNER/ENGINEER AND THE AUTHORITY HAVING JURISDICTION PRIOR TO ACCEPTANCE.

TESTING GRAVITY SEWER SYSTEM:

THE CONTRACTOR SHALL TEST AND INSPECT FOR ALIGNMENT AND INFILTRATION AND EXFILTRATION OF ALL SANITARY SEWERS AND RELATED UTILITY STRUCTURES, INFILTRATION OR EXELL TRATION OF THE SANITARY SEWER SYSTEM SHALL NOT EXCEED 0.80 GAL/INCH OF INTERNAL PIPE DIAMETER PER 1000' OF PIPELINE PER HOUR WITH A MINIMUM HYDROSTATIC HEAD AT THE TOP OF

THE PIPE OF 2 FT, OR AS REQUIRED BY THE AUTHORITY HAVING JURISDICTION. WHEN INFILTRATION OR EXFILTRATION OCCURS IN EXCESS OF ALLOWABLE AMOUNT, DEFECTS SHALL BE LOCATED AND REPAIRED. 3. INFILTRATION LEAKAGE TESTS SHALL BE RUN ON EACH SINGLE MANHOLE-TO-MANHOLE SECTION, OR REACH, INDEPENDENTLY OF

ALL OTHER MANHOLE-TO-MANHOLE SECTIONS. A PIPELINE SECTION UNDER TEST SHALL INCLUDE ALL PIPE AND FITTINGS BETWEEN THE TWO MANHOLES PLUS THE UPSTREAM MANHOLE. 4. EACH MANHOLE-TO-MANHOLE SECTION SHALL BE REJECTED OR ACCEPTED BASED ONLY ON RESULTS OF ITS OWN INDEPENDENT SECTION TEST AND NOT ON RESULTS OF ANY ONE TEST RUN SIMULTANEOUSLY OVER MORE THAN ONE CONSECUTIVE MANHOLE-TO-MANHOLE SECTION, THE ONLY EXCEPTION ALLOWED: ACCEPTING SEVERAL CONSECUTIVE MANHOLE-TO-MANHOLE SECTIONS BASED ON ONE COMBINED INFILTRATION TEST INDICATING ZERO INFILTRATION.

BEING TESTED. TEST DURATION SHALL BE 24 HRS. OR FOR SHORTER PERIOD, PROVIDED A STEADY STATE FLOW CONDITION HAS BEEN ACHIEVED IN THE TEST PERIOD, AND RESULTS PROJECTED TO A 24 HR PERIOD. 6. EXFILTRATION TESTS SHALL BE RUN ON EACH SINGLE MANHOLE-TO-MANHOLE SECTION, OR REACH, INDEPENDENTLY OF ALL OTHER MANHOLE-TO-MANHOLE SECTIONS. A PIPELINE SECTION UNDER TEST SHALL INCLUDE ALL PIPE AND FITTINGS BETWEEN THE TWO MANHOLES PLUS THE UPSTREAM MANHOLE.

5. INFILTRATION TESTS SHALL BE MADE BY INSTALLING A FLOW MEASURING DEVICE IN THE DOWNSTREAM MANHOLE OF SECTION

EXFILTRATION TESTS SHALL BE MADE BY MEASURING THE DROP IN WATER ELEVATION IN THE UPSTREAM MANHOLE 24 HRS AFTER INITIAL WATER LEVEL IS RECORDED. INITIAL WATER LEVEL IN UPSTREAM MANHOLE SHALL BE 2 FEET HIGHER THAN EITHER THE TOP OF PIPE OR GROUNDWATER ELEVATION AT THE DOWNSTREAM MANHOLE. ANY MANHOLE-TO-MANHOLE SECTION UNDERGOING AN EXFILTRATION TEST MUST HAVE THE NEXT ADJACENT SECTIONS, BOTH UPSTREAM AND DOWNSTREAM, DRY AND NOT UNDER TEST. THIS PROCEDURE MINIMIZES HYDROSTATIC PRESSURE PLACED ON STOPPERS, PLUGS, AND END CAPS. 8 LOW PRESSURE AIR TESTING MAY BE ALLOWED IN LIEU OF EXFILTRATION TESTS ONLY, WHEN SO ALLOWED, TEST SHALL BE

PERFORMED UNDER DIRECTION OF ENGINEER ACCORDING TO ASTM F1417. LOW PRESSURE AIR TEST IS A COMPARISON OF THE

THAT PRESSURE DROP TO OCCUR DETERMINED BY METHODS INDICATED IN ASTM F1417. IF THE ONE (1) PSIG PRESSURE DROP

MEASURED TIME NECESSARY FOR ONE (1) PSIG PRESSURE DROP TO OCCUR, IF AT ALL, WITH MINIMUM ALLOWABLE TIME FOR

OCCURS FASTER THAN ALLOWABLE TIME, SECTION IS UNACCEPTABLE 9. AN AIR TEST SHALL NOT BE RUN UNTIL SECTION OF LINE TO BE TESTED HAS BEEN CLEANED OF ALL FOREIGN MATERIAL BY FLUSHING AND HAS BEEN VISUALLY INSPECTED AND APPROVED BY THE ENGINEER. CERTAIN PIPE MATERIALS PRODUCE MORE CONSISTENT RESULTS WHEN INTERIOR OF PIPE IS WETTED PRIOR TO TESTING.

10. WHERE AIR-TESTING IS TO BE USED FOR LINE ACCEPTANCE, CORROBORATIVE HYDROSTATIC TESTING SHALL BE PERFORMED ON SEWER INSTALLATION OF THE SAME PIPE SIZE, MATERIAL, AND CONDITIONS OF INSTALLATION, SEWER SECTIONS WHICH INDICATE RATES OF AIR LOSS PER UNIT OF SURFACE AREA WHICH MOST NEARLY APPROXIMATE RATE FOR PIPELINE ACCEPTANCE SHOULD BE SELECTED FOR CORROBORATIVE TESTS. AT LEAST 3 SECTIONS ARE TO BE SO TESTED. THE PURPOSE OF THESE CORROBORATIVE TESTS IS TO PERMIT A REASONABLE ASSUMPTION THAT, IF THESE 3 TEST SECTIONS MEET THE HYDROSTATIC TEST, THE BALANCE OF PROJECT ALSO MEETS OR EXCEEDS THESE REQUIREMENTS. IF AIR TEST IS NOT SUPPORTED BY ACCEPTABLE CORROBORATIVE HYDROSTATIC TESTS, COMPLETE HYDRO-STATIC TESTING OF SEWER LINES SHALL BE REQUIRED.

11. WHERE FLEXIBLE PIPE IS USED, CONTRACTOR SHALL TEST ALL MAINLINE PIPE FOR MAXIMUM ALLOWABLE DEFLECTION OF 5% OF OUTSIDE DIAMETER. DEFLECTION TESTS SHALL BE PERFORMED USING A CIRCULAR STEEL BALL ON SLED 1/16-INCH IN DIAMETER SMALLER THAN ALLOWABLE INSIDE DIAMETER OF FLEXIBLE PIPE WHEN DEFLECTED A MAXIMUM OF 5% OF OUTSIDE DIAMETER. DEFLECTION TESTING OF ANY PIPE SHALL BE DONE NO SOONER THAN 30 DAYS AFTER DATE OF INSTALLATION OF PIPE SECTION

12. SEWERS SHALL BE LAID WITH STRAIGHT ALIGNMENT BETWEEN MANHOLES. STRAIGHT ALIGNMENT SHALL BE CHECKED EITHER USING A LASER BEAM OR LAMPING, TESTING SHALL COMPLY WITH REQUIREMENTS OF THE AUTHORITY HAVING JURISDICTION. 13. MANHOLES, WHICH CANNOT BE PROPERLY AIR TESTED, SHOULD BE VISUALLY INSPECTED AND LEAKAGE-TESTED USING INTERNAL OR EXTERNAL HYDROSTATIC PRESSURE. LEAKAGE TESTING SHALL COMPLY WITH REQUIREMENTS OF THE AUTHORITY HAVING

14. IN AREAS WHERE CONVENTIONAL TESTING IS IMPRACTICAL (I.E. AREAS DESIGNATED BY ENGINEER WHERE EXISTING SERVICES ARE TIED INTO NEW LINE IMMEDIATELY AND ANY BLOCKAGE COULD RESULT IN HEALTH PROBLEMS) NO LINES SHALL BE BACKFILLED UNTIL EACH PIPE SECTION AND CONNECTION IS INSPECTED AND APPROVED.

15, WHERE SEWERS ARE CONSTRUCTED OF PRESSURE-RATED PIPE AND INSTALLED WITH LESS THAN 18 INCHES VERTICAL SEPARATION FROM EXISTING OR PROPOSED WATER MAINS, SEWERS SHALL BE HYDROSTATICALLY TESTED AT 150 PSI TO ASSURE WATER TIGHTNESS. HYDROSTATIC ACCEPTANCE TESTS SHALL BE CONDUCTED AS SPECIFIED FOR TESTING WATER MAINS, EXCEPT THAT TESTING MAY BE PERFORMED WITH THE PIPE SECTION PARTIALLY BACK-FILLED.

16. IF THE ALLOWABLE RATE OF INFILTRATION, EXFILTRATION, OR AIR LEAKAGE IS EXCEEDED, THE CONTRACTOR SHALL LOCATE POINTS OF EXCESSIVE LEAKAGE AND SHALL PROMPTLY CORRECT, REPAIR, AND BRING SYSTEM UP TO THE STANDARD. COSTS OF ALL SUCH REPAIRS AND CORRECTIVE MEASURES. INCLUDING COSTS OF REPEATED TESTS. SHALL BE BORN BY CONTRACTOR. THE SEWER LINE SECTION (INCLUDING MANHOLES AND BUILDING SERVICES) UNDER TEST SHALL NOT BE ACCEPTED UNTIL THESE TEST

MANHOLES AND OTHER BELOW GRADE STRUCTURES:

BELOW GRADE PRECAST CONCRETE STRUCTURES SHALL BE DESIGNED TO WITHSTAND LOADS IMPOSED BY STRUCTURE WEIGHT. EARTH COVER. LATERAL PRESSURE FROM EARTH AND GROUND WATER, AND LIVE LOADS SUCH AS PEDESTRIAN TRAFFIC OR MACHINERY ON OR ABOVE THE STRUCTURE; AND

BELOW GRADE PRECAST CONCRETE STRUCTURES SHALL BE DESIGNED TO ALSO WITHSTAND TRAFFIC LOADS CREATED BY AN HS20-44 TRUCK PLUS 25% IMPACT AS DEFINED IN THE LATEST EDITION OF THE AMERICAN ASSOCIATION OF STATE HIGHWAY AND TRANSPORTATION OFFICIALS (AASHTO) DESIGN STANDARDS.

2. MATERIAL WHICH SHALL BE UTILIZED IN THE CONSTRUCTION OF PRECAST CONCRETE STRUCTURES: CEMENT: ASTM C-150, TYPES I,II,III,VI NYSDOT STD. SPEC. SECTION NO. 703-0 CONCRETE SAND NYSDOT STD. SPEC. SECTION NO. 703-02 COARSE AGGREGATE STEEL BAR REINFORCEMENT: ASTM A615, GRADE 60 WIRE MESH REINFORCEMENT: ASTM A185 PLAIN

CONCRETE STRENGTH (28 DAY): 4,500 PSI (F'C)

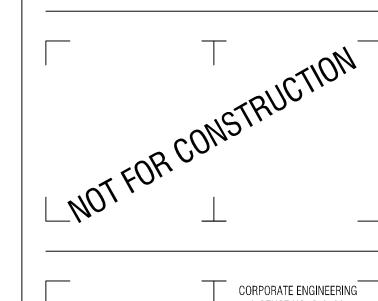
ENTRAINED AIR: 5% MIN. 3. ALL CASTINGS (FRAMES AND COVERS, FRAMES AND GRATES, ETC.) FOR USE IN CONJUNCTION WITH MANHOLES AND OTHER BELOW GRADE STRUCTURES SHALL BE MANUFACTURED FROM GRAY IRON OR DUCTILE IRON. GRAY IRON SHALL CONFORM WITH ASTM A 48, CLASS 30B AND DUCTILE IRON SHALL CONFORM WITH ASTM A 536 AND BE OF A GRADE APPROPRIATE TO

4. ALL CASTINGS (FRAMES AND COVERS, FRAMES AND GRATES, ETC.) FOR USE IN CONJUNCTION WITH MANHOLES AND OTHER BELOW GRADE STRUCTURES SHALL BE DESIGNED TO WITHSTAND AASHTO HS 20-44 HIGHWAY LOADING PLUS 25% IMPACT.

5. ALL ASTM REFERENCES SHALL BE FOR THE LATEST ACTIVE STANDARD.

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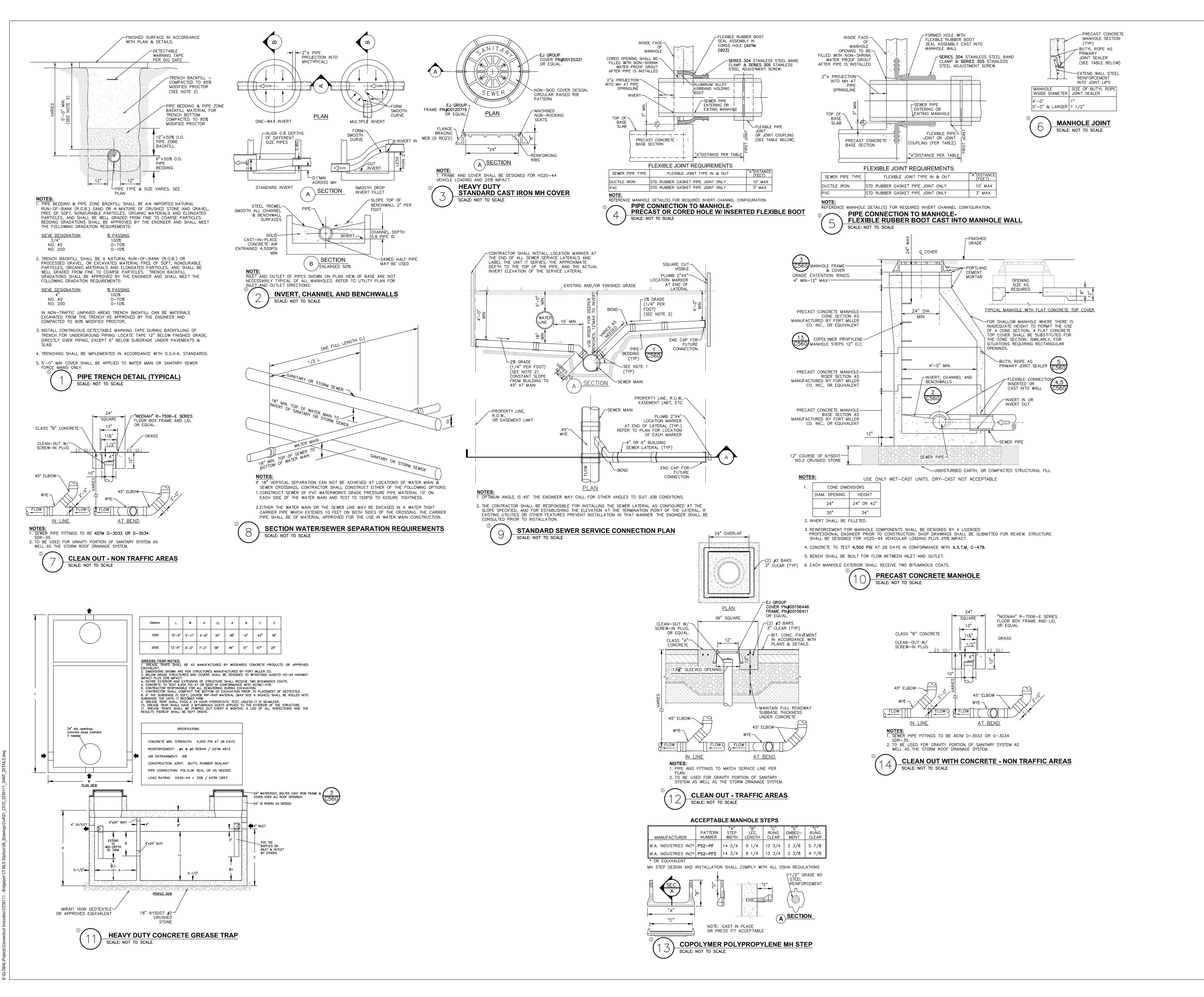
CONNECTICUT 9 W BROAD STREET SUITE 430 STAMFORD, CT 06902

BRIDGEPORT STADIUM & MIXED USE 255 & 363 KOSSUTH STREE

NO: DATE: PROJECT NUMBER: DRAWN BY REVIEWED BY: ISSUED FOR: **ISSUED FOR** DRAWING NAME:

WATER SYSTEM DETAILS 2

DRAWING NUMBER:



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CHARLOTTE. N. C.

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SPORTS GROUP

9 W BROAD STREET
SUITE 430
STAMFORD, CT 06902

BRIDGEPORT STADIUM & MIXED USE

255 & 363 KOSSUTH STREET

BRIDGEPORT, CT 06608

NO: DATE: DESCRIPTION:

Revisions

PROJECT NUMBER:

2230111

DRAWN BY:

AC

REVIEWED BY:

JRS

ISSUED FOR:

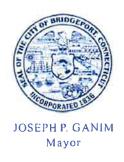
DATE:

04/08/2024

SANITARY SEWER DETAILS

DRAWING NUMBER:

DRAWING NAME:



City of Bridgeport OFFICE OF PLANNING & ECONOMIC DEVELOPMENT

Margaret E. Morton Government Center 999 Broad Street, Bridgeport, Connecticut 06604

> THOMAS F. GILL Director

WILLIAM J. COLEMAN
Deputy Director

TO:

Honorable Members of the Planning and Zoning Commission

COPY:

Paul Boucher, Zoning Administrator

William Coleman, Deputy Director of Economic Development

FROM:

Jackson Strong, Design Review Coordinator

DATE:

9/10/2024

RE:

Zoning Text Amendments

Petition of the Office of Planning and Economic Development to amend provisions of *Zone Bridgeport* related to Row Building site & development standards, procedures, and definitions.

Please find the following items contained in this report:

I. Text Amendments

Pg. 2-4



CITY OF BRIDGEPORT

| File No. | | |
|-----------|--|------|
| I IIC 140 | | |

PLANNING & ZONING COMMISSION APPLICATION

| -44 | COMMITTEE IN COMMI | C D 1 | T WOED | | |
|-------|--|-------------------------|-----------------------------|----------|---------------------|
| . NA | AME OF APPLICANT: City | * Rudgeb | on, open | | |
| . Is | the Applicant's name Trustee of Recor | u! 165 | | | |
| "If y | es, a sworn statement disclosing the E | Beneficiary shall accor | npany this application upon | umg. | |
| . Ad | dress of Property: | | | | (zip code) |
| | (number) | (street) | (state) | | |
| . As | sessor's Map Information: Block No. | | Lot No | | · · |
| . Ar | nendments to Zoning Regulations: (inc | ficate) Article: _Sec_ | affected Section | | |
| | ttach copies of Amendment) | w | 70 | | |
| S. De | escription of Property (Metes & Bounds | | | | |
| | isting Zone Classification: | | | | |
| | ne Classification requested: | | | | |
| 9. De | escribe Proposed Development of Pro | perty: | | | |
| Αp | oproval(s) requested: | Bldg Type | Text Aroulose. | v Kr | |
| lf : | signed by Agent, state capacity (Lawy | Pr | int Name: | | |
| M | ailing Address: | | Eav | | |
| | none: | Cell: | | | |
| E- | mail Address: | | | | |
| \$, | Fee received | Date: | Clerk: | <u> </u> | |
| | THIS APPLICATION MUST B | E SUBMITTED IN P | ERSON AND WITH COMP | LETE | CHECKLIST |
| (2) | Completed & Signed Application Fo | | A-2 Site Survey | | Building Floor Plan |
| 0 | Completed Site / Landscape Plan | × 0 | Drainage Plan | | Building Elevations |
| 0 | | | Property Owner's List | = | Fee |
| 0 | Written Statement of Development Cert. of Incorporation & Organization | | | | |
| 0 | | | | | |
| | PROPE | RTY OWNER'S END | ORSEMENT OF APPLICA | ATION | |
| | Print Owner's Name | Owner's S | ignature | | Date |
| _ | Print Owner's Name | Owner's S | ignature | - | Date |

TEXT AMENDMENTS

Section 3.70: Row Building Type

1. §3.70.9

Description of Change: Create separate columns for NX1 and NX2 to allow for different standards to be established for the different zoning districts

2. §3.70.9 (2)

Description of Change: Reduce primary streetwall percentage to avoid unnecessary variances

Existing Text: 80% min, 85% min

Proposed Text: 70% min.

3. §3.70.8

Description of Change: Limit number of units to 2 per row house in NX1 zone; currently no limit exists for Row Buildings or Row Houses within Row Buildings

Proposed Text: 2 Per Row House

4. **§3.70.9**

Description of Change: Limit number of units to 3 per row house in NX2 zone; currently no limit exists for Row Buildings or Row Houses within Row Buildings

Proposed Text: 3 Per Row House

5. **§3.70.6**

Description of Change: Create separate column for NX3, Combine NX4 and RX2 columns; Combine NX2 and RX1 Columns

Existing Text: NX3, NX4, RX1, RX2

Proposed Text: NX3; NX4; RX2; NX2 RX1

6. §3.70.6 (1)

Description of Change: Change max. no. of stories from 3 to 3.5 within NX3 zoning districts

Existing Text: 3

Proposed Text: 3.5

7. §3.70.6 (1)

Description of Change: Change max. no. of stories from 3 to 5 within NX4 & RX2 zoning districts

Existing Text: 3
Proposed Text: 5

8. §3.70.7 (5)

Description of Change: Allow flat, parapet roof types in NX1 zones

Existing Text: Pitched

Proposed Text: Pitched, flat, parapet

9. §3.70.8 (2)

Description of Change: Change language to specify one entrance per row house

Existing Text: One per unit on primary façade except 1 per every 3 units may be located off a courtyard.

Proposed Text: One per Row House on primary façade except 1 per every 3 units may be located off a courtyard.

10. **§3.70.8 (2)**

Description of Change: Remove restriction on number of row houses to allow for Row Building configuration to be based on size of lot

Existing Text: 4 units max.; 8 units max.; 10 units max

11. **§3.70.10.D**

Description of Change: Provide annotated design diagram for row building types

Proposed Text: (Diagram)

- -Vertical division element between rowhouses
- -Entrance Locations

Chapter 12: Procedures

12. Subdivisions §11.100

Description of Change: Exempt row buildings from §10.40 subdivision standards if lot is being subdivided along Party Walls.

Existing Text: The subdivision procedures of this section are intended to ensure that proposed subdivisions are reviewed to determine compliance with all applicable regulations, including the subdivision design regulations of 10.40. All subdivisions of land are subject to these procedures

Proposed Text: The subdivision procedures of this section are intended to ensure that proposed subdivisions are reviewed to determine compliance with all applicable regulations, including the subdivision design regulations of 10.40. All subdivisions of land are subject to these procedures except where land subdivisions are divided by a Party Wall.

Chapter 14: Measuring & Definitions

13. Row House §14.200

Description of Change: Row House term needs definition

Existing Text: N/A

Proposed Text: Row House: A residential structure within a Row Building, designed to accommodate one or more independent dwelling units. Each Row House shares one or more common dividing walls with adjacent structures and is oriented to the street or courtyard featuring an entrance off the public sidewalk.

Row Building, Subdivision, and Definitions Text Amendments

| Category | Sub Category | Section | Description of Change | Proposed Text Amendment | Page |
|----------------|--------------------------------------|--------------------------|---|--|------------------|
|) Standards | Use | 53.70.9 | Create separate columns for NX1 and NX1; NX2 NX2 | VX1; NX2 | 3-50 |
| 2 | Building Location | \$3,70,4(2) | uce primary streetwall percentage | NX2 Column: 00% Min NX3, NX4, RX1, RX2 Column: 85% Min- 70% Min | 3-46 |
| m | Use | \$3.70.8 | Limit number of units to 2 per row house in NX1 zone | 2 Per Row House | 3-50 |
| 4 | Use | \$3.70.9 | Limit number of units to 3 per row house in NX2 zone | 3 Per Row House | 3-50 |
| ·s | Height | \$3.70.6 | Create separate column for NX3, Combine NX4 and RX2 colums; Combine NX2 and RX1 Columns | NX3,NX4, RX1, RX2,NX3; NX4; RX2; NX2 RX1 | 3-48 |
| • | Height | §3.70 _* 6 (1) | Change max. no. of stories from 3 to 3.5 within NX3 zoning districts | 3.5 | 3-48 |
| | Height | 53.70.6(1) | Change max. no. of stories from 3 to 5 within RX2 & NX4 zoning districts | 5 | 3-48 |
| 80 | Roofs | §3.70,7 (5) | Allow flat, parapet roof types in NX1 zones | Pitched, flat, parapet | 3-48 |
| 6 | Building Entrances Location | \$3.70.8 (2) | Change language to specify one entrance per row house | One per unit Row House on primary façade except 1 per every 3 units may be located off a courtyard. | 3-49 |
| 10 | Façade Witdth Per Street Frontage | 53.70.4(2) | Remove restriction on number of row houses | 4 units max., ੳ units max., 10 units max | 3-46 |
| 11 | Design Standards | §3,70,10,D | Provide annotated design diagram for (Diagram) row building types Entrance Entrance | (Diagram) -Vertical division element between rowhouses -Entrance Locations | 3-52 |
| 72 Procedures | Subdivisions | 811.100 | Exempt row buildings from §10,40 subdivision standards | The subdivision procedures of this section are intended to ensure that proposed subdivisions are reviewed to determine compliance with all applicable regulations, including the subdivision design regulations of 10,40. All subdivisions of land are subject to these procedures except where land subdivisions are divided by a Party Wall. | 2 1.1 |
| 13 Definitions | Row House | \$14.200 | define term | Row House: A residential structure within a Row Building, designed to accommodate one or more independent dwelling units. Each Row House shares one or more common dividing walls with adjacent structures and is oriented to the street or courtyard featuring an entrance off the public sidewalk. | 14-15 |